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# Colvin Development Traffic Impact Analysis 

Jurisdiction: City of Marysville

March 2022


## Kimley»Horn

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## 1. DEVELOPMENT IDENTIFICATION

Kimley-Horn and Associates, Inc. has been retained to provide a traffic impact analysis for the Colvin Development. This report is intended to provide the City of Marysville, Snohomish County, and the Washington State Department of Transportation (WSDOT) with the necessary trip generation, trip distribution and level of service information to facilitate their reviews of the development. The Colvin Development is located on the west side of Densmore Road, south of E Sunnyside School Road in the City of Marysville. A site vicinity map is included in Figure 1.

The Colvin Development is proposed to consist of 29 single-family detached residential units. There is currently 1 existing single-family detached residential units on-site that will be removed and is creditable towards the Colvin Development. Therefore, this report has been completed for 28 net new single-family detached residential units. The site is proposed to have one access to Densmore Road and will provide stub-roads to adjacent parcels.

Brad Lincoln, responsible for this report and traffic analysis, is a licensed professional engineer (Civil) in the State of Washington and member of the Washington State section of ITE.

## 2. METHODOLOGY

The analysis contained in this report is based on the City of Marysville Traffic Impact Analysis Guidelines. The trip generation calculations are based on average trip generation rates published in the Institute of Transportation Engineers (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition (2021). The trip distribution is based on the City of Marysville trip distribution for the Whiskey Ridge North area. Intersection operational analysis is typically required for intersections impacted by 25 PM peak-hour trips generated by the development.

The City of Marysville Traffic Impact Analysis Guidelines typically require analysis for the opening year and a 6-year horizon year beyond the opening year. A reasonable opening year for the Colvin Development is the year 2024. Intersection analysis has therefore been performed for the 2024 opening year and 2030 horizon year as part of this report. The Colvin Development is proposed to have one access to Densmore Road and will also include stub-road connections to adjacent parcels.


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The level of service analysis at the study intersection has been performed in accordance with the Highway Capacity Manual $6^{\text {th }}$ Edition (HCM). Congestion is generally measured in terms of level of service (LOS). Road facilities and intersections are rated between LOS A and LOS F, with LOS A being free flow and LOS F being forced flow or over-capacity conditions. A summary of the level of service criteria is included in Table 1.

Table 1: Level of Service Criteria

| Level of 1 <br> Service | Expected <br> Delay | Intersection Control Delay <br> (Seconds per Vehicle) |  |
| :---: | :---: | :---: | :---: |
|  |  | Unsignalized and <br> Roundabout <br> Intersections | Signalized <br> Intersections |
| A | Little/No Delay | $\leq 10$ | $\leq 10$ |
| B | Short Delays | $>10$ and $\leq 15$ | $>10$ and $\leq 20$ |
| C | Average Delays | $>15$ and $\leq 25$ | $>20$ and $\leq 35$ |
| D | Long Delays | $>25$ and $\leq 35$ | $>35$ and $\leq 55$ |
| E | Very Long Delays | $>35$ and $\leq 50$ | $>55$ and $\leq 80$ |
| F | Extreme Delays ${ }^{2}$ | $>50$ | $>80$ |

The level of service at two-way stop-controlled intersections is based on the average delay for the stopped approach with the highest delay. The level of service at all-way stop-controlled intersections and signalized intersections is based on the average delay for all vehicles. The level of service analysis for unsignalized and signalized intersections has been performed utilizing the Synchro 11.1, Build 1 software. City of Marysville identifies acceptable level of service for the intersections that have been evaluated as part of this report as LOS D.

## ${ }^{1}$ Source: Highway Capacity Manual $6^{\text {th }}$ Edition.

LOS A: Free-flow traffic conditions, with minimal delay to stopped vehicles (no vehicle is delayed longer than one cycle at signalized intersection).
LOS B: Generally stable traffic flow conditions.
LOS C: Occasional back-ups may develop, but delay to vehicles is short term and still tolerable.
LOS D: During short periods of the peak hour, delays to approaching vehicles may be substantial but are tolerable during times of less demand (i.e. vehicles delayed one cycle or less at signal).
LOS E: Intersections operate at or near capacity, with long queues developing on all approaches and long delays.
LOS F: Jammed conditions on all approaches with excessively long delays and vehicles unable to move at times.
2 When demand volume exceeds the capacity of the lane, extreme delays will be encountered with queuing which may cause severe congestion affecting other traffic movements in the intersection.

## 3. TRIP GENERATION

Trip generation calculations were performed using trip generation data contained in the Institute of Transportation Engineers' (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition (2021) for Land Use Code (LUC) 210, Single-Family Detached Housing. The City of Marysville requires the use of a trip generation rate of 1.0 PM peak-hour trips per unit. There are 29 single-family units proposed to be constructed with 1 existing single-family unit being removed the development will therefore result in 28 new single-family units. The trip generation of the Colvin Development is summarized in Table 2.

Table 2: Trip Generation Summary

|  | Average Daily Trips |  |  | AM Peak-Hour Trips |  |  | PM Peak-Hour Trips |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Residential Units | Inbound | Outbound | Total | Inbound | Outbound | Total | Inbound | Outbound | Total |
| Generation Rate | 9.43 trips per unit |  |  | 0.70 trips per unit |  |  | 1.00 trips per unit |  |  |
| Splits | 50\% | 50\% | 100\% | 26\% | 74\% | 100\% | 63\% | 37\% | 100\% |
| Trips | 132.02 | 132.02 | 264.04 | 5.10 | 14.50 | 19.60 | 17,64 | 10.36 | 28.00 |

The Colvin Development is anticipated to generate approximately 264 new average daily trips with approximately 20 AM peak-hour trips and 28 PM peak-hour trips.

## 4. TRIP DISTRIBUTION

The trip distribution for the proposed Colvin Development is based on distributions provided by the City of Marysville for the Whiskey Ridge North area. It is anticipated that $38 \%$ of the trips generated by the development will travel to and from the north along $83^{\text {rd }}$ Avenue NE. Approximately $27 \%$ of the trips generated by the development will travel to and from the west along $44^{\text {th }}$ Street NE. It is estimated that $28 \%$ of the trips generated by the development will travel to and from the south, four percent along $83^{\text {rd }}$ Avenue NE, five percent along $87^{\text {th }}$ Avenue NE, and nineteen percent along SR-9. The remaining 7\% of the trips generated by the development are anticipated to travel to and from the east along SR-92. No significant changes in the development trip distribution are expected to occur in the horizon year distribution. The only change will be a portion of the trips utilizing the future connection of SR-9 at SR-92 intersection.

Separate trip distributions for the 2024 opening year and 2030 horizon year have been prepared for the AM and PM peak-hours. The AM and PM peak-hour 2024 opening year trip distributions are shown in Figure 2 and Figure 3, respectively. The AM and PM peak-hour 2030 horizon year distributions are shown in Figure 4 and Figure 5, respectively.





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The interlocal agreement between the City of Marysville and Snohomish County requires detailed development trip turning movement data at Snohomish County Key Intersections impacted with three or more directional trips on any approach or departure. There are not any Snohomish County Key Intersections within Snohomish County Transportation Service Area A (TSA A) that will be impacted by 3 directional peak-hour trips generated by the Colvin Development.

## 5. INTERSECTION LEVEL OF SERVICE ANALYSIS

The City of Marysville typically Traffic Impact Analysis Guidelines typically require intersections impacted with 25 peak-hour trips to be analyzed for the PM peak hour. The only intersections that will be impacted by 25 PM peak-hour trips generated by the Colvin Development are the intersection of E Sunnyside School Road at Densmore Road and the site access to $87^{\text {th }}$ Avenue NE. The intersection of E Sunnyside School Road at Densmore Road has been analyzed for the existing, 2024 opening year, and 2030 horizon year conditions. The site access to Densmore Road has not been analyzed since there are currently only 6 PM peak-hour trips currently utilizing Densmore Road south of E Sunnyside Road.

### 5.1 Turning Movement Calculations

The existing turning movements for the intersection of E Sunnyside Road at Densmore Road were collected by the independent count firm Traffic Data Gathering (TDG) in November 2021. The 2024 baseline and 2030 baseline turning movements have been calculated by applying a $3 \%$ annually compounding growth rate. The 2024 opening year and 2030 horizon year turning movements have been calculated by adding the trips generated by the Colvin Development to the 2024 baseline and 2030 baseline turning movements. The turning movements are shown in the following figures:

- Figure 6: Existing Turning Movements
- Figure 7: 2024 Baseline Turning Movements
- Figure 8: 2024 Opening Year Turning Movements
- Figure 9: 2030 Baseline Turning Movements
- Figure 10: 2030 Horizon Year Turning Movements

The existing count data and turning movement calculations are included in the attachments.






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### 5.2 Level of Service

The level of service calculations have been performed for the intersection of E Sunnyside School Road at Densmore Road using the existing stop-control on Densmore Road. The intersection is anticipated to operate at LOS B under the existing, 2024 opening year, and 2030 horizon year conditions. The site access to Densmore Road is anticipated to operate at LOS A due to the limited volume on Densmore Road. The level of service calculations are included in the attachments.

## 6. TRAFFIC MITIGATION FEES

The City of Marysville has an interlocal agreement with the City of Lake Stevens for impacts to the intersection of Soper Hill Road at $87^{\text {th }}$ Avenue NE. The City of Marysville also has an interlocal agreement with Snohomish County that provides for the payment of traffic mitigation fees to Snohomish County for City of Marysville developments. The City of Marysville has an understanding with WSDOT for the payment of traffic mitigation fees.

### 6.1 City of Marysville

The City of Marysville standard traffic mitigation fees have been calculated using the residential rate of $\$ 6,300$ per unit. The Colvin Development is proposed to include 28 net new units, which results in a total standard traffic mitigation fee of $\$ 176,400.00$.

### 6.2 City of Lake Stevens

The City of Marysville and the City of Lake Stevens have an interlocal agreement to fund improvements to Soper Hill Road from SR-9 to $83{ }^{\text {rd }}$ Avenue NE. The City of Marysville Whiskey Ridge North trip distribution shows trips travelling to and from the south on SR-9 would use E Sunnyside School Road. The intersection of Soper Hill Road at $87^{\text {th }}$ Avenue NE is therefore not anticipated to be impacted by any trips generated by the Colvin Development. Payment of traffic mitigation fees identified as part of the interlocal agreement with the City of Lake Stevens should therefore not be a condition of the Colvin Development.

### 6.3 Snohomish County

The City of Marysville and Snohomish County have an interlocal agreement that provides for the payment of traffic mitigation for impacts to Snohomish County roadways by developments located in the City of Marysville. Traffic mitigation fees are based on predetermined area impacts or impacts to actual improvement projects. According to Section 3(a)2 of the Snohomish County Traffic Worksheet and Traffic Study Requirements for Developments in the City of Marysville, traffic mitigation fees for development in the City of Marysville are only required if Snohomish County improvements in the Transportation Needs Report are impacted with three directional peak-hour trips. The trip distribution shows that there are not any Snohomish County improvement projects in the Transportation Needs Report impacted by 3 directional PM peak-hour trips generated by the Colvin Development. Snohomish County traffic mitigation fees should therefore not be a condition of the Colvin Development.

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### 6.4 Washington State Department of Transportation

WSDOT traffic mitigation fees are typically required for the City of Marysville developments if improvement projects identify on WSDOT's Exhibit C list are impacted by 3 directional PM peakhour trips and if the improvement project has not already been completed or advertised for construction bid. There are not any WSDOT improvement projects on the Exhibit C list that will be impacted by 3 or more directional PM peak-hour trips generated by the Colvin Development. WSDOT traffic mitigation fees should therefore not be a condition of the Colvin Development.

## 7. CONCLUSIONS

The Colvin Development is proposed to consist of 29 single-family detached units. There is one existing unit on the site that will be removed and is creditable to the development. The 28 new units of the Colvin Development are anticipated to generate approximately 264 new average weekday daily trips with approximately 20 new AM peak-hour trips and 28 new PM peak-hour trips. The intersection of E Sunnyside School Road at Densmore Road is anticipated to operate at LOS B under the 2024 opening year and 2030 horizon year conditions. The City of Marysville traffic impact fees should be $\$ 176,400.00$. Traffic mitigation fees according to the City of Lake Stevens, Snohomish County or WSDOT interlocal agreements should not be conditions of the Colvin Development.

## Count Data and Turning Movement Calculations



PHF = Peak Hour Factor
HV = Heavy Vehicles

## TURNING MOVEMENTS DIAGRAM

PEAK HOUR SUMMARY
(1) Traffic data gathering



## Level of Service Calculations



| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 118 | 0 | 286 | 116 |
| $\quad$ Stage 1 | - | - | - | - | 116 | - |
| Stage 2 | - | - | - | - | 170 | - |
| Critical Hdwy | - | - | 4.22 | - | 6.52 | 6.32 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.52 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.52 | - |
| Follow-up Hdwy | - | -2.308 | -3.608 | 3.408 |  |  |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 684 | 910 |
| $\quad$ Stage 1 | - | - | - | - | 885 | - |
| Stage 2 | - | - | - | - | 836 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1410 | - | 683 | 910 |
| Mov Cap-2 Maneuver | - | - | - | - | 683 | - |
| Stage 1 | - | - | - | - | 885 | - |
| Stage 2 | - | - | - | - | 835 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 9.6 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 780 | - | -1410 | - |  |
| HCM Lane V/C Ratio | 0.003 | - | -0.001 | - |  |
| HCM Control Delay (s) | 9.6 | - | -7.6 | 0 |  |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | Kr |  |
| Traffic Vol, veh/h | 97 | 3 | 1 | 143 | 1 | 1 |
| Future Vol, veh/h | 97 | 3 | 1 | 143 | 1 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 12 | 12 | 12 | 12 | 12 | 12 |
| Mvmt Flow | 124 | 4 | 1 | 183 | 1 | 1 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 128 | 0 | 311 | 126 |  |
| $\quad$ Stage 1 | - | - | - | - | 126 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 185 | - |  |
| Critical Hdwy | - | - | 4.22 | - | 6.52 | 6.32 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.52 | - |  |
| Follow-up Hdwy | - | -2.308 | - | 3.608 | 3.408 |  |  |
| Pot Cap-1 Maneuver | - | - | 1398 | - | 661 | 898 |  |
| $\quad$ Stage 1 | - | - | - | - | 876 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 823 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1398 | - | 660 | 898 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 660 | - |  |
| Stage 1 | - | - | - | - | 876 | - |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 9.7 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 761 | - | - | 1398 | - |
| HCM Lane V/C Ratio | 0.003 | - | -0.001 | - |  |
| HCM Control Delay (s) | 9.7 | - | - | 7.6 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | MF |  |
| Traffic Vol, veh/h | 97 | 16 | 6 | 143 | 8 | 4 |
| Future Vol, veh/h | 97 | 16 | 6 | 143 | 8 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 12 | 12 | 12 | 12 | 12 | 12 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 145 | 0 | 334 | 135 |  |
| $\quad$ Stage 1 | - | - | - | - | 135 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 199 | - |  |
| Critical Hdwy | - | - | 4.22 | - | 6.52 | 6.32 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.52 | - |  |
| Follow-up Hdwy | - | -2.308 | - | 3.608 | 3.408 |  |  |
| Pot Cap-1 Maneuver | - | - | 1378 | - | 641 | 888 |  |
| $\quad$ Stage 1 | - | - | - | - | 867 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 811 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1378 | - | 637 | 888 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 637 | - |  |
| Stage 1 | - | - | - | - | 867 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.3 | 10.2 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 703 | - | - | 1378 | - |
| HCM Lane V/C Ratio | 0.022 | - | -0.006 | - |  |
| HCM Control Delay (s) | 10.2 | - | - | 7.6 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | Kr |  |
| Traffic Vol, veh/h | 116 | 4 | 1 | 171 | 1 | 1 |
| Future Vol, veh/h | 116 | 4 | 1 | 171 | 1 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 12 | 12 | 12 | 12 | 12 | 12 |
| Mvmt Flow | 149 | 5 | 1 | 219 | 1 | 1 |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 154 | 0 | 373 | 152 |
| $\quad$ Stage 1 | - | - | - | - | 152 | - |
| Stage 2 | - | - | - | - | 221 | - |
| Critical Hdwy | - | - | 4.22 | - | 6.52 | 6.32 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.52 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.52 | - |
| Follow-up Hdwy | - | -2.308 | -3.608 | 3.408 |  |  |
| Pot Cap-1 Maneuver | - | - | 1368 | - | 609 | 869 |
| Stage 1 | - | - | - | - | 852 | - |
| Stage 2 | - | - | - | - | 793 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1368 | - | 608 | 869 |
| Mov Cap-2 Maneuver | - | - | - | - | 608 | - |
| Stage 1 | - | - | - | - | 852 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 10.1 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 715 | - | - | 1368 | - |
| HCM Lane V/C Ratio | 0.004 | - | -0.001 | - |  |
| HCM Control Delay (s) | 10.1 | - | - | 7.6 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\mathbf{\uparrow}$ | Ki |  |
| Traffic Vol, veh/h | 116 | 16 | 1 | 171 | 8 | 1 |
| Future Vol, veh/h | 116 | 16 | 1 | 171 | 8 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 12 | 12 | 12 | 12 | 12 | 12 |
| Mvmt Flow | 149 | 21 | 1 | 219 | 10 | 1 |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 170 | 0 | 381 | 160 |
| $\quad$ Stage 1 | - | - | - | - | 160 | - |
| Stage 2 | - | - | - | - | 221 | - |
| Critical Hdwy | - | - | 4.22 | - | 6.52 | 6.32 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.52 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.52 | - |
| Follow-up Hdwy | - | -2.308 | -3.608 | 3.408 |  |  |
| Pot Cap-1 Maneuver | - | - | 1349 | - | 602 | 860 |
| Stage 1 | - | - | - | - | 845 | - |
| Stage 2 | - | - | - | - | 793 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1349 | - | 601 | 860 |
| Mov Cap-2 Maneuver | - | - | - | - | 601 | - |
| Stage 1 | - | - | - | - | 845 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 10.9 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 622 | - | - | 1349 | - |
| HCM Lane V/C Ratio | 0.019 | - | -0.001 | - |  |
| HCM Control Delay (s) | 10.9 | - | - | 7.7 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0 | - |

## WSDOT Exhibit C List

EXHIBIT "C" 2009

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LIST OF PROGRAMED AINOO HSIWOHONS


