# LAND TECHNOLOGIES, INC. PLANNING • PERMITTING • ENGINEERING



Smokey Point Investments LLC

14XXX Smokey Pt Blvd, Marysville, WA 98271

PN SPA

SEPA SPA: October 2021

# Stormwater Site Plan Report for Undi Commerce Park



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# Contents

Contents
Section 1 – Report Summary 1
1.1 Project Description 1
1.2 Project Data Summary 2
Section 2 - Minimum Requirements1-1
2.1 Assessment of Minimum Requirements and Thresholds1-1
2.2 MR #1: Preparation of Stormwater Site Plans1-2
2.3 MR #2: Stormwater Pollution Prevention Plans (SWPPPs)
2.4 MR #3: Source Control of Pollution1-6
2.5 MR #4: Preservation of Natural Drainage Systems and Outfalls
2.6 MR #5: On-Site Stormwater Management1-8
2.7 MR #6: Runoff Treatment1-9
2.8 MR #7: Flow Control
2.9 MR #8: Wetlands Protection1-11
2.10 MR # 9: Operation and Maintenance1-12
Section 3 - Maps & Figures
Section 4 - Support Data
4.1 Soils Data 4-1
Section 5 Works Cited
Section 6 - Continuous Simulation Modeling6-1
6.1 Continuous Simulation Background6-1
6.2 Modeling Methodology6-1
Section 7 - Software Output

# Figures

Figure 1 - Vicinity Map	.3-1
Figure 2 - Existing Conditions (not to scale)	. 3-2
Figure 3 – Downstream Flow Path	. 3-3
Figure 4 - Site Plan	.3-4
Figure 5 – Soil Map (Not to Scale)	. 3-5

# Tables

Table 1 - Project Parcel Summary	2
Table 2 - Project Area Analysis & Activities Summary	2

### Acronyms

The following acronyms and abbreviations may or may not be called out within the body of this report.

0	ASTM	- American Society for Testing and Materials
0	BMPs	- Best Management Practices
0	СВ	- Catch Basin
0	CAO	- Critical Areas Ordinance
0	CESCL	- Certified Erosion and Sediment Control Lead
0	DOE	- Department of Ecology
0	EDDS	<ul> <li>Engineering Design &amp; Development Standards</li> </ul>
0	FEMA	- Federal Emergency Management Agency
0	HSPF	<ul> <li>Hydrological Simulation Program—Fortran</li> </ul>
0	Lidar	- Light Detecting And Ranging
0	LDA	- Land disturbing activity
0	LID	- Low Impact Development
0	LID Manual	- DOE 2005 LID Technical Guidance Manual for Puget Sound
0	MRs MS4	- Minimum Requirements (for Stormwater Management)
0	MS4 MSL	- Municipal Separate Storm Sewer System - Mean Sea Level
0	NAVD88	- North American Vertical Datum of 1888
0	NGVD29	- National Geodetic Vertical Datum of 1929
0	NPDES	- National Pollutant Discharge Elimination System
0	NRCS	- Natural Resources Conservation Service
0	NPGIS	- Non-Pollutant Generating Impervious Surface
0	O&M	- Operations and Maintenance
0	PGIS	- Pollutant Generating Impervious Surface
0	PGPS	- Pollutant Generating Pervious Surface
0	PLSS	- Public Land Survey System
0	POC	- Point of Compliance
0	RCW	- Revised Code of Washington
0	ROW	- Right-of-Way
0	SCDM-2010	- Snohomish County 2010 Drainage Manual
0	SMMWW	- DOE 2005 Stormwater Management Manual for Western Washington
0	SWPPP	- Stormwater Pollution Prevention Plan
0	TDA	- Threshold Discharge Area
0	TESC	- Temporary Erosion and Sediment Controls
0		- United States Department of Agriculture
0	US EPA WSDOT	<ul> <li>United States Environmental Protection Agency</li> <li>Washington State Department of Transportation</li> </ul>
0	WWHM	- Western Washington Hydrology Model
0		

# Section 1 – Report Summary

# **1.1 Project Description**

Smokey Point Investments LLC is planning for the future development of 47.95-*acres* of land in north Marysville, WA alongside Smokey Point Boulevard. The proposed development will be a Commerce Park which will house several large buildings. A SEPA plan approval is pursued for the future development of the commerce park in part or whole.

Stormwater Management for the anticipated full build out of the site will rely on full infiltration. Stormwater is divided amongst the site based on NPGHS and PGHS. All NPGHS is infiltrated within a rock infiltration chamber. All PGHS is distributed within a bioretention cell/swale that is comprised of 1.5-*feet* of bioretention soil media. The bioretention soil media is placed on top of an expanded rock infiltration bed that exceeds the footprint of the bioretention cell. This expansive rock infiltration bed is modeled independently in the WWHM to account for the larger surface area interface provided by the rock blanket dimensions.

Buildings within the bulk of the site may be equipped with loading docks. The three proposed buildings along the northern panhandle extending to 152<sup>nd</sup> St will be at grade with overhead doors.

Groundwater monitoring is currently underway for the 2021-22 Wet Season to establish a precise groundwater elevation and trend. Due to the potential likelihood of shallow groundwater at the site and significant size of land, stormwater is proposed to be pumped from the loading dock zones to adjacent surface bioretention swales for treatment. Loading dock zones are less than 4-ft from the final grade of building elevation. Extensive fill would be required to provide gravity flow from these elements. It is anticipated that stormwater generated from buildings and passenger vehicle parking areas will sheet flow to adjacent stormwater facilities.

The enhanced treatment afforded by the bioretention swales will provide a multitude of uses for future tenants provided adequate pre-treatment is maintained.

The parcel is currently vacant and vegetated with pasture type grasses. No known critical areas occur onsite or directly offsite. An unregulated ditch extends through the project site.

The site will be accessed along Smokey Point Boulevard at each parcel's frontage location. The northern panhandle portion of the site will be accessed via 152<sup>nd</sup> St NE. At full buildout the parcels will be connected through a drive aisle. However, each parcel requires its own independent access and fire lane so each parcel may be a standalone project based on timing and phasing.

The 2014 DOE Stormwater Management Manual for Western Washington will be adhered to for stormwater management. Stormwater management will rely on infiltration of treated stormwater.

Extensive groundwater monitoring and geologic studies have occurred in the past for adjacent properties. Some geotechnical work has already been conducted and more is planned.

Per NRCS mappings, type "C/D" Norma and Custer fine sandy loam soils are found throughout the site. The site lies within Recessional Outwash soils of the Marysville Sand member. These sands begin at depth and are clean and extensive.

## **1.2 Project Data Summary**

Existing and proposed project areas are presented for determination of stormwater management requirements based on prescribed thresholds as outlined in the Marysville Municipal Code (MMC 22C) and the 2014 SMMWW Vol-1, Ch-2, Section 2.4 are summarized in the following tables.

Project Data:	
Applicant	Smokey Point Investments
Site Owner	Smokey Point Investments LLC
Project Name	Undi Commerce Park
Project T.S.R. Location	Twn 31 N, Rng 5 E, Sec 33, Qtr-W
Project Address	14XXX Smokey Pt Blvd, Marysville, WA 98271
Parcel ID(s)	3105330030-2500,-1900,-0300,-1000,-2200,-3100,- 2600,-2300,-2700,-0900,-0500,-3000,-1100,-1200
Watershed	Snohomish
Basin	Quilceda Creek
Sub-Basin	Hayho Creek
WRIA Number	7
Analysis Standard	2014 DOE SMMWW

### **Table 1 - Project Parcel Summary**

 Table 2 - Project Area Analysis & Activities Summary

Existing Conditions:		
Total Site Area	2,088,697	sf (47.95 ac)
Existing Impervious Area	0	sf (0.00 ac) 0%
Proposed Activity:		
Proposed Activity	LI – Commerc	e Park
Total Proposed Disturbance Area	2,088,697	sf (47.95 ac)
Proposed Grading Area	2,088,697	sf (47.95 ac)
Proposed New NPGIS (roof)	815,484	sf (18.7 ac)
Proposed New PGIS (Road and Driveway/Parking)	959,908	sf (22.0 ac)
Proposed Replaced Impervious Area	0	sf (0.00 ac)
Native Vegetation convert to Lawn	0	sf (0.00 ac)
Native Vegetation convert to Pasture	0	sf (0.00 ac)
Total New Impervious Area	1,775,392 sf	sf (40.7 ac)
Total Site Impervious Area (new+exist)	1,775,392 sf	sf (40.7 ac)
Grading is ≤ 2 feet from P/L	No	-
Any excavation 4+' at <1:1 slope to P/L	No	
Fill Slopes 4+' and >33% slope	No	

# **Section 2 - Minimum Requirements**

### 2.1 Assessment of Minimum Requirements and Thresholds

Minimum requirements and thresholds are established by City of Marysville Municipal Code 14.15.050 – Minimum Requirements. Minimum Requirements for new development and Redevelopment are based on a development's disturbance area. Existing and proposed project areas for determination of stormwater management requirements are presented in Table 2.

The existing impervious area is less than 35% so this project qualifies as 'new development'. The proposed condition of the fully developed site will have impervious area in excess of 5,000 sf. This requires construction activities and stormwater management to comply with Minimum Requirements 1 through 9. A full construction SWPPP is also required.

Minimum Requirements per SMMWW:

MR-1: Prepare Stormwater Site Plan. MMC 14.15.050 (1)

MR-2: Stormwater Pollution Prevention Plan (SWPPP). MMC 14.15.050 (2)

MR-3: Water pollution source control for new development. MMC 14.15.050 (3)

MR-4: Preservation of natural drainage systems and outfalls. MMC 14.15.050 (4)

MR-5: On-site stormwater management. MMC 14.15.050 (5)

MR-6: Runoff treatment. MMC 14.15.050 (6)

MR-7: Flow control requirements. MMC 14.15.050 (7)

MR-8: Detention or treatment in wetlands and wetland buffers. MMC 14.15.050 (8)

MR-9: Inspection, operation and maintenance requirements. MMC 14.15.050 (9)

Each Minimum Requirements is described in the following sections. There are no additional requirements to be met.

# 2.2 MR #1: Preparation of Stormwater Site Plans

This document is the Stormwater Site Plan Report that addresses the requirements of MR-1. This section presents the portion of the Stormwater Site Plan that includes recommendations, calculations, and procedures required to adhere to Minimum Requirement #1. The evaluation of the existing site conditions follows.

### 2.2.1 Site Location

The site is located in the West half of Section 33 of Township 31 North, Range 5 East. The street address is 14XXX Smokey Pt Blvd, Marysville, WA 98271 and the parcels are located on the south side of 152<sup>nd</sup> St NE and East along Smokey Point Boulevard. See Figure 1 for a vicinity map.

### 2.2.2 Site Description, Existing Conditions

The project site is 47.95-*acres*. The parcels are owned by Smokey Point Investments LLC. The Snohomish County parcel number are 3105330030-2500,-1900,-0300,-1000,-2200,-3100,-2600,-2300,-2700,-0900,-0500,-3000,-1100,-1200. It is zoned Light Industrial and is located in Snohomish County.

The parcel is vacant. The existing drainage system(s) are undetermined but largely surface runoff over the top silt layer and some infiltration. One parcel group recently had an early grade permit with a detention pond installed. Site investigation reveals that not much stormwater can reach this pond based on grade.

All maps and figures are presented in the Support Data section of this document.

A vicinity map that shows the site location is shown as Figure 1.

A site map that shows the property lines is shown in Figure 2.

A topographic map that shows the site boundaries, study area boundaries, and the downstream flow-paths is also presented in Figure 3.

### 2.2.3 Existing Basin Analysis

The project is defined by the development within the subject parcels. Existing project flow paths are shown in Figure 2.

The study area is located in the Hayho Creek sub-basin of the Quilceda Creek Basin in the Snohomish watershed (WRIA-7), which drains to the Puget Sound.

All existing flow assessment and site related basin delineations were established by tracing analysis of a LIDAR surface model.

### 2.2.4 Other Information on the Study Area

The site is not in or adjacent to a USEPA Sole Source Aquifer.

The site is not in a well-head protection area.

The site is not in a floodway or floodplain.

### 2.2.5 Critical Areas

No recent Critical Area Report or Study has been conducted. No wetlands were observed after a site visit in October 2021. No wetlands are mapped or recorded within the City's GIS repository. An unregulated ditch flows through the site but is not considered a critical area.

### 2.2.6 Topography

The site and surrounding topography is analyzed using survey topographic points provided by the Puget Sound Lidar Consortium. A 3D surface model was generated and augmented with on-site survey topographic provided by Innova Architects.

The site has mostly flat slopes with a high point around 108 feet MSL in the northwest corner of the site.

Slopes average in the range of 0 to 2 percent for the majority of the developable area. The site has an average slope of 0.5%.

### 2.2.7 Soils

Per NRCS mappings, type "C/D" Norma and Custer fine sandy loam soils are found throughout the site. The site lies within Recessional Outwash soils of the Marysville Sand member. These sands begin at depth and are clean and extensive.

Norma loam soils have a 0-10 *inch* first layer of fine ashy loam with the remaining profile being sandy loam. Custer fine sandy loam soils have 0 to 9 inch first layer of fine sandy loam with the remaining profile being sand.

Detailed physical and chemical properties of these soils are presented in Section 4.1. The NRCS mapping can be seen in Figure 5.

Onsite geotechnical work and soils exploration by Zipper Geotech's is underway. An updated Geotech report was issued in August of 2021. Preliminary groundwater elevations of 3 to 4-ft BPG are reported and a preliminary infiltration rate of 2-*in/hr* is stated. Stormwater design relies on this stunted 2-*in/hr* rate. Stormwater management will be preliminarily designed with these values. Groundwater elevation is conservatively shallower within the preliminary concept project drawings.

### 2.2.8 Field Inspection

The site was visited in October 2021, a clear and dry Sunday. All site evaluation conducted per remote sensing

### 2.2.9 Upstream Analysis

A relative high point of 110 *feet* MSL is located offsite directly northwest of the site. The upstream area to the site is directly to the north- northwest of the site on the adjoining parcel and north of 152<sup>nd</sup> St NE. This upstream area drains to the unregulated ditch. The unregulated ditch is conveyed through the site in an existing 36-inch diameter CMP Culvert to the unregulated ditch along the eastern property boundary.

### 2.2.10 Downstream Analysis

The downstream area was established by tracing analysis of a LIDAR surface model and evaluation of various GIS data, aerial imagery, and City of Marysville Drainage Inventory. The development area flows to the east property boundary line and flows south in the unregulated ditch. Stormwater then flows east at the southernmost property corner. This unregulated ditch flows east along the southernmost border of the Marysville Regional Stormwater pond where it joins with the Hayho Creek. Stormwater flows along Hayho Creek to the crossing of 136<sup>th</sup> St NE. Hayho Creek crosses beneath 136<sup>th</sup> St NE within a 48 *inch* diameter culvert. Hayho Creek travels south before reaching the Quilceda Creek. Quilceda Creek drains to the Puget Sound.

Stormwater generated from the project site is to be infiltrated. (Stormwater will be treated prior to discharge).

Figure 3 shows a portion of the downstream flow path.

# 2.3 MR #2: Stormwater Pollution Prevention Plans (SWPPPs)

MMC 14.15.050 (2) specifies the requirements for development and redevelopment projects to be responsible for preventing erosion and discharge of sediment and other pollutants into receiving waters. Volume I, Chapter 2.5.2 of the 2014 SMMWW specifies that all new development and redevelopment implement a Stormwater Pollution Prevention Plans (SWPPP), which is a list of 13 elements that present measures and methods for all permanent and temporary erosion and sediment control (TESC), pollution prevention, inspection/monitoring activities, and recordkeeping required during the proposed construction project.

Based on the MR#2 thresholds, this project generates more than 2,000 *square feet* of impervious area, so a full SWPPP is required. Required elements for the SWPPP:

- SWPPP element 1: Preserve vegetation/mark clearing limits
- SWPPP element 2: Establish construction access
- SWPPP element 3: Control flow rates
- SWPPP element 4: Install sediment controls
- SWPPP element 5: Stabilize soils
- SWPPP Element 6: Protect slopes
- SWPPP element 7: Protect permanent drain inlets
- SWPPP element 8: Stabilize channels and outlets
- SWPPP element 9: Control pollutants
- SWWP element 10: Control dewatering
- SWPPP element 11: Maintain best management practices
- SWPPP element 12: Manage the project
- SWPPP element 13: Protect On-Site Stormwater Management BMPs for Runoff from Roofs and Other Hard Surfaces

The SWPPP is assembled as a separate document for portability and reproduction purposes. The document is titled "**Stormwater Pollution Prevention Plan for Undi Commerce Park**", dated 21 October 2021. This document will be provided with Construction Plan Submittal.

# 2.4 MR #3: Source Control of Pollution

MMC 14.15.050 (3) specifies the requirements for water pollution source control for new development or redevelopment activities in accordance with Volume IV of the SMMWW. These activities are primarily commercial industrial developments that represent significant pollutant generation potential and the associated source control BMPs are designed to suit those activities.

Per Chapter 2.5.3, MR#3 does not apply to the intended future use of this industrial development. Hence such source controls are not specified for this project. Project specific controls may be required for specific proposals. The site is designed to accommodate these source controls for specific tenants as required.

# 2.5 MR #4: Preservation of Natural Drainage Systems and Outfalls

MMC 14.15.050 (4) specifies the requirements for preservation of natural drainage systems or outfalls for all new development and redevelopment activities under Minimum Requirement 4 in the 2014 SMMWW.

Natural drainage patterns as they once existed shall be retained. Existing conditions experience a sheet drainage pattern to the site's east property boundary. Stormwater generated onsite reaches the property boundary through surface runoff during only extreme storm events (exceeding 100-year storm). Stormwater is infiltrated onsite.

## 2.6 MR #5: On-Site Stormwater Management

MMC 14.15.050 (5) specifies requirements for implementing on-site stormwater BMPs. This requirement mandates that on-site stormwater runoff be infiltrated, dispersed, and/or retained to the maximum extent feasible without causing flooding or erosion impacts. Projects triggering Minimum Requirements 1 through 5 must use On-site stormwater management BMPs from List #1 for all surfaces or demonstrate compliance with the LID Performance Standard. Projects triggering Minimum Requirements 1 through 9 must meet the requirements of Table 2.5.1 in Vol. 1 of the 2014 SMMWW. Table 2.5.1 specifies the requirements for new or redevelopment depending on UGA and parcel size to meet the requirements of the LID Performance Standard and/or List #2. List #1 and List #2 specify stormwater BMPs in order of preference. The first BMP determined feasible is required.

<u>This project triggers MR's 1-9.</u> This project is within the City's UGA. This project is required to adhere to the LID Performance Standard or List #2 per Table 2.5.1.

List #1 and #2 contain appropriate BMPs to mitigate a particular developed surface. The surfaces included in the list are Lawn and Landscaped Areas, Roofs, and other hard surfaces (road/driveway/parking).

Lawn/Landscape is required to utilize BMP T5.13, Post-Construction Soil Quality and Depth.

Roofs are required to employ BMP T5.30 Full Dispersion or Downspout Infiltration, Rain Gardens or Bioretention, BMP T5.10A Downspout Dispersion Systems, or perforated stubout connections. The first feasible BMP in this list must be used.

Other Hard surfaces (Roads, Driveways, Parking Lots, Etc.) must utilize BMP T5.30 Full Dispersion, BMP T5.15 Permeable Pavement, Bioretention, Sheet Flow Dispersion, or Concentrated Flow Dispersion. The first feasible BMP in this list must be used.

Lawn/landscape will utilize BMP T5.13, Post Construction Soil Quality and Depth.

Roofs and Driveways will not be able to provide BMP T5.30 Full Dispersion. Full Dispersion requires 100 *foot* flow paths within native areas. The project will not be able to maintain 65% open space.

Individual "Lot" Infiltration is feasible based on the permeability of native soils. Roofs will be routed to rock infiltration chambers for full infiltration.

BMP T5.10B Downspout Dispersion or Driveway Dispersion will not be utilized as each individual building site lacks the prescriptive flow path length through native vegetation.

Road and Driveway/Parking areas will be routed to Bioretention Cells, BMP T7.30. The bioretention cells will treat stormwater through filtering, phytoremediation, and microbial action from within the compost. The Bioretention Cells also perform enhanced treatment.

Bioretention cells will treat more than 99% of incoming stormwater generated from the PGIS (per MR #6). See Minimum Requirement #6.

Permeable pavement may not be used as due to the site use is a commercial/industrial activity defined by 40 CFR 122.26(b)(14).

A site plan showing the stormwater management and development can be seen in Figure 4.

# 2.7 MR #6: Runoff Treatment

Minimum Requirement #6 in MMC 14.15.050 (6) specifies the requirements for providing runoff treatment. The threshold for requiring a treatment BMP is 5,000 *square feet* of PGIS (Pollution Generating Impervious Surface) or a total of more than  $\frac{3}{4}$  of an acre of PGPS (Pollution Generating Pervious Surface).

This project is expected to generate 959,908 *square feet* (22.0 *acres*) of PGIS based on road, driveway, sidewalk, and parking areas, therefore treatment facility BMPs are required for this project.

Runoff treatment facility selection is outlined in Vol. I, Ch. 4.2, Step V of the 2014 SMMWW. Step V outlines the treatment facility selection flow chart based on the intended use of a project. Treatment selection is based on if the site is a high-use site, if the downstream receiving waters are phosphorous sensitive, and/or if the site is required to provide enhanced treatment. The definitions of high-use, phosphorous control, and enhanced treatment can be found in Step V in Section 4.2 of the 2014 SMMWW.

The project is not a high use site and infiltration is practicable for the site.

Enhanced and Basic treatment is provided through the use of a bioretention facility per Vol. III Section 3.3.12 of the 2014 SMMWW. The bioretention specified will provide enhanced treatment. The bio-cell treats stormwater through the percolation of stormwater through soils and their ability to absorb pollutants. See Vol III. Section 3.3.12 of the 2014 SMMWW for specific soil design criteria.

If the project is determined to be a high-use site in the future – oil control facilities may be required prior to discharge to the bioretention cell. These areas will primarily be located in the loading dock zones of the development and may be pumped from the oil control facility prior to the bioretention cells for final treatment and infiltration.

The bioretention cell mitigates polluted stormwater through physical, chemical and biological treatment processes. The treatment process will break down heavy metals that are not easily separated by physical means. Stormwater percolates through compost amended soils and plantings to obtain treatment. Stormwater flows through this part of the cell at a rate of 2.0 *inches/hour*. Infiltration is allowed to occur below the bio-cells. The total percolated runoff through the bio-cell's amended soils is well over the 91% total runoff volume treatment requirement. See Section 7.

# 2.8 MR #7: Flow Control

Minimum Requirement #7 in MMC 14.15.050 (7) specifies the requirements for runoff flow control. The threshold for requiring Minimum Requirement #7 is 5,000 square feet of impervious surface. Flow control shall be provided if the project creates more than 10,000 square feet of effective impervious area in a threshold discharge area, converts ¾ of an acre or more of native vegetation to lawn, 2.5 *acres* or more native vegetation is converted to pasture, or a combination of impervious and converted pervious surfaces cause a 0.1 *cfs* increase in the 100-*year* flow frequency from a continuous simulation runoff model.

The project exceeds this requirement and is required to provide flow control. Flow Control is provided by infiltration.

The project uses bioretention cells to detain and treat all incoming stormwater flow from PGIS. The bioretention cell marginally detains stormwater but provides 100% treatment of stormwater generated by PGIS. The bio-cells are comprised of 1.5 *feet* of amended soils. The bioretention cells discharge to a rock infiltration bed beneath. The rock infiltration bed has an expanded footprint beneath the cells to position the infiltrating blanket beneath pavement, sidewalk, and curb. The bio-cell utilizes a 0.5 *foot* ponded area with 0.5 *feet* of freeboard to allow stormwater to infiltrate through the amended soils and in to this rock infiltration chamber. The modeled bioretention cell element is connected at both Outlets 1 and 2 to the rock bed to precisely monitor all stormwater leaving the amended soils to the rock bed. The rock bed is receiving all stormwater flowing through the bioretention cell. The rock bed infiltrates to the native soils below. The modeling for this bioretention cell and expanded rock bed was required to be separate facilities due to the inequivalent width of both facilities and the required 'expanded' rock bed to premit 100% infiltration of stormwater.

Roofs will be directed to a separate rock infiltration chamber. Rock infiltration chambers are provided to mimic BMP T5.10A Full Infiltration but utilize the WWHM for size determination. The rock infiltration chamber is 1 *feet* thick and has an overall footprint of 6500-*ft* x 20-*ft* (130,000 *square feet*.)

See Section 7 for bio-cell and rooftop infiltration modeling parameters.

## 2.9 MR #8: Wetlands Protection

MMC 14.15.050 (8) specifies requirements for discharge of stormwater in wetlands and wetland buffers as well as discharge of stormwater to a stream.

Since there is no detention or treatment in critical areas, MR-8 does not apply to this project.

# 2.10 MR # 9: Operation and Maintenance

Minimum Requirement #9 specified in MMC 14.15.050 (9) contains requirements for inspection, operation and maintenance of stormwater facilities and BMPs. Specific maintenance standards and requirements are outlined in Volume V of the 2014 SMMWW. The 2014 SMMWW requires the regular maintenance and inspection of drainage facilities.

For portability and reproduction purposes, the Operations and Maintenance Manual is presented in a separate stand-alone document titled "**Operations and Maintenance Manual for Undi Commerce Park**", dated **21 October 2021.** This document will be provided with the construction plan submittal.



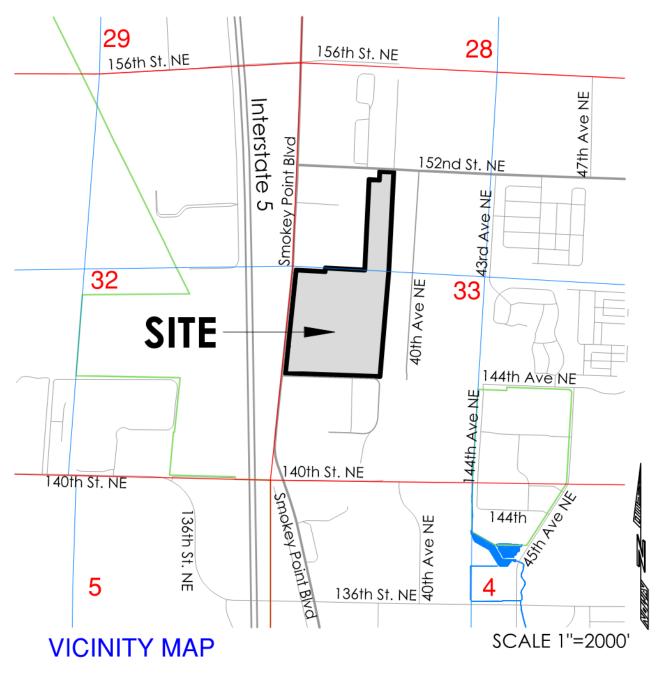


Figure 1 - Vicinity Map

3-3-1



Figure 2 - Existing Conditions (not to scale)

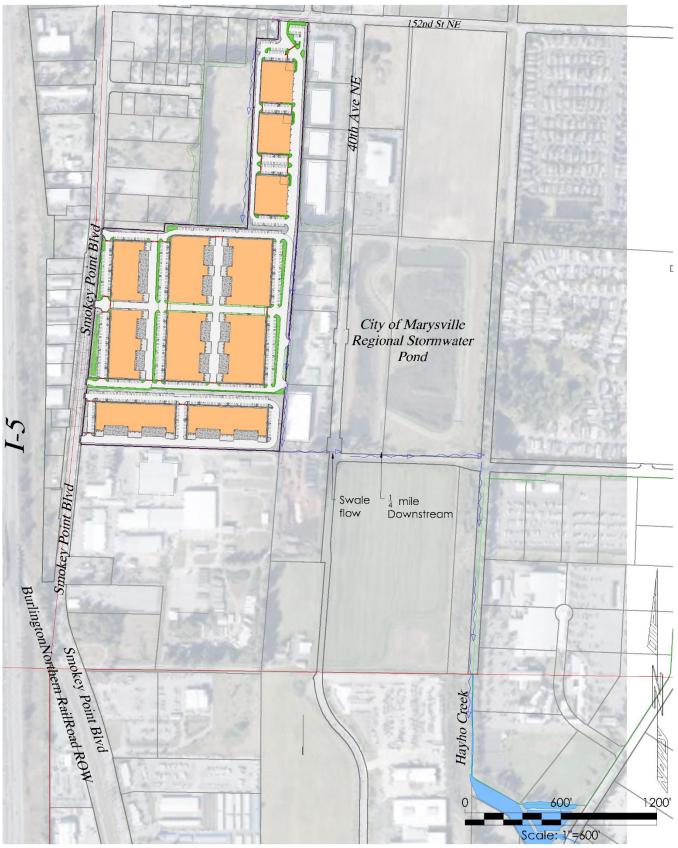


Figure 3 – Downstream Flow Path

3-3-3





Figure 5 – Soil Map (Not to Scale)

# Section 4 - Support Data

### 4.1 Soils Data

### 13—Custer fine sandy loam

#### Map Unit Setting

National map unit symbol: 2hy0

Elevation: 0 to 150 feet

Mean annual precipitation: 32 to 50 inches

Mean annual air temperature: 48 to 50 degrees F

Frost-free period: 150 to 200 days

Farmland classification: Prime farmland if irrigated and drained

### Map Unit Composition

Custer, undrained, and similar soils: 85 percent

*Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### Description of Custer, Undrained

### Setting

Landform: Outwash plains Parent material: Glacial outwash

### Typical profile

H1 - 0 to 9 inches: fine sandy loam

H2 - 9 to 35 inches: sand

### H3 - 35 to 60 inches: sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 20 to 40 inches to strongly contrasting textural stratification Natural drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None

Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water storage in profile: Low (about 3.1 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: C/D

Forage suitability group: Wet Soils (G002XN102WA)

Hydric soil rating: Yes

### **Minor Components**

### Norma, undrained

*Percent of map unit:* 5 percent *Landform:* Depressions *Hydric soil rating:* Yes

#### **Custer, drained**

Percent of map unit: 5 percent Landform: Depressions Hvdric soil rating: Yes Indianola Percent of map unit: 5 percent Hydric soil rating: No 39—Norma loam Map Unit Setting National map unit symbol: 2hyx Elevation: 0 to 1,000 feet Mean annual precipitation: 35 to 60 inches Mean annual air temperature: 48 to 52 degrees F Frost-free period: 150 to 200 days Farmland classification: Prime farmland if drained Map Unit Composition Norma, undrained, and similar soils: 85 percent *Minor components:* 15 percent Estimates are based on observations, descriptions, and transects of the mapunit. **Description of Norma, Undrained** Setting Landform: Depressions, drainageways Parent material: Alluvium Typical profile H1 - 0 to 10 inches: ashy loam H2 - 10 to 28 inches: sandy loam H3 - 28 to 60 inches: sandy loam **Properties and gualities** Slope: 0 to 3 percent Depth to restrictive feature: More than 80 inches Natural drainage class: Poorly drained Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr) Depth to water table: About 0 inches Frequency of flooding: None Frequency of ponding: Frequent Available water storage in profile: Moderate (about 9.0 inches) Interpretive groups Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: B/D Forage suitability group: Wet Soils (G002XN102WA) Hydric soil rating: Yes **Minor Components** Bellingham, undrained Percent of map unit: 5 percent Landform: Depressions

Hydric soil rating: Yes Norma, drained Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes Terric medisaprists, undrained Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes Custom Soil Resource Report

# **Section 5 Works Cited**

- Puget Sound Action Team. (2005, January). Low Impact Development Technical Guidance Manual for Puget Sound. *Publication No. PSAT 05-03*. Washington: Washington State University -Pierce County Extension.
- Puget Sound LIDAR Consortium. (2003, April). LIDAR Bare Earth DEM File. q47121h24be.e00. Snohomish County, Washington. Retrieved May 2013, from http://pugetsoundlidar.ess.washington.edu/index.htm
- Snohomish County Planning and Development Services. (2007, October 1). Aquifer Recharge/Wellhead Protection. Everett, WA.
- Snohomish County Surface Water Management Division. (2002, December). Snohomish UGA Drainage Needs Report. Everett, Washington.

# **Section 6 - Continuous Simulation Modeling**

### 6.1 Continuous Simulation Background

HSPF based continuous simulation modeling was used to evaluate the hydrologic performances of the pre-developed and developed sub-basins in order to accurately assess flow rates.

The currently adopted continuous simulation models use the HSPF (Hydraulic Simulation Program in FORTRAN) software engine. The HSPF model uses a robust and detail accounting of the 'water budget', including evaporation, evapotranspiration, interception, interflow, and groundwater. The modeling accounts for and assesses land segment areas that include vegetation or impervious cover, soil types, and slopes. The modeling also uses utilized over 50 years of continuous rainfall data (precipitation) and evaporation data for the area. The HSPF continuous modeling is considered the best available science for hydrologic analysis.

### 6.2 Modeling Methodology

HSPF modeling was managed via the Western Washington Hydrology Model (WWHM) interface program. The current professional version of WWHM by Clearcreek Solutions, Inc., WWHM-2012 was used. The current data precipitation and evaporation set provided by DOE with the WWHM-2012 software interface was used that includes quantized data in 15-minute time steps from October 1948 to October 2009. Projects within the WSDOT Data zones may also elect to use the WSDOT precipitation data that extends the time series to 1901 and extrapolates to 2058. The WSDOT precipitation data may be used.

The WWHM program comes packaged with generic, well considered HSPF modeling parameters. These settings allow for the modeling of the majority of the topological conditions found in the Puget Sound area. Where conditions fall reasonably outside the range of the default HSPF parameters, adjustments should be made to more accurately reflect those conditions. These is generally limited to the pervious land segments (IMPLNDS) and are mostly limited to slopes (SLSUR), infiltration rates (INFILT), and length of flow path (LSUR). For this project, HSPF parameters were not adjusted to reflect site conditions.

### **6.2.1 Existing Conditions**

The surface vegetative cover is assumed fully forested with an average slope of 1% in the area of development, based on the LIDAR based TIN analysis. The LIDAR model represents the pre-graded conditions and is in accordance with the predeveloped requirements to be represented as native vegetation and soils that existed at a site prior to the influence of Euro-American settlement.

The NRCS soil mapping of Custer within the modeled area is a <u>Type C/D</u> hydrologic soils by NRCS and DOE.

### 6.2.2 Developed Conditions

Default mapping for flat road was used for the road, driveway, and parking areas. These areas will be pumped or sheet flow to bioretention cells placed throughout the site.

The entire site is required fill to maintain separation between the high groundwater table. Fill beneath the facilities is required to have infiltration properties consistent with the native soils.

The bioretention cells discharge to a rock infiltration chamber beneath. The rock infiltration chamber has an expanded footprint beneath the cells to position the infiltrating blanket beneath pavement, sidewalk, and curb. The bio-cell utilizes a 0.5 *foot* ponded area with 0.5 *feet* of freeboard to allow stormwater to infiltrate through the amended soils and in to this rock infiltration chamber. The bioretention cell is connected at both WWHM outlets 1 and 2 to the rock bed. The rock bed is receiving all stormwater flowing through the bioretention cell. The rock bed infiltrates to the native soils below. The modeling for this bioretention cell and expanded rock bed is required to be separate facilities due to the inequivalent width of both facilities and the required 'expanded' rock bed to permit 100% infiltration of stormwater. This modeling method permits the accurate infiltration component to be calculated within the rock bed. The infiltration of the bioretention cell matches the rate of the BSM and is connected (outflows) to the rock bed. This is the Outlet 2 connection of the WWHM element.

It should be noted that when ponds, bio-swales, or other open detention facilities are used, the corresponding WWHM analysis module includes the ponded area. Consequently, this area is not included in the basin land segment mappings, so the total area is often different between the developed and pre-developed conditions. The bioretention cells provided account for 0.96 *acres* of surface area that is accounted for.

Per C.10.3 Modeling of Multiple Bioretention facilities of Volume III, of the 2014 DOE SMMWW, multiple bio-cell facilities, have similar characteristics, could represent as one large bio-cell facility serving the cumulative area tributary to those facilities. The bioretention areas will be specified at a ratio that is consistent with the entire site plan for the Commerce Park as development occurs.

The current DOE specification for amended soils in 2014 is labeled as 'SMMWW' in the Bio-Swale and other WWHM modules that employ amended soils. The parameters for modeling the SMMWW are preset and based on current state-of-the-art modeling using a combination of the Darcy's and Van Genuchten's equations to account for the variability of permeability and water content as the soils transition from dry or partly damp to saturated conditions as the bio-cell cycles through the process of filling, emptying, and drying out. The SMMWW settings based on the WSU amended soils.

The rooftop rock infiltration chambers are separately modeled and follow the multiple facilities as described above. In the future, specific construction plans for individual buildings and sites within the commerce park will likely have their own modeling and design constituents. The rooftop rock infiltration chambers are modeled based on cumulative area draining to each. Chambers will be parsed through the site at a ratio of rooftop draining to each.

The pasture representative in the model as bypass will likely drain to bioretention cells on the site or discharge to the native drainage pathways. These areas are distributed throughout the entire 50-*acre* parcel and not representative of any one single, or significant area.

# Section 7 - Software Output

The following WWHM reports in this section represent individual sub-basin analysis for hydrologic flow evaluations. The following heading is common to all reports.

### Western Washington Hydrology Model,

#### **PROJECT REPORT**

WWHM2012 PROJECT REPORT

Project Name: Undi Co Site Name: Undi Comme	ommorgo CEDA Dian	
Site Name: Undi Comme		
Site Address: Smky Pt		
City : Marysville		
<b>Report Date:</b> 10/20/20		
MGS Regoin : Puget Ea		
Data Start : 1901/10/	/1	
Data End : 2058/09/30	0	
DOT Data Number: 05		
Version Date: 2019/09	9/13	
<b>Version</b> : 4.2.17		
Low Flow Threshold fo	or POC 1 : 50 Percent of the 2 Year	
High Flow Threshold f	for POC 1: 50 year	
PREDEVELOPED LAND USE	E	
Name : Basin 1		
Bypass: No		
GroundWater: No		
Giodiana cei : 110		
Pervious Land Use	acre	
C, Forest, Flat	47.95	
Pervious Total	47.95	
Fervious iotai	47:55	
	acre	
Impervious Land Use		
Impervious Land Use		
	0	
Impervious Land Use Impervious Total		
Impervious Total	0	
Impervious Total	0	
Impervious Total Basin Total	0	
Impervious Total Basin Total Element Flows To:	0 47.95	

#### MITIGATED LAND USE

Name : Basin 1 Bypass: No GroundWater: No

acre 0
<u>acre</u> 22.03
22.03
22.03

Element Flows To:GroundwaterSurfaceInterflowGroundwaterSurface retention1Surface retention1

**Name** : Bioretention 1 Bottom Length: 7000.00 ft. Bottom Width: 3.00 ft. Material thickness of first layer: 1.5 Material type for first layer: SMMWW 12 in/hr Material thickness of second layer: 0 Material type for second layer: Sand Material thickness of third layer: 0 Material type for third layer: GRAVEL Infiltration On Infiltration rate: 12 Infiltration safety factor: 1 Total Volume Infiltrated (ac-ft.): 9581.809 Total Volume Through Riser (ac-ft.): 30.981 Total Volume Through Facility (ac-ft.): 9612.79 Percent Infiltrated: 99.68 Total Precip Applied to Facility: 228.001 Total Evap From Facility: 117.491 Underdrain not used Discharge Structure Riser Height: 0.5 ft. Riser Diameter: 12 in.

Element Flows To: Outlet 1 Outlet 2 Gravel Trench Bed 1 Gravel Trench Bed 1

Bioretention 1 Hydraulic Table					
Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs)	
0.0000	0.4821	0.000	0.0000	0.000	
0.0330	0.4821	0.0073	0.0000	0.0000	
0.0659	0.4821	0.0145	0.0000	0.0000	
0.0989	0.4821	0.0218	0.0000	0.0000	
0.1319	0.4821	0.0291	0.0000	0.0001	
0.1648	0.4821	0.0363	0.0000	0.0131	
0.1978	0.4821	0.0436	0.0000	0.0203	
0.2308	0.4821	0.0509	0.0000	0.0293	
0.2637	0.4821	0.0581	0.0000	0.0405	
0.2967	0.4821	0.0654	0.0000	0.0538	
0.3297	0.4821	0.0727	0.0000	0.0694	
0.3626	0.4821	0.0799	0.0000	0.0875	
0.3956	0.4821	0.0872	0.0000	0.1081	

0.46150.48210.10180.00000.15760.49450.48210.10900.00000.18650.52750.48210.11630.00000.21850.56040.48210.12360.00000.25350.59340.48210.13080.00000.2917	
0.52750.48210.11630.00000.21850.56040.48210.12360.00000.25350.59340.48210.13080.00000.2917	) }
0.56040.48210.12360.00000.25350.59340.48210.13080.00000.2917	)
0.5934 0.4821 0.1308 0.0000 0.2917	7 2 3 3
	) }
0 0000 0 1001 0 0000 0 0000	) 3 -
0.6264 0.4821 0.1381 0.0000 0.3332	3
0.6593 0.4821 0.1454 0.0000 0.3780	
0.6923 0.4821 0.1526 0.0000 0.4263	
0.7253 0.4821 0.1599 0.0000 0.4781	
0.7582 0.4821 0.1672 0.0000 0.5335	1
0.7912 0.4821 0.1744 0.0000 0.5926	;
0.8242 0.4821 0.1817 0.0000 0.6555	j
0.8571 0.4821 0.1890 0.0000 0.7222	
0.8901 0.4821 0.1962 0.0000 0.7928	;
0.9231 0.4821 0.2035 0.0000 0.8674	
0.9560 0.4821 0.2108 0.0000 0.9460	J
0.9890 0.4821 0.2180 0.0000 1.0288	;
1.0220 0.4821 0.2253 0.0000 1.1158	;
1.0549 0.4821 0.2326 0.0000 1.2071	
1.0879 0.4821 0.2398 0.0000 1.3026	;
1.1209 0.4821 0.2471 0.0000 1.4026	;
1.1538 0.4821 0.2544 0.0000 1.5070	)
1.1868 0.4821 0.2616 0.0000 1.6159	)
1.2198 0.4821 0.2689 0.0000 1.7293	5
1.2527 0.4821 0.2762 0.0000 1.8474	
1.2857 0.4821 0.2835 0.0000 1.9700	J
1.3187 0.4821 0.2907 0.0000 2.0974	
1.3516 0.4821 0.2980 0.0000 2.2293	5
1.3846 0.4821 0.3053 0.0000 2.3660	J
1.4176 0.4821 0.3125 0.0000 2.5071	
1.4505 0.4821 0.3198 0.0000 2.6525	j
1.4835 0.4821 0.3271 0.0000 2.8008	;
1.5000 0.4821 0.3307 0.0000 3.8889	)

	Surfac	e retention	1 Hydraulic	Table	
Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	To Amended(cfs)	Wetted Surface
1.5000	0.4821	0.3307	0.000	2.9167	0.000
1.5330	0.4927	0.3468	0.000	2.9167	0.000
1.5659	0.5033	0.3632	0.000	3.0449	0.0000
1.5989	0.5139	0.3799	0.000	3.1090	0.000
1.6319	0.5245	0.3971	0.0000	3.1731	0.000
1.6648	0.5351	0.4145	0.0000	3.2372	0.0000
1.6978	0.5457	0.4323	0.0000	3.3013	0.000
1.7308	0.5563	0.4505	0.0000	3.3654	0.000
1.7637	0.5669	0.4690	0.0000	3.4295	0.0000
1.7967	0.5775	0.4879	0.0000	3.4936	0.0000
1.8297	0.5881	0.5071	0.0000	3.5577	0.000
1.8626	0.5987	0.5267	0.0000	3.6218	0.000
1.8956	0.6093	0.5466	0.0000	3.6859	0.0000
1.9286	0.6199	0.5668	0.0000	3.7500	0.000
1.9615	0.6305	0.5874	0.0000	3.8141	0.000
1.9945	0.6411	0.6084	0.0000	3.8782	0.0000
2.0275	0.6517	0.6297	0.0483	3.8889	0.000
2.0604	0.6623	0.6514	0.1574	3.8889	0.000
2.0934	0.6729	0.6734	0.3014	3.8889	0.0000
2.1264	0.6835	0.6957	0.4712	3.8889	0.0000
2.1593	0.6941	0.7185	0.6597	3.8889	0.0000

2.95050.94871.36843.07083.88890.00002.98350.95931.39983.12363.88890.0000	2.3571 2.3901 2.4231 2.4560 2.4890 2.5220 2.5549 2.5579 2.6209 2.6538 2.6868 2.7198 2.7527 2.7857 2.8187 2.8516 2.8846 2.9176 2.9505 2.9835	0.9593	1.3998	3.1236	3.8889	0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000000
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Name : Surface retention 1

Element Flows To: Outlet 1 Outlet 2 Gravel Trench Bed 1 Bioretention 1

```
: Gravel Trench Bed 1
Name
Bottom Length: 7000.00 ft.
Bottom Width: 15.00 ft.
Trench bottom slope 1: 0 To 1
Trench Left side slope 0: 0 To 1
Trench right side slope 2: 0 To 1
Material thickness of first layer: 0.5
Pour Space of material for first layer:
                                        0.4
Material thickness of second layer: 0
Pour Space of material for second layer: 0
Material thickness of third layer:
                                    0
Pour Space of material for third layer:
                                       0
Infiltration On
Infiltration rate: 2
Infiltration safety factor: 1
Wetted surface area On
Total Volume Infiltrated (ac-ft.): 9612.214
Total Volume Through Riser (ac-ft.): 0.016
Total Volume Through Facility (ac-ft.): 9612.23
Percent Infiltrated: 100
Total Precip Applied to Facility: 0
Total Evap From Facility: 0
Discharge Structure
```

Riser Height: 0.5 ft. Riser Diameter: 24 in.

Element Flows To: Outlet 1 Outlet 2

	Gravel	Trench Bed	Hudraulia	Table
Stage(feet)	Area(ac.)	Volume (ac-ft.		
0.0000	2.410	0.000	0.000	0.000
0.0056	2.410	0.005	0.000	4.861
0.0111	2.410	0.010	0.000	4.861
0.0167	2.410	0.016	0.000	4.861
0.0222	2.410	0.021	0.000	4.861
0.0278	2.410	0.026	0.000	4.861
0.0333	2.410	0.032	0.000	4.861
0.0389	2.410	0.037	0.000	4.861
0.0444	2.410	0.042	0.000	4.861
0.0500	2.410	0.048	0.000	4.861
0.0556	2.410	0.053	0.000	4.861
0.0611	2.410	0.058	0.000	4.861
0.0667	2.410	0.064	0.000	4.861
0.0722	2.410	0.069	0.000	4.861
0.0778	2.410	0.075	0.000	4.861
0.0833	2.410	0.080	0.000	4.861
0.0889	2.410	0.085	0.000	4.861
0.0944	2.410	0.091	0.000	4.861
0.1000	2.410	0.096	0.000	4.861
0.1056	2.410	0.101	0.000	4.861
0.1111	2.410	0.107	0.000	4.861
0.1167	2.410	0.112	0.000	4.861
0.1222	2.410	0.117	0.000	4.861
0.1278	2.410	0.123	0.000	4.861
0.1333	2.410	0.128	0.000	4.861
0.1389	2.410	0.133	0.000	4.861
0.1444	2.410	0.139	0.000	4.861
0.1500	2.410	0.144	0.000	4.861
0.1556	2.410	0.150	0.000	4.861
0.1611	2.410	0.155	0.000	4.861
0.1667	2.410	0.160	0.000	4.861
0.1722	2.410	0.166	0.000	4.861
0.1778	2.410	0.171	0.000	4.861
0.1833	2.410	0.176	0.000	4.861
0.1889	2.410	0.182	0.000	4.861
0.1944	2.410	0.187	0.000	4.861
0.2000 0.2056	2.410	0.192	0.000	4.861
	2.410	0.198	0.000	4.861
0.2111	2.410	0.203	0.000	4.861
0.2167 0.2222	2.410 2.410	0.208 0.214	0.000 0.000	4.861 4.861
0.2278	2.410	0.214	0.000	4.861
0.2333	2.410	0.219	0.000	4.861
0.2333	2.410	0.225	0.000	4.861
0.2444	2.410	0.235	0.000	4.861
0.2500	2.410	0.241	0.000	4.861
0.2556	2.410	0.246	0.000	4.861
0.2611	2.410	0.251	0.000	4.861
0.2667	2.410	0.257	0.000	4.861
3.200/	2.110	0.201	0.000	1.001

Basin Tot	al	6	.24		
Imperviou Imperviou	s Land Use s Total	<u>acr</u> 0			
Pervious : C, Pastu: Pervious '	Land Use re, Flat		<u>e</u> .24 .24		
Name : 1 Bypass: Y GroundWate					
	2.410	0.482	0.000	4.861	
0.4944 0.5000	2.410 2.410	0.476 0.482	0.000 0.000	4.861	
0.4889	2.410	0.471	0.000	4.861	
0.4833	2.410	0.466	0.000	4.861	
0.4778	2.410	0.460	0.000	4.861	
0.4722	2.410	0.455	0.000	4.861	
0.4667	2.410	0.450	0.000	4.861	
0.4611	2.410	0.444	0.000	4.861	
0.4500 0.4556	2.410 2.410	0.433 0.439	0.000 0.000	4.861 4.861	
0.4444	2.410	0.428	0.000	4.861	
0.4389	2.410	0.423	0.000	4.861	
0.4333	2.410	0.417	0.000	4.861	
0.4278	2.410	0.412	0.000	4.861	
0.4222	2.410	0.407	0.000	4.861	
0.4167	2.410	0.401	0.000	4.861	
0.4111	2.410	0.396	0.000	4.861	
0.4000	2.410	0.305	0.000	4.861	
D.3944 D.4000	2.410 2.410	0.380 0.385	0.000 0.000	4.861 4.861	
0.3889	2.410	0.375	0.000	4.861	
0.3833	2.410	0.369	0.000	4.861	
0.3778	2.410	0.364	0.000	4.861	
0.3722	2.410	0.358	0.000	4.861	
0.3667	2.410	0.353	0.000	4.861	
0.3611	2.410	0.348	0.000	4.861	
0.3556	2.410	0.342	0.000	4.861	
0.3500	2.410	0.337	0.000	4.861	
0.3389 0.3444	2.410 2.410	0.326 0.332	0.000 0.000	4.861 4.861	
0.3333	2.410	0.321	0.000	4.861	
0.3278	2.410	0.316	0.000	4.861	
0.3222	2.410	0.310	0.000	4.861	
0.3167	2.410	0.305	0.000	4.861	
0.3111	2.410	0.300	0.000	4.861	
0.3056	2.410	0.294	0.000	4.861	
0.3000	2.410	0.283	0.000	4.861	
0.2889 0.2944	2.410 2.410	0.278 0.283	0.000 0.000	4.861 4.861	
0.2833	2.410	0.273	0.000	4.861	
0.2778	2.410	0.267	0.000	4.861	

Element Flows To:

Surface	Interflow	Groundwater	
Name : Basin 3 Bypass: No GroundWater: No			
Pervious Land Use Pervious Total	acre 0		
Impervious Land Use	acre		
ROOF TOPS FLAT	18.72		
Impervious Total	18.72		
Basin Total	18.72		
Element Flows To:			
Surface	Interflow	Groundwater	
Gravel Trench Bed 2	Gravel Trench	Bed 2	
Name : Gravel Tren	ch Bed 2		
Bottom Length: 6500.			
Bottom Width: 20.00			
Trench bottom slope			
Trench Left side slop			
Trench right side slo	ope 2: 0.1 To 1	1	
Material thickness of	_		
Pour Space of materia	al for first lag	<b>yer:</b> 0.4	
Material thickness of	— — — — — — — — — — — — — — — — — — — —	0	
Pour Space of materia		-	
Material thickness of			
Pour Space of materia	al for third lay	<b>yer:</b> 0	
Infiltration On			
<b>Infiltration rate:</b> 2			
Infiltration safety			
Wetted surface area			
Total Volume Infiltra			
Total Volume Through			
Total Volume Through		<b>t.):</b> 8074.363	
Percent Infiltrated:			
Total Precip Applied			
Total Evap From Facility: 0			
Discharge Structure			
Riser Height: 0.99 f			
Riser Diameter: 12 i:	n.		
Element Flows To:	0+1.e+ 0		
Outlet 1	Outlet 2		
Gravel	French Bed Hydra	aulic Table	
	_	harge(cfs) Infilt(cfs)	
0.0000 2.984		.000 0.000	

Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs)
0.0000	2.984	0.000	0.000	0.000
0.0111	2.984	0.013	0.000	6.019
0.0222	2.985	0.026	0.000	6.019
0.0333	2.985	0.039	0.000	6.020
0.0444	2.985	0.053	0.000	6.021
0.0556	2.986	0.066	0.000	6.021
0.0667	2.986	0.079	0.000	6.022

0 0 0 0 0 0	0 000	0 000	0 0 0 0	6 000
0.0778	2.986	0.092	0.000	6.023
0.0889	2.987	0.106	0.000	6.023
0.1000	2.987	0.119	0.000	6.024
0.1111	2.987	0.132	0.000	6.025
0.1222	2.988	0.146	0.000	6.025
0.1333	2.988	0.159	0.000	6.026
0.1444	2.988	0.172	0.000	6.027
0.1556	2.989	0.185	0.000	6.027
0.1667	2.989	0.199	0.000	6.028
0.1778	2.989	0.212	0.000	6.029
0.1889	2.990	0.225	0.000	6.029
0.2000	2.990	0.239	0.000	6.030
0.2111	2.990	0.252	0.000	6.031
0.2222	2.991	0.265	0.000	6.031
0.2333	2.991	0.203	0.000	6.032
0.2444	2.991	0.292	0.000	6.033
0.2556	2.991	0.292	0.000	
0.2550	2.992			6.033
		0.318	0.000	6.034
0.2778	2.992	0.332	0.000	6.035
0.2889	2.993	0.345	0.000	6.036
0.3000	2.993	0.358	0.000	6.036
0.3111	2.993	0.372	0.000	6.037
0.3222	2.994	0.385	0.000	6.038
0.3333	2.994	0.398	0.000	6.038
0.3444	2.994	0.411	0.000	6.039
0.3556	2.995	0.425	0.000	6.040
0.3667	2.995	0.438	0.000	6.040
0.3778	2.995	0.451	0.000	6.041
0.3889	2.996	0.465	0.000	6.042
0.4000	2.996	0.478	0.000	6.042
0.4111	2.996	0.491	0.000	6.043
0.4222	2.997	0.505	0.000	6.044
0.4333	2.997	0.518	0.000	6.044
0.4444	2.997	0.531	0.000	6.045
0.4556	2.998	0.545	0.000	6.046
0.4667	2.998	0.558	0.000	6.046
0.4778	2.998	0.571	0.000	6.047
0.4889	2.999	0.585	0.000	6.048
0.5000	2.999	0.598	0.000	6.048
0.5111	2.999	0.611	0.000	6.049
0.5222	3.000	0.625	0.000	6.050
0.5333	3.000	0.638	0.000	6.050
0.5444	3.000	0.651	0.000	6.051
0.5556	3.001	0.665	0.000	6.051
0.5667	3.001	0.678	0.000	6.052
0.5778	3.001	0.691	0.000	6.053
0.5889	3.002	0.705	0.000	6.054
0.6000	3.002	0.718	0.000	6.054
0.6111	3.002	0.731	0.000	6.055
0.6222	3.003	0.745	0.000	6.056
0.6333	3.003	0.758	0.000	6.056
0.6444	3.003	0.771	0.000	6.057
0.6556	3.004	0.785	0.000	6.058
0.6667	3.004	0.798	0.000	6.058
0.6778	3.004	0.811	0.000	6.059
0.6889	3.005	0.825	0.000	6.060
0.7000	3.005	0.838	0.000	6.060
0.7111	3.005	0.851	0.000	6.061

#### ANALYSIS RESULTS Stream Protection Duration

Predeveloped Landuse Totals for POC #1 Total Pervious Area:47.95 Total Impervious Area:0

Mitigated Landuse Totals for POC #1 Total Pervious Area:6.24 Total Impervious Area:40.75

Flow Frequency Return Periods for Predeveloped. POC #1 Return Period Flow(cfs) 2 year 1.036878 5 year 1.574987 10 year 1.862724 25 year 2.152995 50 year 2.324448 100 year 2.46489

 Flow Frequency Return Periods for Mitigated.
 POC #1

 Return Period
 Flow(cfs)

 2 year
 0.159235

 5 year
 0.256797

 10 year
 0.333181

 25 year
 0.535719

 100 year
 0.636989

Stream	Protection Duration		
	Peaks for Predevelop	ped and Mitigated.	POC #1
Year	Predeveloped	Mitigated	
1902	1.275	0.188	
1903	0.497	0.083	
1904	1.083	0.250	
1905	0.518	0.083	
1906	0.387	0.069	
1907	1.558	0.257	
1908	0.992	0.147	
1909	1.013	0.151	
1910	1.625	0.264	
1911	0.873	0.137	
1912	3.380	0.630	
1913	1.443	0.213	
1914	0.379	0.066	
1915	0.539	0.096	
1916	0.875	0.139	
1910	0.404	0.065	
1917	0.915	0.140	
1918	0.915	0.120	
1920	0.945	0.146	
1921	0.991	0.157	
1922	1.045	0.184	
1923	0.849	0.156	
1924	0.496	0.089	
1925	0.549	0.097	
1926	0.840	0.145	
1927 1928	1.071 0.674	0.165 0.118	
		0.260	
1929 1930	1.615 0.879	0.129	
1931	0.929	0.149	
1932	0.696	0.131	
1933	0.794	0.147	
1934	2.102	0.347	
1935	0.810	0.125	
1936	1.202	0.177	
1937	1.334	0.252	
1938	1.015	0.147	
1939	0.132	0.060	
1940	0.853	0.145	
1941	0.810	0.134	
1942	1.364	0.215	
1943	0.540	0.101	
1944	1.557	0.383	
1945	0.970	0.160	
1946	0.827	0.151	
1947	0.616	0.105	
1948	2.042	0.299	
1949	1.756	0.297	
1950	0.896	0.143	
1951	0.989	0.149	
1952	3.095	0.560	
1953	2.509	0.468	
1954	0.826	0.141	
1955	0.710	0.111	
1956	0.544	0.095	

1957 $1.143$ $0.170$ $1958$ $2.627$ $0.413$ $1959$ $1.585$ $0.253$ $1960$ $0.570$ $0.095$ $1961$ $1.630$ $0.240$ $1962$ $0.904$ $0.153$ $1963$ $0.692$ $0.115$ $1964$ $1.931$ $0.538$ $1965$ $1.909$ $0.280$ $1966$ $0.464$ $0.082$ $1967$ $0.766$ $0.146$ $1968$ $1.034$ $0.166$ $1969$ $0.766$ $0.132$ $1970$ $1.136$ $0.209$ $1971$ $1.976$ $0.280$ $1972$ $1.304$ $0.429$ $1973$ $1.640$ $0.273$ $1974$ $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1993$ $1.223$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1999$ $0.337$ $0.033$ $2000$ <t< th=""><th>1057</th><th>1 1 1 2</th><th>0 170</th></t<>	1057	1 1 1 2	0 170
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1970 $1.136$ $0.209$ $1971$ $1.976$ $0.290$ $1972$ $1.304$ $0.429$ $1973$ $1.640$ $0.273$ $1974$ $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ <t< td=""><td>1968</td><td></td><td></td></t<>	1968		
1971 $1.976$ $0.290$ $1972$ $1.304$ $0.429$ $1973$ $1.640$ $0.273$ $1974$ $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.100$ $2013$ <t< td=""><td>1969</td><td>0.766</td><td></td></t<>	1969	0.766	
1972 $1.304$ $0.429$ $1973$ $1.640$ $0.273$ $1974$ $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.377$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.100$ $2010$ <t< td=""><td>1970</td><td>1.136</td><td>0.209</td></t<>	1970	1.136	0.209
1973 $1.640$ $0.273$ $1974$ $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.377$ $0.333$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.1004$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.1006$ $2013$	1971	1.976	0.290
1974 $0.969$ $0.178$ $1975$ $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.37$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2013$ <td< td=""><td>1972</td><td>1.304</td><td>0.429</td></td<>	1972	1.304	0.429
1975 $2.260$ $0.411$ $1976$ $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.100$ $2011$ $0.651$ $0.100$ $2013$ $0.851$ $0.128$	1973	1.640	0.273
1976 $1.008$ $0.209$ $1977$ $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2013$ $0.851$ $0.128$	1974	0.969	0.178
1977 $0.635$ $0.105$ $1978$ $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.377$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.922$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.100$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1975	2.260	0.411
1978 $1.812$ $0.283$ $1979$ $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.377$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.922$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1976	1.008	0.209
1979 $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1977	0.635	0.105
1979 $0.526$ $0.085$ $1980$ $0.980$ $0.148$ $1981$ $0.970$ $0.145$ $1982$ $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.187$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1978	1.812	0.283
1981 $0.970$ $0.145$ 1982 $0.634$ $0.101$ 1983 $1.576$ $0.230$ 1984 $0.464$ $0.145$ 1985 $1.121$ $0.173$ 1986 $0.879$ $0.144$ 1987 $1.806$ $0.304$ 1988 $1.169$ $0.170$ 1989 $1.019$ $0.157$ 1990 $1.262$ $0.189$ 1991 $0.974$ $0.160$ 1992 $1.310$ $0.197$ 1993 $1.223$ $0.189$ 1994 $1.946$ $0.292$ 1995 $0.551$ $0.087$ 1996 $2.141$ $0.329$ 1997 $1.065$ $0.163$ 1998 $1.023$ $0.187$ 1999 $0.037$ $0.033$ 2000 $0.747$ $0.150$ 2001 $0.537$ $0.092$ 2002 $1.724$ $0.357$ 2003 $1.141$ $0.185$ 2004 $1.124$ $0.184$ 2005 $1.549$ $0.290$ 2006 $0.697$ $0.112$ 2007 $0.808$ $0.127$ 2008 $1.039$ $0.156$ 2009 $0.651$ $0.104$ 2010 $0.573$ $0.092$ 2011 $0.651$ $0.100$ 2012 $1.061$ $0.219$ 2013 $0.851$ $0.128$	1979	0.526	0.085
1982 $0.634$ $0.101$ $1983$ $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1980	0.980	0.148
1983 $1.576$ $0.230$ $1984$ $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1981	0.970	0.145
1984 $0.464$ $0.145$ $1985$ $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1982	0.634	0.101
1985 $1.121$ $0.173$ $1986$ $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1983	1.576	0.230
1986 $0.879$ $0.144$ $1987$ $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1984	0.464	0.145
1987 $1.806$ $0.304$ $1988$ $1.169$ $0.170$ $1989$ $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1985	1.121	0.173
1988 $1.169$ $0.170$ 1989 $1.019$ $0.157$ 1990 $1.262$ $0.189$ 1991 $0.974$ $0.160$ 1992 $1.310$ $0.197$ 1993 $1.223$ $0.189$ 1994 $1.946$ $0.292$ 1995 $0.551$ $0.087$ 1996 $2.141$ $0.329$ 1997 $1.065$ $0.163$ 1998 $1.023$ $0.187$ 1999 $0.037$ $0.033$ 2000 $0.747$ $0.150$ 2001 $0.537$ $0.092$ 2002 $1.724$ $0.357$ 2003 $1.141$ $0.185$ 2004 $1.124$ $0.184$ 2005 $1.549$ $0.290$ 2006 $0.697$ $0.112$ 2007 $0.808$ $0.127$ 2008 $1.039$ $0.156$ 2009 $0.651$ $0.104$ 2010 $0.573$ $0.092$ 2011 $0.651$ $0.100$ 2012 $1.061$ $0.219$ 2013 $0.851$ $0.128$	1986	0.879	0.144
1989 $1.019$ $0.157$ $1990$ $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1987	1.806	0.304
1990 $1.262$ $0.189$ $1991$ $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1988	1.169	0.170
1991 $0.974$ $0.160$ $1992$ $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1989	1.019	0.157
1992 $1.310$ $0.197$ $1993$ $1.223$ $0.189$ $1994$ $1.946$ $0.292$ $1995$ $0.551$ $0.087$ $1996$ $2.141$ $0.329$ $1997$ $1.065$ $0.163$ $1998$ $1.023$ $0.187$ $1999$ $0.037$ $0.033$ $2000$ $0.747$ $0.150$ $2001$ $0.537$ $0.092$ $2002$ $1.724$ $0.357$ $2003$ $1.141$ $0.185$ $2004$ $1.124$ $0.184$ $2005$ $1.549$ $0.290$ $2006$ $0.697$ $0.112$ $2007$ $0.808$ $0.127$ $2008$ $1.039$ $0.156$ $2009$ $0.651$ $0.104$ $2010$ $0.573$ $0.092$ $2011$ $0.651$ $0.100$ $2012$ $1.061$ $0.219$ $2013$ $0.851$ $0.128$	1990	1.262	0.189
19931.2230.18919941.9460.29219950.5510.08719962.1410.32919971.0650.16319981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1991	0.974	0.160
19941.9460.29219950.5510.08719962.1410.32919971.0650.16319981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1992	1.310	0.197
19950.5510.08719962.1410.32919971.0650.16319981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1993	1.223	0.189
19962.1410.32919971.0650.16319981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1994	1.946	0.292
19971.0650.16319981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1995		
19981.0230.18719990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1996	2.141	0.329
19990.0370.03320000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1997	1.065	0.163
20000.7470.15020010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1998	1.023	0.187
20010.5370.09220021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	1999	0.037	0.033
20021.7240.35720031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2000	0.747	0.150
20031.1410.18520041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2001	0.537	0.092
20041.1240.18420051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2002	1.724	0.357
20051.5490.29020060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2003	1.141	0.185
20060.6970.11220070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2004		0.184
20070.8080.12720081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2005	1.549	0.290
20081.0390.15620090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2006	0.697	0.112
20090.6510.10420100.5730.09220110.6510.10020121.0610.21920130.8510.128	2007	0.808	0.127
20100.5730.09220110.6510.10020121.0610.21920130.8510.128	2008		0.156
20110.6510.10020121.0610.21920130.8510.128	2009		0.104
20121.0610.21920130.8510.128	2010	0.573	
2013 0.851 0.128			
2014 0.510 0.084			
	2014	0.510	0.084

2015 2016 2017 2018 2019 2020 2021 2022 2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 2036 2037 2038 2039 2040 2035 2036 2037 2038 2039 2040 2041 2042 2043 2044 2045 2044 2045 2044 2045 2044 2045 2044 2045 2046 2047 2048 2049 2050 2051 2055	1.553 0.362 1.606 2.936 3.116 0.974 1.320 0.495 1.080 3.777 0.864 1.550 0.739 0.408 1.047 2.071 0.576 0.483 0.573 2.385 1.219 0.277 1.287 0.155 0.535 1.219 0.2777 1.287 0.155 0.535 1.219 0.2777 1.287 0.155 0.535 1.165 1.471 0.904 1.087 0.756 1.066 0.964 0.657 1.112 0.551 1.013 1.368 0.483	0.360 0.062 0.248 0.469 0.558 0.206 0.217 0.082 0.162 0.770 0.144 0.245 0.128 0.077 0.153 0.331 0.094 0.091 0.092 0.365 0.194 0.052 0.228 0.034 0.108 0.117 0.127 0.1710 0.175 0.113 0.286 0.089 0.162 0.345 0.090
2053	1.013	0.162
2054	1.368	0.345

Stream	Protection Durat	ion	
Ranked	Annual Peaks for	Predeveloped and Mitigated.	POC #1
Rank	Predeveloped	Mitigated	
1	3.7773	0.7700	
2	3.3797	0.6298	
3	3.1157	0.5596	
4	3.0947	0.5583	
5	2.9360	0.5378	
6	2.6265	0.4695	
7	2.5654	0.4681	
8	2.5093	0.4305	
9	2.3848	0.4288	
10	2.2599	0.4133	

11	2.1415	0.4108
12	2.1015	0.3827
13	2.0713	0.3655
14	2.0416	0.3598
15	1.9761	0.3575
16	1.9459	0.3470
17	1.9311	0.3451
18 19	1.9088	0.3306 0.3285
20	1.8120 1.8058	0.3039
21	1.7558	0.2992
22	1.7236	0.2971
23	1.6403	0.2922
24	1.6297	0.2899
25	1.6247	0.2897
26	1.6152	0.2860
27 28	1.6063 1.5853	0.2829 0.2796
20	1.5764	0.2798
30	1.5582	0.2638
31	1.5569	0.2597
32	1.5527	0.2568
33	1.5498	0.2533
34	1.5485	0.2516
35	1.4714	0.2497
36 37	1.4428 1.3684	0.2479 0.2446
38	1.3636	0.2397
39	1.3343	0.2302
40	1.3202	0.2283
41	1.3102	0.2193
42	1.3043	0.2168
43	1.2872	0.2147
44 45	1.2749 1.2622	0.2133 0.2097
46	1.2226	0.2094
47	1.2189	0.2085
48	1.2024	0.2063
49	1.1688	0.1971
50	1.1651	0.1966
51	1.1433	0.1938
52 53	1.1409 1.1363	0.1893 0.1889
54	1.1239	0.1879
55	1.1211	0.1872
56	1.1118	0.1852
57	1.0869	0.1840
58	1.0832	0.1837
59	1.0798	0.1783
60 61	1.0715 1.0656	0.1767 0.1752
62	1.0648	0.1732
63	1.0614	0.1728
64	1.0470	0.1702
65	1.0448	0.1702
66	1.0389	0.1697
67	1.0337	0.1656
68	1.0232	0.1653

69	1.0191	0.1626
70	1.0154	0.1624
71	1.0133	0.1617
72	1.0128	0.1604
73	1.0078	0.1598
74	0.9918	0.1574
75	0.9913	0.1572
76	0.9889	0.1563
77	0.9797	0.1561
78	0.9739	0.1528
79	0.9736	0.1528
80	0.9700	0.1514
81	0.9699	0.1508
82	0.9687	0.1496
83 84 85	0.9638 0.9447 0.9292	0.1490 0.1495 0.1489 0.1484
86	0.9148	0.1470
87	0.9040	0.1469
88	0.9037	0.1466
89	0.8955	0.1464
90	0.8791	0.1457
91	0.8789	0.1454
92	0.8747	0.1450
93	0.8731	0.1450
94	0.8640	0.1447
95	0.8533	0.1445
96	0.8515	0.1444
97	0.8486	0.1433
98	0.8400	0.1413
99	0.8273	0.1402
100	0.8260	0.1391
101	0.8182	0.1367
102	0.8099	0.1338
103	0.8096	0.1319
104	0.8080	0.1311
105	0.7938	0.1305
106	0.7773	0.1291
107	0.7663	0.1289
108	0.7659	0.1281
109	0.7556	0.1276
110	0.7472	0.1273
111	0.7386	0.1265
112	0.7191	0.1249
113	0.7100	0.1201
114	0.6973	0.1182
115	0.6962	0.1166
116	0.6924	0.1155
117	0.6741	0.1152
118	0.6569	0.1127
119	0.6513	0.1116
120	0.6506	0.1111
121	0.6479	0.1079
122	0.6350	0.1053
123	0.6340	0.1046
124	0.6161	0.1044
125	0.5755	0.1015
126	0.5733	0.1014

127	0.5729	0.0997
128	0.5697	0.0988
129	0.5512	0.0965
130	0.5510	0.0964
131	0.5486	0.0953
132	0.5444	0.0949
133	0.5395	0.0940
134	0.5388	0.0925
135	0.5375	0.0918
136	0.5351	0.0910
137	0.5341	0.0897
138	0.5258	0.0894
130	0.5178	0.0894
140		
	0.5096	0.0888
141	0.4966	0.0872
142	0.4957	0.0849
143	0.4948	0.0842
144	0.4831	0.0834
145	0.4829	0.0828
146	0.4637	0.0820
147	0.4637	0.0817
148	0.4092	0.0771
149	0.4084	0.0721
150	0.4037	0.0694
151	0.3870	0.0663
152	0.3794	0.0646
153	0.3623	0.0619
154	0.2768	0.0599
155	0.1548	0.0525
156	0.1317	0.0343
157	0.0373	0.0328

Stream Protection Duration POC #1 The Facility PASSED The Facility PASSED.

Flow(cfs)	Predev	Mit	Percentage	Pass/Fail
0.5184	13447	8	0	Pass
0.5367	12377	7	0	Pass
0.5549	11355	6	0	Pass
0.5732	10400	4	0	Pass
0.5914	9621	3	0	Pass
0.6097	8951	2	0	Pass
0.6279	8286	2	0	Pass
0.6461	7651	1	0	Pass
0.6644	7097	1	0	Pass
0.6826	6616	1	0	Pass
0.7009	6181	1	0	Pass
0.7191	5738	1	0	Pass
0.7373	5340	1	0	Pass
0.7556	4983	1	0	Pass
0.7738	4643	0	0	Pass
0.7921	4319	0	0	Pass
0.8103	4034	0	0	Pass
0.8286	3767	0	0	Pass
0.8468	3516	0	0	Pass

0.8650 0.8833 0.9015	3274 3081 2898	0 0 0	0 0 0	Pass Pass Pass
0.9198 0.9380 0.9563	2729 2552 2406	0 0 0	0 0 0	Pass Pass Pass
0.9745	2250	0	0	Pass
0.9927	2113	0	0	Pass
1.0110	2000	0	0	Pass
1.0292	1870	0	0	Pass
1.0475	1773	0	0	Pass
1.0657 1.0840	1690 1607	0 0	0 0	Pass Pass
1.1022	1535	0	0	Pass
1.1204	1453	0	0	Pass
1.1387	1385	0	0	Pass
1.1569	1323	0	0	Pass
1.1752	1263	0	0	Pass
1.1934	1208	0	0	Pass
1.2117	1145	0	0	Pass
1.2299	1080	0	0	Pass
1.2481 1.2664	1024 976	0 0	0 0	Pass
1.2846	976	0	0	Pass Pass
1.3029	896	0	0	Pass
1.3211	848	0	0	Pass
1.3394	822	0	0	Pass
1.3576	791	0	0	Pass
1.3758	764	0	0	Pass
1.3941	739	0	0	Pass
1.4123	720	0	0	Pass
1.4306 1.4488	697 667	0 0	0 0	Pass
1.4488	667 635	0	0	Pass Pass
1.4853	607	0	0	Pass
1.5035	587	0	0	Pass
1.5218	559	0	0	Pass
1.5400	536	0	0	Pass
1.5583	502	0	0	Pass
1.5765	480	0	0	Pass
1.5947	468	0	0	Pass
1.6130 1.6312	448 425	0 0	0 0	Pass Pass
1.6495	402	0	0	Pass
1.6677	384	0	0	Pass
1.6860	374	0	0	Pass
1.7042	353	0	0	Pass
1.7224	340	0	0	Pass
1.7407	326	0	0	Pass
1.7589	307	0	0	Pass
1.7772	294	0	0	Pass
1.7954 1.8137	281 272	0 0	0 0	Pass Pass
1.8319	263	0	0	Pass
1.8501	248	0	0	Pass
1.8684	242	0	0	Pass
1.8866	229	0	0	Pass
1.9049	211	0	0	Pass

1.9231	200	0	0	Pass
1.9414	190	0	0	Pass
1.9596	177	0	0	Pass
1.9778	168	0	0	Pass
1.9961	157	0	0	Pass
2.0143	146	0	0	Pass
2.0326	137	0	0	Pass
2.0508	129	0	0	Pass
2.0691	122	0	0	Pass
2.0873	112	0	0	Pass
2.1055	103	0	0	Pass
2.1238	98	0	0	Pass
2.1420	92	0	0	Pass
2.1603	87	0	0	Pass
2.1785	84	0	0	Pass
2.1968	81	0	0	Pass
2.2150	75	0	0	Pass
2.2332	69	0	0	Pass
2.2515	63	0	0	Pass
2.2697	57	0	0	Pass
2.2880	53	0	0	Pass
2.3062	49	0	0	Pass
2.3244	46	0	0	Pass

Water Quality BMP Flow and Volume for POC #1 On-line facility volume: 0 acre-feet On-line facility target flow: 0 cfs. Adjusted for 15 min: 0 cfs. Off-line facility target flow: 0 cfs. Adjusted for 15 min: 0 cfs.

#### LID Report

LID Technique Water Quality Percent	Used for Comment	Total Volume	Volume	Infiltration	Cumulative	Percent
water guarity rescent	Treatment?	Needs	Through	Volume	Volume	Volume
Water Quality						
		Treatment	Facility	(ac-ft.)	Infiltratio	on
Infiltrated	Treated					
		(ac-ft)	(ac-ft)		Credit	
Gravel Trench Bed 1 POC	N	8747.13			N	100.00
retention 1	Ν	8747.64			N	99.68
Gravel Trench Bed 2 POC	Ν	7347.67			Ν	100.00
Total Volume Infiltrated		24842.44	0.00	0.00		99.89
0.00 0%	No Treat. Cr	redit				
Compliance with LID Standard 8						
Duration Analysis Result = Passed						

#### Perlnd and Implnd Changes

No changes have been made.

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