## CORNELIUS LACEY

JURISDICTION: CITY OF MARYSVILLE, WA<br>LOCATION: $83^{\text {RD }}$ AVE NE, SOUTH OF E SUNNYSIDE SCHOOL RD

## Prepared for:

Land Pro Group Inc.
$1051520^{\text {th }}$ Street SE
Suite 202
Lake Stevens, Washington 98258

Prepared by:

## Kimley»Horn

March 2024
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TRAFFIC IMPACT ANALYSIS

FOR

## CORNELIUS LACEY

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## 1. Development Identification

Kimley-Horn and Associates, Inc. (Kimley-Horn) has been retained to provide a traffic impact analysis for the Cornelius Lacey Development (Development). This report is intended to provide the City of Marysville (City) and Snohomish County (County) with the necessary traffic generation, trip distribution, and mitigation fee determination to facilitate their reviews of the Development. This report also addresses City comments dated February 28, 2024. The Development is located on the east side of $83{ }^{\text {rd }}$ Avenue NE, south of E Sunnyside School Road. A site vicinity map is included in Figure 1. The Development is proposed to consist of 67 single-family detached residential units. The site is currently listed as developed with two single-family detached units and one mobile home per the Snohomish County Online Property Information (SCOPI) web map. The site will primarily access the City street network via one proposed access drive connected to $83^{\text {rd }}$ Avenue NE. A site plan has been provided in Appendix A.

Brad Lincoln, responsible for this report and traffic analysis, is a licensed professional engineer (Civil) in the State of Washington and member of the Washington State section of the Institute of Transportation Engineers (ITE).

## 2. Methodology

Congestion at intersections and along arterials is generally measured in terms of level of service (LOS). In accordance with Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition by the Transportation Research Board, road facilities and intersections are rated between LOS A and LOS F, with LOS A being free flow and LOS F being forced flow or over-capacity conditions. The LOS at signalized, roundabout, and all-way stopcontrolled intersections is based on the average delay of all approaches. The LOS for two-way stopcontrolled intersections is based on average delays for the critical stopped approach. Geometric characteristics and conflicting traffic movements are taken into consideration when determining LOS values. A summary of the intersection LOS criteria is included in Table 1.


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Table 1: Level of Service Criteria

| Level of Service ${ }^{1}$ | Expected Delay | Intersection Control Delay <br> (Seconds per Vehicle) |  |
| :---: | :---: | :---: | :---: |
|  |  | Unsignalized <br> Intersections | Signalized <br> Intersections |
| A | Little/No Delay | $\leq 10$ | $\leq 10$ |
| B | Short Delays | $>10$ and $\leq 15$ | $>10$ and $\leq 20$ |
| C | Average Delays | $>15$ and $\leq 25$ | $>20$ and $\leq 35$ |
| D | Long Delays | $>25$ and $\leq 35$ | $>35$ and $\leq 55$ |
| E | Very Long Delays | $>35$ and $\leq 50$ | $>55$ and $\leq 80$ |
| F | Extreme Delays $^{2}$ | $>50$ | $>80$ |

The LOS at two-way stop-controlled intersections is based on the average delay for the stopped approach with the highest delay. The LOS at all-way stop-controlled intersections and signalized intersections is based on the average delay for all vehicles. The LOS analysis for unsignalized and signalized intersections has been performed utilizing the Synchro 11 software. The City identifies acceptable level of service for intersections as LOS D for all intersections.

The trip generation calculations for the Development are based on average trip generation rates published in the ITE Trip Generation Manual, $11^{\text {th }}$ Edition (2021). The opening year has been estimated for the year 2026, which accounts for a three-year construction window. The horizon year has therefore been evaluated for the year 2032.
${ }^{1}$ Source: Highway Capacity Manual, $6{ }^{\text {th }}$ Edition.
LOS A: Free-flow traffic conditions, with minimal delay to stopped vehicles (no vehicle is delayed longer than one cycle at signalized intersection).
LOS B: Generally stable traffic flow conditions.
LOS C: Occasional back-ups may develop but delay to vehicles is short term and still tolerable.
LOS D: During short periods of the peak hour, delays to approaching vehicles may be substantial but are tolerable during times of less demand (i.e., vehicles delayed one cycle or less at signal).
LOS E: Intersections operate at or near capacity, with long queues developing on all approaches and long delays. LOS F: Jammed conditions on all approaches with excessively long delays and vehicles unable to move at times. ${ }^{2}$ When demand volume exceeds the capacity of the lane, extreme delays will be encountered with queuing which may cause severe congestion affecting other traffic movements in the intersection.

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## 3. Trip Generation

The Development is proposed to consist of 67 single-family detached units. The site is currently developed with two single-family detached units and a mobile home. The trip generation calculations have been performed using data published by the ITE Trip Generation Manual, $11^{\text {st }}$ Edition (2021) and the City rate of 1.0 PM peak-hour trips per single-family residential unit. The average trip generation rates for ITE Land Use Codes (LUC) 210, Single-Family Detached Housing, and ITE LUC 240, Mobile Home, have been used for the trip generation calculations. The trip generation calculations for the Development are summarized in Table 2.

Table 2: Trip Generation Summary

| Land Use | Size | AverageDailyTrips(ADTs) | AM Peak-Hour Trips |  |  | PM Peak-Hour Trips |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Single-Family Detached Housing ITE LUC 210 | 67 Units | 632 | 12 | 35 | 47 | 42 | 25 | 67 |
| Single-Family Detached Housing <br> ITE LUC 210 <br> (Removed) | -2 Units | -19 | 0 | -1 | -1 | -1 | -1 | -2 |
| Mobile Home <br> ITE LUC 240 <br> (Removed) | -1 Unit | -7 | 0 | 0 | 0 | -1 | 0 | -1 |
| TOTAL |  | 606 | 12 | 34 | 46 | 40 | 24 | 64 |

The Development is anticipated to generate approximately 606 new ADTs with approximately 46 new AM peak-hour trips and 64 new PM peak-hour trips. The trip generation calculations are provided in Appendix B.

## 4. Trip Distribution

The trip distribution for the Development is based on comparison of Whiskey Ridge North and Whiskey Ridge East distributions established by the City since the site is located in the middle of the two areas. The trip distribution for the 2026 opening year is:

- $30 \%$ to and from the north along $83{ }^{\text {rd }}$ Avenue NE
- $28 \%$ to and from the east
- $20 \%$ to and from the south along SR-9
- $5 \%$ to and from the east along SR-92
- $3 \%$ to and from the north along SR-9
- $22 \%$ to and from the south along $83^{\text {rd }}$ Avenue NE
- $20 \%$ to and from the west along $44^{\text {th }}$ Street NE


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The trip distribution for the 2032 horizon year is:

- $33 \%$ to and from the east
- $25 \%$ to and from the south along SR-9
- $5 \%$ to and from the east along SR-92
- $3 \%$ to and from the north along SR-9
- $30 \%$ to and from the north along $83{ }^{\text {rd }}$ Avenue NE
- $15 \%$ to and from the south along $83^{\text {rd }}$ Avenue NE
- $22 \%$ to and from the west along $44^{\text {th }}$ Street NE

The Horizon Year distribution accounts for future connections south of the site and the conversion of Sunnyside School Road to a pedestrian trail. Detailed trip distributions for the AM peak-hour and PM peakhour during existing conditions are shown in Figure 2, and Figure 3, respectively. Detailed trip distributions for the AM peak-hour and PM peak-hour during horizon-year conditions are shown in Figure 4, and Figure 5, respectively. The established distributions are provided in Appendix C.

## 5. Intersection Level of Service Analysis

The following intersections have been analyzed based on an impact of 25 trips generated by the Development:

1. $83^{\text {rd }}$ Avenue NE at Line Road/44 ${ }^{\text {th }}$ Street NE
2. $83^{\text {rd }}$ Avenue NE at E Sunnyside School Road

The intersections have been analyzed for the weekday PM peak-hour.


FIGURE 2-AM PEAK HOUR OPENING YEAR TRIP DISTRIBUTION



FIGURE 4 - AM PEAK HOUR HORIZON YEAR TRIP DISTRIBUTION


FIGURE 5 - PM PEAK HOUR HORIZON YEAR TRIP DISTRIBUTION

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### 5.1. Turning Movement Calculations

The interlocal agreement between the City and County requires detailed development trip turning movement data at County key intersections impacted with three or more directional trips on an approach or departure. The Development will impact two key intersections during the AM peak-hour and PM Peakhour. The AM peak-hour key intersection impacts are shown in tabular form in Table 3 and the PM peakhour key intersection impacts are shown in tabular form in Table 4.
Table 3: Key Intersection Volumes - AM Peak Hour

| Intersection | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#147: | SR-9 at S Lake Stevens Road | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 13 | 0 |
| \#420: | SR-9 at $32^{\text {nd }}$ Street SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 13 | 0 |

Table 4: Key Intersection Volumes - PM Peak Hour

| Intersection | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#147: | SR-9 at S Lake Stevens Road | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 8 | 0 |
| \#420: | SR-9 at 32 ${ }^{\text {nd }}$ Street SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 8 | 0 |

The key intersection impacts are also shown in graphical form in Figure $\mathbf{2}$ and Figure $\mathbf{3}$ for the AM and PM peak-hours, respectively.

### 5.1.1. Intersection Volumes

The existing PM peak-hour turning movements at the study intersections were collected by the independent count firm Traffic Data Gathering (TDG) in March 2023. The 2023 existing turning movements at the study intersections are shown in Figure 6. The count data is included in Appendix C.

The future analysis has been performed for an opening year of 2026, which represents when the Development is expected to be constructed and occupied. The 2026 opening year baseline turning movements have been calculated by applying a 3\% annually compounding growth rate applied to the 2023 existing turning movements. The 2026 opening year baseline turning movements at the study intersections are shown in Figure 7. The 2026 opening year future with development turning movements at the study intersections have been calculated by adding the trips generated by the Development to the 2026 opening year baseline turning movements. The 2026 opening year future with development turning movements are shown in Figure 8.

The horizon year analysis accounts for the typical six-year concurrency period after the expected opening year. The 2032 horizon year baseline turning movements have been calculated using the same $3 \%$ annually compounding growth rate. Sunnyside School Road is planned to be converted to a pedestrian trail and will therefore not be an intersection under the 2032 horizon year conditions. The volumes calculated to be turning to and from Sunnyside School Road under the 2032 baseline conditions have been assigned to the $44^{\text {th }}$ Street NE intersection with the addition of 50 eastbound and westbound through trips to account for the potential diversion of trips with the closure. The 2032 horizon year baseline turning movements at the study intersection is shown in Figure 9. The 2032 horizon year future with development turning movements at the study intersection has been calculated by adding the trips generated by the Development to the 2032 horizon year baseline turning movements. The 2032 horizon year future with development turning movements are shown in Figure 10. The turning movement calculations are included in Appendix D.


83RD AVENUE NE AT E SUNNYSIDE
SCHOOL ROAD




## 83RD AVENUE NE AT

E SUNNYSIDE
SCHOOL ROAD




83RD AVENUE NE AT E SUNNYSIDE
SCHOOL ROAD



44TH ST NE


ヨN ヨヘV H6L


SOPER HILL RD

Study Intersection
Development Site
$\mathrm{PM} \rightarrow$ Turning Movement Volumes



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### 5.2. Level of Service Calculations

The level of service calculations have been performed utilizing the existing channelization, existing intersection control and peak-hour factors and heavy vehicle factors from the 2023 turning movement counts. The level of service summary for the opening-year is included in Table 5 and the level of service summary for the horizon-year is included in Table 6 for the PM peak-hour. It should be noted that the future conversion of Sunnyside School Road to a pedestrian trail will remove the east leg extension along 83rd Avenue NE. With this removal the intersection will only be impacted by through traffic and no longer have stop-control delay. The intersection of $83^{\text {rd }}$ Avenue NE at E Sunnyside School Road has therefore been removed from the horizon-year analysis.

Table 5: Level of Service Summary - 2026 Opening-Year

| Intersection |  | Approach | 2023 Existing |  | 2026 Baseline |  | $2026$ <br> Future w Dev. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay | LOS | Delay | LOS | Delay |
| 1: | 83 ${ }^{\text {rd }}$ Avenue NE at <br> $44^{\text {th }}$ Street NE |  | Two-Way Stop Control | B | 11.3 sec | B | 11.7 sec | B | 12.8 sec |
|  | $83^{\text {rd }}$ Avenue NE at E <br> Sunnyside School Road | Two-Way Stop Control | B | 10.8 sec | B | 11.2 sec | B | 11.7 sec |

Table 6: Level of Service Summary - 2032 Horizon-Year

| Intersection |  | Approach | 2023 Existing |  | 2032 Baseline |  | $\begin{gathered} 2032 \\ \text { Future w Dev. } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay | LOS | Delay | LOS | Delay |
|  | $83^{\text {rd }}$ Avenue NE at 44 ${ }^{\text {th }}$ Street NE |  | Two-Way Stop Control | B | 11.3 sec | D | 25.4 sec | D | 29.8 sec |

The analysis shows that the study intersections currently operate at LOS B during the PM peak-hour. In the 2026 opening-year baseline and future with development conditions, all study intersections are anticipated to continue operating at LOS B with the Development. In the 2032 horizon-year baseline and future with development conditions, the study intersection is anticipated to operating at LOS D with the Development. The intersection LOS calculations are provided in the Appendix E.

## 6. Site Access

The Development is proposed to have one access driveway to 83 rd Avenue NE and an access that will form the extension of $44^{\text {th }}$ Street NE. The access locations appear to have adequate sight distance, based on preliminary evaluations.

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## 7. Transportation Impact Fees

The City has interlocal agreements with the County and WSDOT for transportation impact fees. These transportation impact fees are based on the area wide traffic mitigation fee or actual impacts to improvement projects.

### 7.1. City of Marysville

The City traffic mitigation fees have been calculated using the residential rates of $\$ 6,300$ per new singlefamily unit. The Development is anticipated to consist of 65 new single-family units with credit for the two existing single-family detached units. The City of Marysville traffic mitigation fees for the Development should therefore be $\$ 409,500.00$. It is important to note that these calculations do not include a credit for the mobile home unit on the site. Including the credit for that unit would reduce the fees to $\$ 403,200.00$.

### 7.2. Snohomish County

The City and County have an interlocal agreement that provides for the payment of traffic mitigation for impacts to County roadways by City developments. Traffic mitigation fees are based on predetermined area impacts or impacts to actual improvement projects. The only County improvement project in the area is along $88^{\text {th }}$ Street NE, between approximately $44^{\text {th }}$ Drive NE to $66^{\text {th }}$ Drive NE. This improvement project is not anticipated to be impacted by three directional PM peak-hour trips from the Development. County traffic mitigation fees should therefore not be required for the Development.

### 7.3. Washington State Department of Transportation

The WSDOT mitigation fees are based on impacts to improvement projects identified in the Exhibit C List included in the interlocal agreement between the County and WSDOT. There are not any WSDOT intersections on the Exhibit C List that will be impacted by three directional PM peak-hour trips generated by the Development. WSDOT transportation impact fees should therefore not be required for the Development.

## 8. Conclusions

The Development is proposed to consist of 67 single-family detached residential units. The site is currently listed as occupied with two single-family detached units and one mobile home. The Development is anticipated to generate approximately 606 new ADTs with approximately 46 new AM peak-hour trips and 60 new PM peak-hour trips. The Development is anticipated to construct 65 new single-family units. The City traffic mitigation fees for the Development should therefore be $\$ 409,500.00$, with fees as low as $\$ 403,200.00$ with credit for the mobile home. Neither County nor WSDOT traffic mitigation fees should be required for the Development.

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## APPENDIX A Site Plan



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## APPENDIX B <br> Trip Generation Calculations

Trip Generation for: Weekday
(a.k.a.): Average Weekday Daily Trips (AWDT)

|  |  |  |  |  |  |  |  |  | NET EXTERNAL TRIPS BY TYPE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Gross Trips |  |  |  |  |  | IN BOTH DIRECTIONS |  |  |  |  |  | DIRECTIONAL ASSIGNMENTS |  |  |  |  |  |
|  |  |  | Internal Crossover | TOTAL | PASS-BY |  | DIVERTED LINK |  | NEW | PASS-BY |  | DIVERTED <br> LINK |  | NEW |  |
| LAND USES | VARIABLE | $\begin{array}{\|c\|} \hline \text { ITE } \\ \text { LU } \\ \text { code } \end{array}$ |  |  |  |  | Trip Rate | $\begin{aligned} & \% \\ & \text { IN } \end{aligned}$ | $\begin{gathered} \% \\ \text { OUT } \end{gathered}$ | In+Out (Total) | \% of Gross Trips | $\begin{gathered} \text { Trips } \\ \text { In+Out } \\ \text { (Total) } \end{gathered}$ | In+Out <br> (Total) | \% of <br> Ext. <br> Trips | In+Out (Total) | \% of <br> Ext. <br> Trips | In+Out (Total) | In+Out (Total) | In | Out | In | Out | In | Out |
| Single-Family Detached Housing | 67 units | 210 | 9.43 | 50\% | 50\% | 632 | 0\% | 0 | 632 | 0\% | 0 | 0\% | 0 | 632 | 0 | 0 | 0 | 0 | 316 | 316 |
| Single-Family Detached Housing (Removed) | -2 units | 210 | 9.43 | 50\% | 50\% | -19 | 0\% | 0 | -19 | 0\% | 0 | 0\% | 0 | -19 | 0 | 0 | 0 | 0 | -10 | -9 |
| Mobile Home (Removed) | -1 unit | 240 | 7.12 | 50\% | 50\% | -7 | 0\% | 0 | -7 | 0\% | 0 | 0\% | 0 | -7 | 0 | 0 | 0 | 0 | -4 | -3 |
| Total |  |  |  |  |  | 606 |  | 0 | 606 |  | 0 |  | 0 | 606 | 0 | 0 | 0 | 0 | 302 | 304 |

Trip Generation for: Weekday, Peak Hour of Adjacent Street Traffic, One Hour between 7 and 9 AM
(a.k.a.): Weekday AM Peak Hour

|  |  |  |  |  |  |  |  |  | NET EXTERNAL TRIPS BY TYPE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Gross Trips |  |  |  |  |  | IN BOTH DIRECTIONS |  |  |  |  |  | DIRECTIONAL ASSIGNMENTS |  |  |  |  |  |
|  |  |  | Internal Crossover | TOTAL | PASS-BY |  | DIVERTED LINK |  | NEW | PASS-BY |  | DIVERTEDLINK |  | NEW |  |
| LAND USES | VARIABLE | $\begin{gathered} \hline \text { ITE } \\ \text { LU } \\ \text { code } \end{gathered}$ |  |  |  |  | Trip <br> Rate | $\begin{aligned} & \% \\ & \text { IN } \end{aligned}$ | $\begin{gathered} \text { \% } \\ \text { OUT } \end{gathered}$ | In+Out (Total) | \% of Gross Trips | $\begin{array}{\|c\|} \hline \text { Trips } \\ \text { In+Out } \\ \text { (Total) } \\ \hline \end{array}$ | In+Out (Total) | \% of <br> Ext. <br> Trips | In+Out (Total) | \% of <br> Ext. <br> Trips | In+Out <br> (Total) | In+Out (Total) | In | Out | In | Out | In | Out |
| Single-Family Detached Housing | 67 units | 210 | 0.70 | 26\% | 74\% | 47 | 0\% | 0 | 47 | 0\% | 0 | 0\% | 0 | 47 | 0 | 0 | 0 | 0 | 12 | 35 |
| Single-Family Detached Housing (Removed) | -2 units | 210 | 0.70 | 26\% | 74\% | -1 | 0\% | 0 | -1 | 0\% | 0 | 0\% | 0 | -1 | 0 | 0 | 0 | 0 | 0 | -1 |
| Mobile Home (Removed) | -1 unit | 240 | 0.39 | 21\% | 79\% | 0 | 0\% | 0 | 0 | 0\% | 0 | 0\% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total |  |  |  |  |  | 46 |  | 0 | 46 |  | 0 |  | 0 | 46 | 0 | 0 | 0 | 0 | 12 | 34 |

Trip Generation for: Weekday, Peak Hour of Adjacent Street Traffic, One Hour between 4 and 6 PM (a.k.a.): Weekday PM Peak Hour

|  |  |  |  |  |  |  |  |  | NET EXTERNAL TRIPS BY TYPE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Gross Trips |  |  |  |  |  | IN BOTH DIRECTIONS |  |  |  |  |  | DIRECTIONAL ASSIGNMENTS |  |  |  |  |  |
|  |  |  | Internal Crossover | TOTAL | PASS-BY |  | DIVERTED LINK |  | NEW | PASS-BY |  | DIVERTEDLINK |  | NEW |  |
| LAND USES | VARIABLE | $\begin{array}{\|c\|} \hline \text { ITE } \\ \text { LU } \\ \text { code } \end{array}$ |  |  |  |  | Trip Rate | $\begin{aligned} & \% \\ & \text { IN } \end{aligned}$ | $\begin{gathered} \% \\ \text { OUT } \end{gathered}$ | In+Out (Total) | \% of Gross Trips | Trips In+Out (Total) | In+Out (Total) | $\begin{array}{\|l} \hline \% \text { of } \\ \text { Ext. } \\ \text { Trips } \\ \hline \end{array}$ | In+Out (Total) | $\begin{array}{\|l\|} \hline \% \text { of } \\ \text { Ext. } \\ \text { Trips } \\ \hline \end{array}$ | In+Out (Total) | In+Out (Total) | In | Out | In | Out | In | Out |
| Single-Family Detached Housing | 67 units | 210 | 1.00 | 63\% | 37\% | 67 | 0\% | 0 | 67 | 0\% | 0 | 0\% | 0 | 67 | 0 | 0 | 0 | 0 | 42 | 25 |
| Single-Family Detached Housing (Removed) | -2 units | 210 | 1.00 | 63\% | 37\% | -2 | 0\% | 0 | -2 | 0\% | 0 | 0\% | 0 | -2 | 0 | 0 | 0 | 0 | -1 | -1 |
| Mobile Home (Removed) | -1 unit | 240 | 0.58 | 62\% | 38\% | -1 | 0\% | 0 | -1 | 0\% | 0 | 0\% | 0 | -1 | 0 | 0 | 0 | 0 | -1 | 0 |
| Total |  |  |  |  |  | 64 |  | 0 | 64 |  | 0 |  | 0 | 64 | 0 | 0 | 0 | 0 | 40 | 24 |

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## APPENDIX C <br> Distribution and Count Data






83rd Avenue NE @ Line Road/44th Street NE


Marysville, WA


TURNING MOVEMENTS DIAGRAM PEAK HOUR SUMMARY

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## APPENDIX D <br> Turning Movement Calculations





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## APPENDIX E

Level of Service Calculations


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 373 | 373 | 137 | 395 | 395 | 170 | 159 | 0 | 0 | 170 | 0 | 0 |  |
| Stage 1 | 137 | 137 | - | 236 | 236 | - | - | - | - | - | - | - |  |
| Stage 2 | 236 | 236 | - | 159 | 159 | - | - | - | - | - | - | - |  |
| Critical Hdwy | 7.11 | 6.51 | 6.21 | 7.11 | 6.51 | 6.21 | 4.11 | - | - | 4.11 | - | - |  |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 | 3.509 | 4.009 | 3.309 | 2.209 | - |  | 2.209 | - | - |  |
| Pot Cap-1 Maneuver | 586 | 559 | 914 | 567 | 543 | 876 | 1427 | - | - | 1413 | - | - |  |
| Stage 1 | 869 | 785 | - | 769 | 712 | - | - | - | - | - | - | - |  |
| Stage 2 | 769 | 712 | - | 846 | 768 | - | - | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |  |
| Mov Cap-1 Maneuver | 574 | 544 | 914 | 530 | 529 | 876 | 1427 | - | - | 1413 | - | - |  |
| Mov Cap-2 Maneuver | 574 | 544 | - | 530 | 529 | - | - | - | - | - | - | - |  |
| Stage 1 | 846 | 785 | - |  | 693 | - | - | - | - | - | - | - |  |
| Stage 2 | 749 | 693 | - | 806 | 768 | - | - | - | - | - | - | - |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, S | 11.3 | 0 | 1.2 | 0 |
| HCM LOS | B | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1427 | - | -679 | -1413 | - | - |  |
| HCM Lane V/C Ratio | 0.023 | - | -0.152 | - | - | - | - |
| HCM Control Delay (s) | 7.6 | 0 | -11.3 | 0 | 0 | - | - |
| HCM Lane LOS | A | A | - | B | A | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0.5 | - | 0 | - |
| (ven | - |  |  |  |  |  |  |



| Major/Minor | Minor1 | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 409 | 202 | 0 | 0 | 219 |
| $\quad$ Stage 1 | 202 | - | - | - | - |
| $\quad$ Stage 2 | 207 | - | - | - | - |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 10.8 | 0 | 1.6 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -749 | 1344 | - |
| HCM Lane V/C Ratio | - | -0.173 | 0.026 | - |
| HCM Control Delay (s) | - | - | 10.8 | 7.8 |
| HCM Lane LOS | - | - | 0 | A |
| A | A |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 0.6 | 0.1 |



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 408 | 408 | 150 | 432 | 432 | 186 | 174 | 0 | 0 | 186 | 0 | 0 |  |
| Stage 1 | 150 | 150 | - | 258 | 258 | - | - | - | - | - | - | - |  |
| Stage 2 | 258 | 258 | - | 174 | 174 | - | - | - | - | - | - | - |  |
| Critical Hdwy | 7.11 | 6.51 | 6.21 | 7.11 | 6.51 | 6.21 | 4.11 | - | - | 4.11 | - | - |  |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 | 3.509 | 4.009 | 3.309 | 2.209 | - |  | 2.209 | - | - |  |
| Pot Cap-1 Maneuver | 555 | 534 | 899 | 536 | 518 | 859 | 1409 | - | - | 1395 | - | - |  |
| Stage 1 | 855 | 775 | - | 749 | 696 | - | - | - | - | - | - | - |  |
| Stage 2 | 749 | 696 | - | 830 | 757 | - | - | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |  |
| Mov Cap-1 Maneuver | 543 | 519 | 899 | 497 | 503 | 859 | 1409 | - | - | 1395 | - | - |  |
| Mov Cap-2 Maneuver | 543 | 519 | - | 497 | 503 | - | - | - | - | - | - | - |  |
| Stage 1 | 831 | 775 | - |  | 677 | - | - | - | - | - | - | - |  |
| Stage 2 | 728 | 677 | - | 786 | 757 | - | - | - | - | - | - | - |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, S | 11.7 | 0 | 1.2 | 0 |
| HCM LOS | B | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1409 | - | -651 | - | 1395 | - | - |
| HCM Lane V/C Ratio | 0.026 | - | -0.174 | - | - | - | - |
| HCM Control Delay (s) | 7.6 | 0 | -11.7 | 0 | 0 | - | - |
| HCM Lane LOS | A | A | - | B | A | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0.6 | - | 0 | - |
| ( |  | - |  |  |  |  |  |



| Major/Minor | Minor1 | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 446 | 219 | 0 | 0 | 238 |
| $\quad$ Stage 1 | 219 | - | - | - | - |
| $\quad$ Stage 2 | 227 | - | - | - | - |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 11.2 | 0 | 1.6 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -725 | 1323 | - |
| HCM Lane V/C Ratio | - | -0.196 | 0.029 | - |
| HCM Control Delay (s) | - | -11.2 | 7.8 | 0 |
| HCM Lane LOS | - | - | B | A |
| HCM 95th \%tile Q(veh) | - | - | 0.7 | 0.1 |
| A |  | - |  |  |




| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | :--- | :--- |
| HCM Control Delay, s | 12.8 | 10.9 | 1.2 | 0.9 |
| HCM LOS | B | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1409 | - | - | 581 | 637 | 1384 | - |
| - |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.026 | - | - | 0.21 | 0.036 | 0.017 | - |



| Major/Minor | Minor1 | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 470 | 231 | 0 | 0 | 253 |
| $\quad$ Stage 1 | 231 | - | - | - | - |
| $\quad$ Stage 2 | 239 | - | - | - | - |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 11.7 | 0 | 1.5 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -692 | 1306 | - |
| HCM Lane V/C Ratio | - | -0.222 | 0.029 | - |
| HCM Control Delay (s) | - | - | 11.7 | 7.8 |
| HCM Lane LOS | - | - | B | A |
| A | A |  |  |  |
| HCM 95th \%tile Q(veh) | - | - | 0.8 | 0.1 |
|  |  | - |  |  |



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 693 | 626 | 180 | 658 | 631 | 245 | 208 | 0 | 0 | 268 | 0 | 0 |  |
| Stage 1 | 272 | 272 | - | 331 | 331 | - | - | - | - | - | - | - |  |
| Stage 2 | 421 | 354 | - | 327 | 300 | - | - | - | - | - | - | - |  |
| Critical Hdwy | 7.11 | 6.51 | 6.21 | 7.11 | 6.51 | 6.21 | 4.11 | - | - | 4.11 | - | - |  |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - | 6.11 | 5.51 | . | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 | 3.509 | 4.009 | 3.309 | 2.209 | - |  | 2.209 | - | - |  |
| Pot Cap-1 Maneuver | 359 | 402 | 865 | 379 | 399 | 796 | 1369 | - | - | 1302 | - | - |  |
| Stage 1 | 736 | 686 | - | 684 | 647 | - | - | - | - | - | - | - |  |
| Stage 2 | 612 | 632 | - | 688 | 667 | - | - | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |  |
| Mov Cap-1 Maneuver | 253 | 371 | 865 | 296 | 369 | 796 | 1369 | - | - | 1302 | - | - |  |
| Mov Cap-2 Maneuver | 253 | 371 | - | 296 | 369 | - | - | - | - | - | - | - |  |
| Stage 1 | 709 | 659 | - | 659 | 623 | - | - | - | - | - | - | - |  |
| Stage 2 | 453 | 609 | - | 566 | 640 | - | - | - | - | - | - | - |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | :--- | :--- |
| HCM Control Delay, s | 25.4 | 18.2 | 1.1 | 1.4 |
| HCM LOS | D | $C$ |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1369 | - | - | 362 | 493 | 1302 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 11.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | ${ }_{\text {¢ }}$ |  |  | $\dagger$ |  |  | ¢ |  |
| Traffic Vol, veh/h | 72 | 58 | 51 | 43 | 55 | 121 | 39 | 202 | 48 | 53 | 137 | 52 |
| Future Vol, veh/h | 72 | 58 | 51 | 43 | 55 | 121 | 39 | 202 | 48 | 53 | 137 | 52 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# |  | 0 |  | - | 0 | - | - | 0 | - |  | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 79 | 64 | 56 | 47 | 60 | 133 | 43 | 222 | 53 | 58 | 151 | 57 |


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 727 | 657 | 180 | 691 | 659 | 249 | 208 | 0 | 0 | 275 | 0 | 0 |  |
| Stage 1 | 296 | 296 | - | 335 | 335 | - | - | - | - | - | - | - |  |
| Stage 2 | 431 | 361 | - | 356 | 324 | - | - | - | - | - | - | - |  |
| Critical Hdwy | 7.11 | 6.51 | 6.21 | 7.11 | 6.51 | 6.21 | 4.11 | - | - | 4.11 | - | - |  |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - | 6.11 | 5.51 | - | - | - | - | - | - | - |  |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 | 3.509 | 4.009 | 3.309 | 2.209 | - |  | 2.209 | - | - |  |
| Pot Cap-1 Maneuver | 341 | 386 | 865 | 360 | 385 | 792 | 1369 | - | - | 1294 | - | - |  |
| Stage 1 | 715 | 670 | - | 681 | 644 | - | - | - | - | - | - | - |  |
| Stage 2 | 605 | 628 | - | 664 | 651 | - | - | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |  |
| Mov Cap-1 Maneuver | 231 | 353 | 865 | 271 | 352 | 792 | 1369 | - | - | 1294 | - | - |  |
| Mov Cap-2 Maneuver | 231 | 353 | - | 271 | 352 | - | - | - | - | - | - | - |  |
| Stage 1 | 689 | 636 | - | 656 | 620 | - | - | - | - | - | - | - |  |
| Stage 2 | 438 | 605 | - | 530 | 618 | - | - | - | - | - | - | - |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | :--- |
| HCM Control Delay, s | 29.8 | 20.6 | 1 | 1.7 |
| HCM LOS | D | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1369 | - | -338 | 468 | 1294 | - | - |
| HCM Lane V/C Ratio | 0.031 | - | -0.588 | 0.514 | 0.045 | - | - |
| HCM Control Delay (s) | 7.7 | 0 | - | 29.8 | 20.6 | 7.9 | 0 |
| - |  |  |  |  |  |  |  |
| HCM Lane LOS | A | A | - | D | C | A | A |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 3.6 | 2.9 | 0.1 | - |
| H |  |  |  |  |  |  |  |

