

Traffic Impact Analysis

BROWN BEAR (WHITE BARN DEVELOPMENT LOTS 4 AND 5)

Prepared for:
Brown Bear

August 2023

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Introduction

This traffic impact analysis (TIA) identifies potential transportation-related impacts associated with the construction of a Brown Bear Car Wash located north of Soper Hill Road and east of 87th Avenue NE in The City of Marysville. As necessary, mitigation measures are identified that would reduce or offset significant transportation related impacts that the project may have on the surrounding transportation system.

Project Description

The proposed project is located north of Soper Hill Road and west of SR 9 within the approved White Barn Development¹. Figure 1 illustrates the site vicinity and surrounding streets. The project includes a car wash with 5 touchless bays, 1 automated tunnel, and 26 vacuuming stalls located on lots 4 and 5 within the White Barn development. No new access points are proposed as part of this project. Access to this site would be provided to the south of the project via an existing right-in/right-out (RIRO) driveway at the 89th Ave NE/Soper Hill Road intersection as well as west of the site via 87th Ave NE. Approximately 12 on-site parking spaces are proposed. A site plan is included in Figure 2. The project is anticipated to be constructed and occupied by the end of 2024.

Study Scope

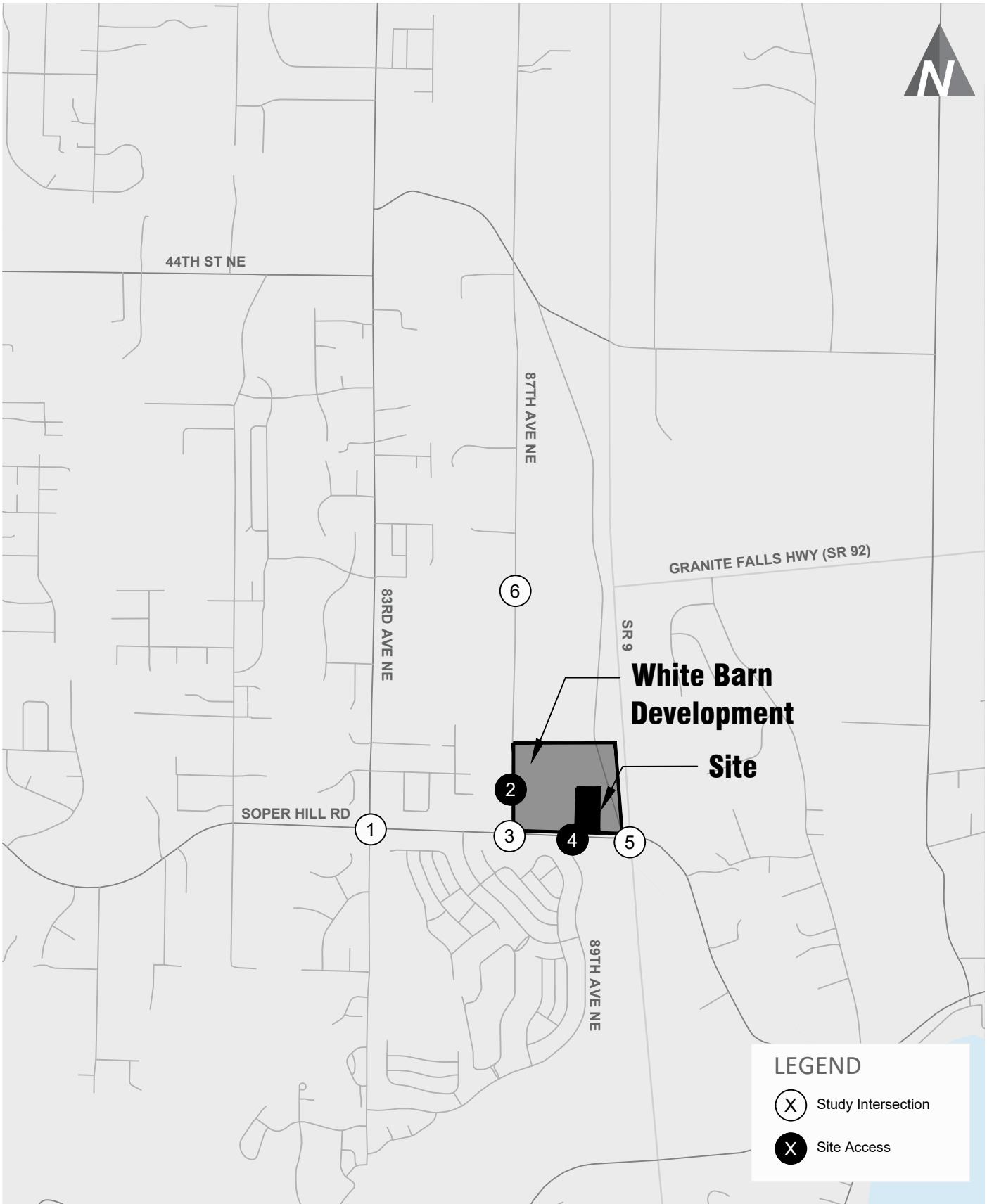
Although a TIA was prepared for the full buildout of the White Barn development, concurrency was issued for the initial phase only as part of that study. Concurrency for the individual lots has been reviewed and issued subsequent to that initial phase.

The scope of the analysis conducted for the Brown Bear project is consistent with the City's *Guidelines for the Preparation of Traffic Impact Analysis - 2017*. The scope of the analysis includes a review of existing and future without-project conditions in the vicinity of the project site under weekday PM peak hour conditions. Future analysis years include the project's opening year of 2024 as well as a horizon year of 2030 (i.e. 6 years following the project's opening year). The study intersections include those forecast to be impacted by 25 or more weekday PM peak hour trips (see Table 6). As coordinated with the City of Marysville and based on the anticipated vehicular impacts of the proposed project, the following intersections were identified for analysis:

1. 83rd Avenue NE/Soper Hill Road (*2024 analysis only*)
2. 87th Avenue NE/Northern Site Access
3. 87th Avenue NE/Soper Hill Road
4. 89th Avenue NE/Soper Hill Road
5. SR 9/Soper Hill Road
6. 87th Avenue NE/35th Street NE (*2030 analysis only*)

This report includes a review of the surrounding street system, transit service, non-motorized facilities, existing and future (2024 and 2030) without-project weekday peak hour traffic volumes, traffic operations, and traffic safety. Future (2024 and 2030) with-project conditions were estimated by adding site-generated traffic to future without-project volumes. The project's impacts on the surrounding transportation system were identified by comparing the future with-project conditions to the future without-project conditions.

¹ The full buildout of the White Barn development was previously completed and is included in the *White Barn Development Traffic Impact Analysis* (GTC, February 2021).



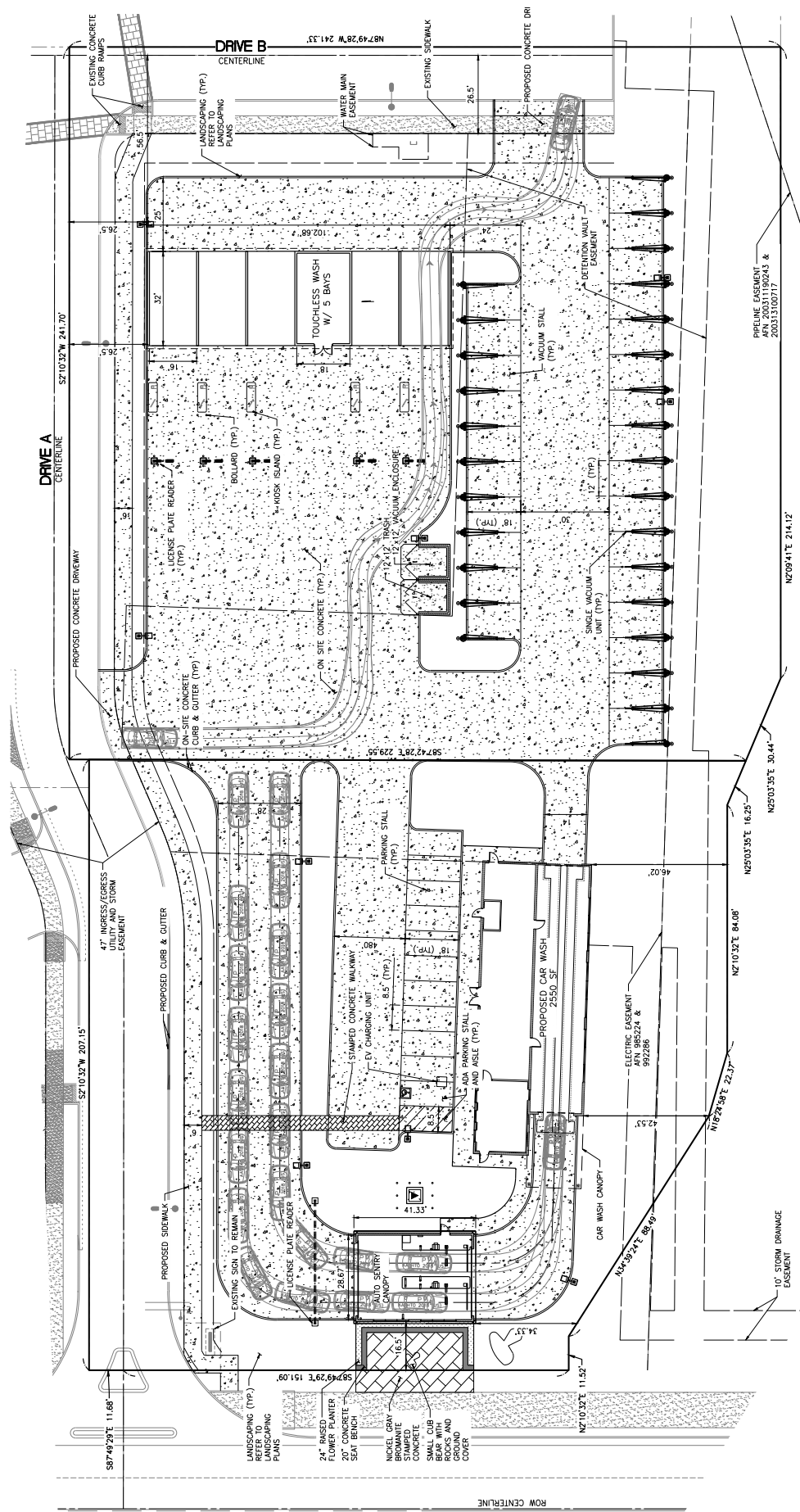
Site Vicinity and Study Intersections

White Barn Brown Bear - Marysville

FIGURE

1





PRELIM EASEMENT
REFERS 22451
&
200313100717

NZ0941E 214.12'

NZ50335E 16.25'

NZ1039E 84.08'

NZ1039E 22.37'

NZ1039E 30.44'

NZ1039E 11.52'

NZ1039E 88.19'

NZ1039E 88.19'

Site Plan

White Barn Brown Bear - Marysville

FIGURE

2



Existing and Future Without-Project Conditions

This section describes both existing and future (2024 and 2030) without-project conditions within the identified study area. Characteristics are provided for the roadway network, transit service, non-motorized facilities, traffic volumes, traffic operations, and traffic safety.

Street System

The following describes the existing street network within the vicinity of the proposed project and any anticipated changes resulting from planned improvements.

Existing Inventory

Characteristics of the existing street system in the project vicinity are described in Table 1. The roadways adjacent to the project site are currently collector and minor arterials.

Table 1. Roadway Network Existing Conditions Summary

| Roadway | Classification | Posted Speed Limit | # Lanes | Parking | Pedestrian Facilities | Bicycle Facilities |
|---------------------------------|--------------------|--------------------|---------|---------|-----------------------|------------------------|
| SR9 | State Highway | 55mph | 3 | No | No | No |
| SR92 (Granite Falls Hwy) | State Highway | 55mph | 3 | No | No | No |
| Sunnyside Blvd | Minor Arterial | 25mph | 2 | No | Sidewalk | No |
| Line Rd/44th St NE | Collector Arterial | 35 mph | 2 | No | No | No |
| 83rd Ave NE/ Whiskey Ridge Rd | Minor Arterial | 35 mph | 2 | No | Sidewalk | Intermittent Bike Lane |
| Morgan Branch Road (40th St NE) | Minor Arterial | 35 mph | 2 | Yes | No | No |
| Soper Hill Rd | Minor Arterial | 35 mph | 2 | No | Sidewalk | No |
| 87th Ave NE | Collector Arterial | 25mph | 2 | Yes | No | No |
| 79th Ave NE | Collector Arterial | 35 mph | 2 | No | No | No |

Note: mph = miles per hour

Planned Improvements

Based on a review of the Washington Department of Transportation (WSDOT) 2023-2026 Statewide Transportation Program (STIP), and the *City of Marysville 2023-2028 Transportation Improvement Plan (TIP)* there are several planned improvements in the area that would impact both capacity at study intersections and travel patterns in the area. The following improvements were funded or partially funded and assumed to be complete by the 2030 horizon year. Note that given the project's near-term year of opening (2024), planned improvement projects were only assumed for the horizon year (2030) analysis.

- **83rd Avenue NE from Soper Hill Road to SR528 (64th St NE):** Widen to three-lane roadway including bicycle lanes and sidewalks. *City of Marysville TIP Number 34.*
- **35th Street NE from 87th Avenue NE to Intersection of SR9/SR92:** New 4-5 lane roadway including pedestrian and bicycle facilities. *City of Marysville TIP Number 49.*
- **40th Street NE:** New 4-5 lane roadway from 83rd Avenue NE to 87th Avenue NE and widen to three lane roadway Sunnyside Blvd to 83rd Ave NE. Include pedestrian and bicycle facilities along entire section Sunnyside to 87th Ave NE. *City of Marysville TIP Number 50 and 35.*
- **87th Avenue NE:** Five-lane cross section between 40th and 35th Street NE; three-lane cross section south of 35th Street NE and between 40th and Sunnyside. Include

a multiuse path along entire section (Sunnyside-Soper Hill Road). *City of Marysville TIP Numbers 37-39.*

In addition to the above planned improvements that were identified through review of local documents, additional planned improvements were included in the analysis that are anticipated to be in place with continued development in the vicinity. These improvements are included in the City's comprehensive plan and traffic model and are consistent with the previous analysis of the full buildout of the White Barn development.

- **44th Street NE Extension** – New roadway connection between 83rd Avenue NE to 87th Avenue NE.
- **87th Avenue NE/35th Street NE:** New two-lane roundabout.
- **SR 9/Soper Hill Road:** Construction of an eastbound left-turn lane.

Also, the planned installation of the roundabout at the 87th Avenue NE/Soper Hill Road intersection has recently been completed and is assumed under existing conditions.

Transit Service

Transit service in the study is provided by Community Transit, route 209. The nearest bus stop to the site is located on SR 9 at Soper Hill Rd. Route 209 provides service between Lake Stevens and Smokey Point along SR 9 and SR 528 within the study area. Service along this route is offered seven days a week with headways of approximately 60 minutes daily.

Non-Motorized

Existing non-motorized facilities in the vicinity of the project are limited. There are intermittent sidewalks available surrounding the project site as well as an intermittent bicycle lane along 83rd Ave NE between Soper Hill Rd and 30th PI NE, west of the project site. Additionally, signalized pedestrian crossings are provided across 3 legs of the adjacent SR 9/Soper Hill Road intersection located southeast of the project.

The City of Marysville has a Priority Pedestrian System Plan which identifies numerous planned additions to the pedestrian access route network within the East Sunnyside-Whiskey Ridge Subarea. Additionally, the City's Bicycle Systems Plan when completed, will provide a comprehensive network of bicycle facilities between the City's residential neighborhoods, the transit system, employment areas, schools, and parks and includes improvements to the arterials and SR 9 within the study area. Specifically, as identified in the planned improvements above, there is a substantial amount of pedestrian infrastructure planned in the vicinity of the proposed project. This includes bicycle lanes and sidewalks planned along 83rd Avenue NE between Soper Hills Road and SR 528, 35th Street NE from 87th Avenue NE to SR 9, 40th Street NE from Sunnyside to 87th Avenue NE as well as a multiuse path along 87th Avenue NE between Sunnyside-Soper Hill Road.

Traffic Volumes

The following sections summarize existing and future (2024 and 2030) without-project traffic volumes within the study area.

Existing

Existing weekday PM peak period traffic volumes were collected in August 2022. Note that a 2 percent annual growth rate was applied to the 2022 traffic counts to estimate the existing 2023 conditions, which is consistent with the growth rate utilized in the horizon year analysis. The existing weekday peak hour traffic volumes at the study intersections are shown in Figure 3. Volumes are rounded to the nearest 5 vehicles to account for the daily fluctuations in traffic volumes. Detailed traffic counts are provided in Appendix A.

Future (2024) Without-Project Traffic Volumes

Future (2024) without-project traffic volumes were forecasted by applying an annual growth rate to existing traffic volumes. An annual growth rate of 3 percent was applied to existing study intersection traffic volumes to estimate the 2024 opening year background traffic growth, consistent with previous studies. No pipeline developments were included in the opening year analysis with the exception of the remainder of the White Barn development. This project was included so that the traffic volumes at the site driveways represent full build-out of the site. The forecast future 2024 without-project weekday peak hour traffic volumes are shown in Figure 4.

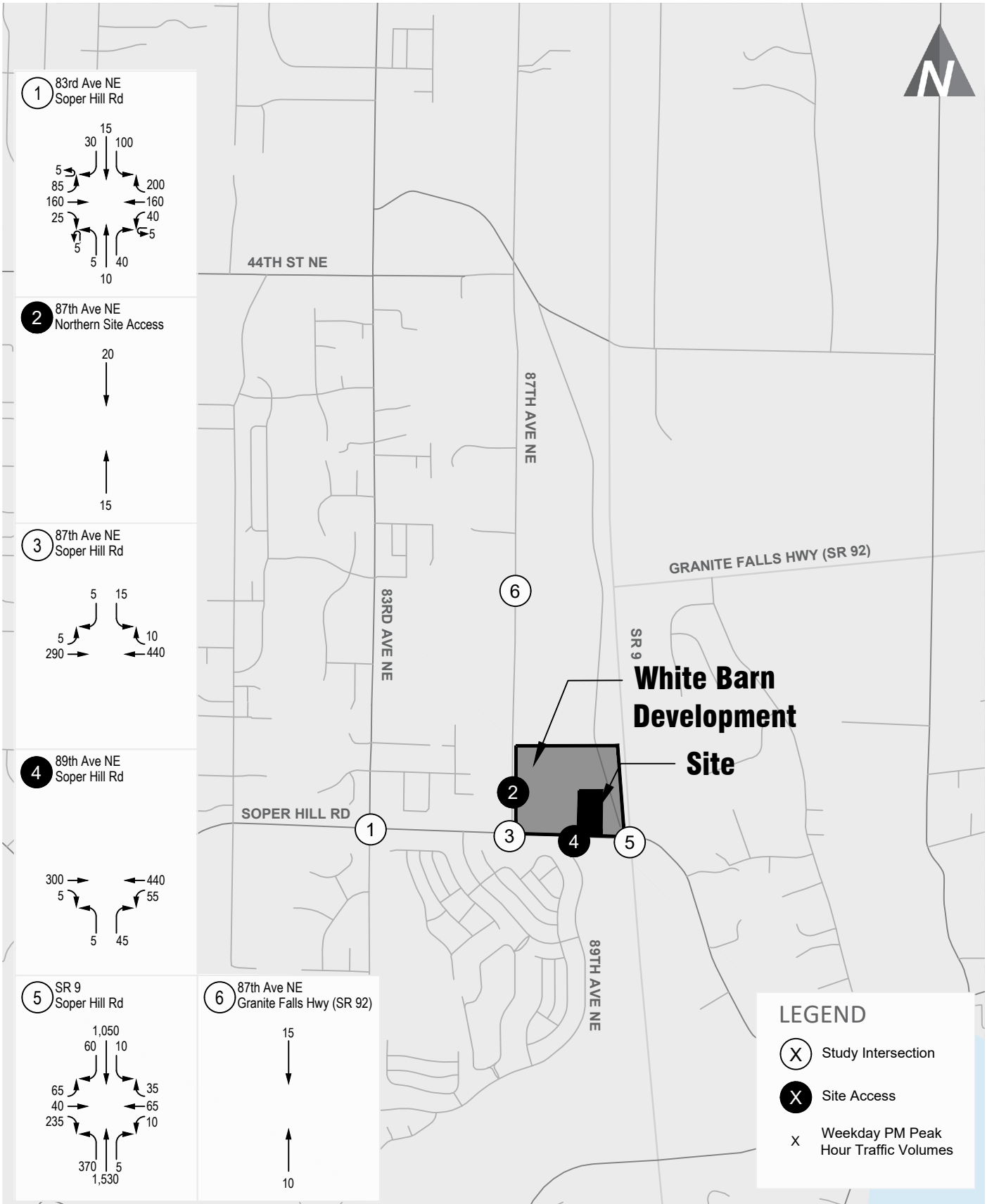
Future (2030) Without-Project Traffic Volumes

Consistent with City requirements and other studies prepared in the area, future (2030) without-project traffic volumes were forecasted by applying a 2 percent annual growth rate to existing traffic volumes and adding traffic from pipeline development projects. The following studies were included in the forecasts as pipeline projects to be completed by 2030.

- GroundHog PRD
- Nordstrom Property
- 87th Assembly
- Hunters Grove
- The Retreat
- Prospector Division 2
- Stevens Ridge
- Firerock
- Havenwood
- Village at WR
- Whiskey Ridge³
- White Barn development – the remainder of the project (i.e. full buildout less the proposed project)

In addition to the above pipeline projects, traffic shifts associated with the 35th Street NE connection planned improvement were also accounted for in the analysis. The forecast future 2030 without-project weekday peak hour traffic volumes are shown in Figure 5.

³ Information included for Whiskey Ridge is based on preliminary information provided to the City of Marysville, as the applicant has not submitted a formal application or initiated the pre-application process.

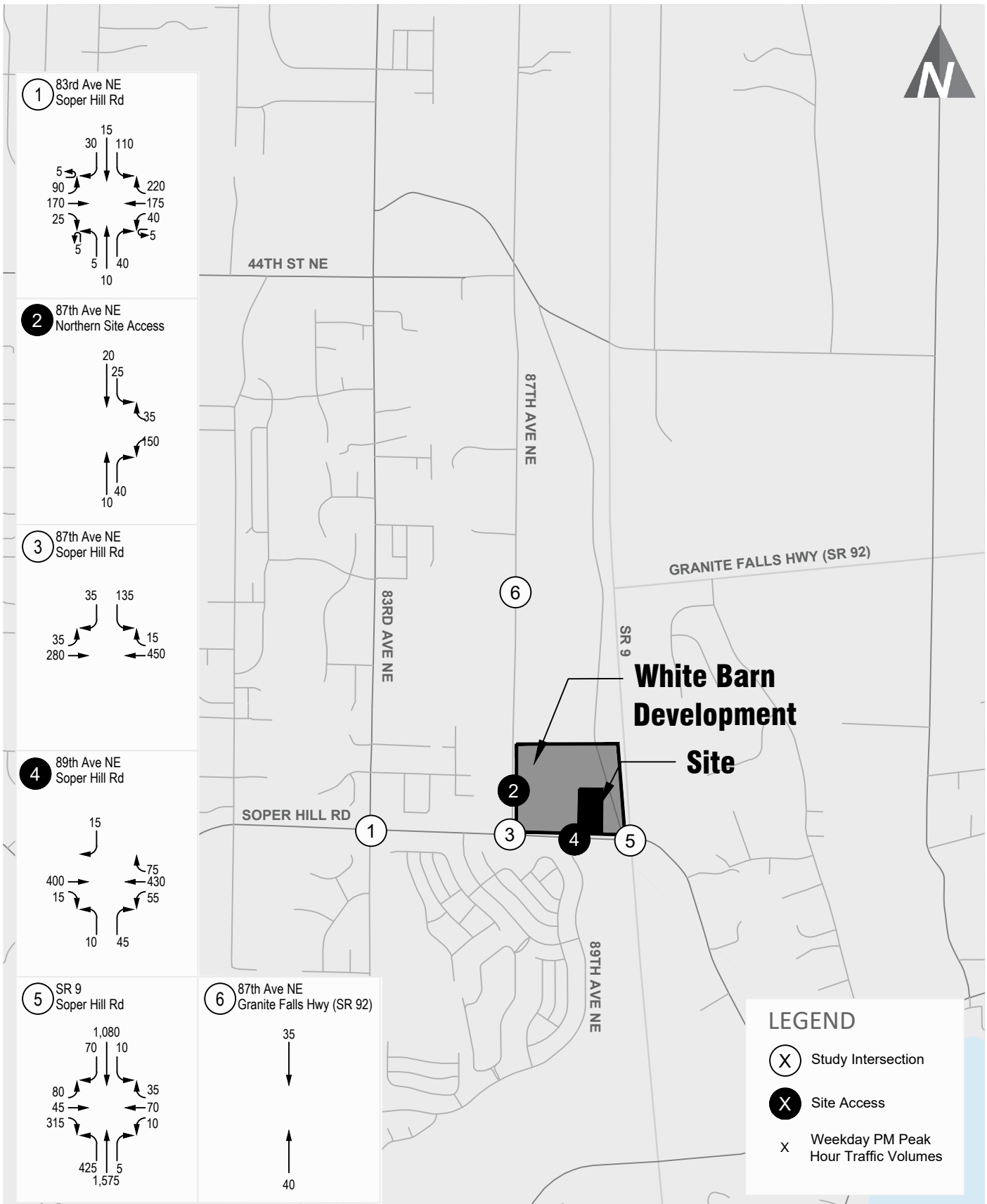


Existing Weekday PM Peak Hour Traffic Volumes

White Barn Brown Bear - Marysville

FIGURE

3

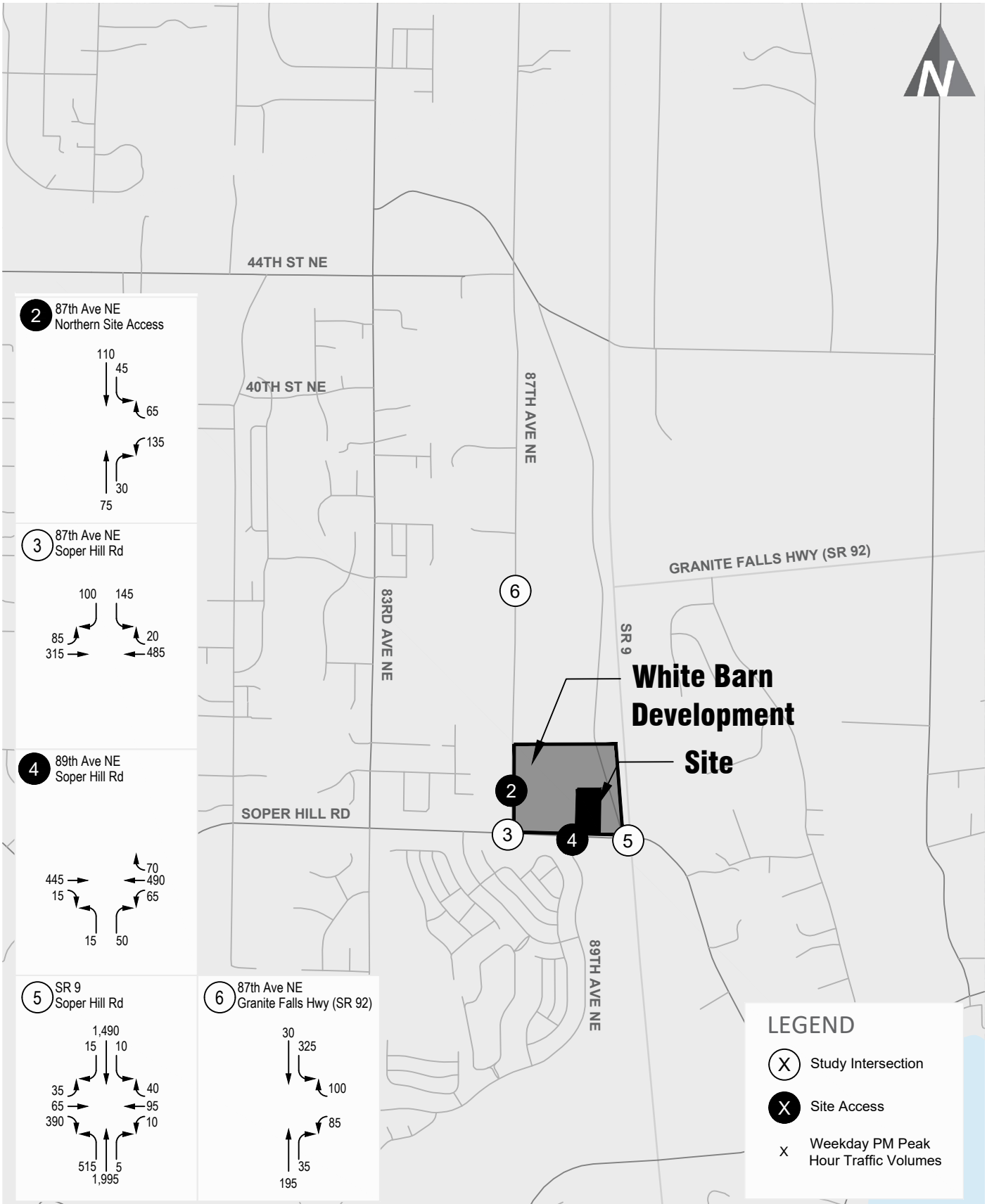


Future (2024) Without-Project PM Peak Hour Traffic Volumes

FIGURE

White Barn Brown Bear - Marysville





Future (2030) Without-Project PM Peak Hour Traffic Volumes **FIGURE 5**

White Barn Brown Bear - Marysville

Traffic Operations

The operational characteristics of an intersection are determined by calculating the intersection level of service (LOS). At signalized and roundabout intersections, LOS is measured in average control delay per vehicle and is typically reported using the intersection delay. At unsignalized side-street, stop-controlled intersections, LOS is measured by the average delay on the worst-movement of the intersection. Traffic operations and average vehicle delay for an intersection can be described qualitatively with a range of levels of service (LOS A through LOS F), with LOS A indicating free-flowing traffic and LOS F indicating extreme congestion and long vehicle delays. Appendix B contains a detailed explanation of LOS criteria and definitions.

The City of Marysville and WSDOT have a LOS D standard at their respective study intersections. For roundabout controlled intersections, WSDOT is targeting a v/c ratio threshold of 0.90 and LOS D.

Signal timing was provided by WSDOT. Analysis parameters such as lane channelization and signal timing were maintained for future (2024) without-project conditions from existing conditions. Under future (2030) without-project conditions, signal timing optimization was applied as well as inclusion of the planned improvements as noted above.

Weekday PM peak hour traffic operations for existing and future without-project conditions were evaluated at the study intersections based on the procedures identified in the *Highway Capacity Manual* 6th Edition for the unsignalized locations and based on HCM 2000 at the signalized study intersection due to limitations of the signal timing parameters. *Synchro 11* was used for the analysis, which is a software program that uses *HCM* methodology to evaluate intersection LOS and average vehicle delays. Roundabout controlled intersections were evaluated utilizing *Sidra 9* and the WSDOT Sidra Policy for analyzing roundabouts. Results for the existing and future without-project operations analyses are summarized in Table 2. Detailed LOS worksheets for each intersection analysis are included in Appendix C.

Table 2. Existing and Future Without-Project PM Peak Hour LOS Summary

| Intersection | Existing/ Future ⁵ Traffic Control | Existing | | | Future (2024) Without- Project | | | Future (2030) Without-Project | | |
|--|--|------------------|--------------------|--|-----------------------------------|-------|--------------|----------------------------------|-------|--------------|
| | | LOS ¹ | Delay ² | WM ³ or V/C ⁴ | LOS | Delay | WM or V/C | LOS | Delay | WM or V/C |
| 1. 83rd Ave NE/Soper Hill Rd | RAB | A | 7 | 0.47 | A | 7 | 0.51 | Not Studied | | |
| 2. 87th Ave NE/Northern Site Access | TWSC | | - | | B | 10 | WB | B | 12 | WB |
| 3. 87th Ave NE/Soper Hill Rd | RAB | A | 4 | 0.40 | A | 6 | 0.42 | A | 7 | 0.46 |
| 4. 89th Ave NE/Soper Hill Rd/ Site Access | TWSC | B | 11 | NB | B | 13 | NB | B | 15 | NB |
| 5. SR 9/Soper Hill Rd | Signal | C | 28 | - | D | 41 | - | D | 47 | - |
| 6. 87th Ave NE/35th St NE | - / RAB | | | <i>Future Intersection</i> | | | | A | 8 | 0.39 |

Note: TWSC = Two-way Stop Controlled, RAB = roundabout.

- LOS = Level of service (A-F), based on 6th Edition *Highway Capacity Manual* with the exception of the traffic signal which is evaluated based on HCM 2000 due to limitations of HCM 6th edition to evaluate the exclusive phases at the SR 9/Soper Hills intersection.
- Delay = Average delay in seconds per vehicle, rounded to the nearest whole second
- WM = Worst movement or approach reported for stop-controlled intersections
- Volume-to-capacity ratio reported for signalized intersections and maximum lane group v/c ratio for roundabout intersections.
- If a planned change in traffic control, future traffic control assumed under the future (2030) horizon year.

As shown in Table 2, all of the study intersections are currently operating at LOS C or better during the weekday PM peak hour, meeting the City's LOS standard. Under the future (2024 and 2030) without-project conditions, the study intersections are forecast to continue operating

acceptably at LOS D or better. Additionally, at the roundabout controlled intersections, the v/c ratios are forecast to operate at 0.51 or lower, meeting the recommended v/c ratio threshold.

Traffic Safety

The five most recent years of collision records (January 1, 2017 and December 31, 2021) provided by the Washington State Department of Transportation (WSDOT) were reviewed within the study area to identify any existing traffic safety issues at the study intersections. A summary of the total and average annual number of reported collisions at the study intersections to the project site are provided in Table 3.

Table 3. Five-Year Collision Summary (2017-2021)

| Location ² | Traffic Control | Number of Collisions | | | | | Total | Annual Average |
|------------------------------|-------------------------|----------------------|------|------|------|------|-------|----------------|
| | | 2017 | 2018 | 2019 | 2020 | 2021 | | |
| 1. 83rd Ave NE/Soper Hill Rd | TWSC / RAB ¹ | 4 | 2 | 6 | 2 | 4 | 18 | 3.60 |
| 3. 87th Ave NE/Soper Hill Rd | TWSC | 0 | 0 | 0 | 0 | 0 | 1 | 0.00 |
| 4. 89th Ave NE/Soper Hill Rd | TWSC | 0 | 0 | 0 | 0 | 2 | 2 | 0.40 |
| 5. SR 9/Soper Hill Rd | Signal | 6 | 6 | 5 | 4 | 7 | 28 | 5.60 |

Source: WSDOT 2022.

Note: TWSC = Two-Way Stop Controlled, RAB = roundabout.

1. A roundabout was installed at the 83rd Avenue NE/Soper Hill Road intersection in 2020.

2. Locations 2 and 6 do not exist during the review period.

As shown in Table 3, there was an average of less than 1 collision per year at the two-way stop-controlled (TWSC) intersections. At the signalized SR 9/Soper Hill Road intersection, there was an average of approximately 6 collisions per year with the majority being property damage only collisions resulting from rear-end collisions. The 83rd Avenue NE/Soper Hill Road intersection had an average of approximately 4 collisions per year but during the study period, the traffic control type changed from TWSC to a roundabout. Prior to the installation of the roundabout, approximately 65 percent of the collisions resulted in injury. Since the installation of the roundabout, the severity of collisions has reduced to approximately 30 percent resulting in injury, which is consistent with the benefits of a roundabout in reducing the severity of collisions.

Within the overall study area, no fatalities were reported nor did any of the collisions reported involve a pedestrian or bicyclist. Based on the collision history review in the study area, no existing safety patterns or issues requiring specific improvements were identified.

Project Impacts

The following sections summarize the proposed project’s impacts on the surrounding street system. First, traffic volumes generated by the proposed project are estimated and then distributed and assigned to adjacent roadways within the study area. Next, project trips are added to future without-project traffic volumes and the potential impact to traffic operations are identified. Site-specific items are also discussed.

Trip Generation

The car wash facility includes an automated car wash tunnel, 5 touchless car wash bays, and 26 vacuuming stalls. Trip generation for the proposed project was calculated based on trip rates identified in the Institute of Transportation Engineers (ITE) *Trip Generation Manual* (11th Edition, 2021) as well as local observations. ITEs Automated Car Wash (LU #948) land use was assumed for the proposed automated tunnel car wash. However, ITE does not contain data applicable to the touchless carwash stations. Trip generation rates applied to touchless bays was based on local data collected at similar facilities as described below. The proposed project also includes vacuuming stations. This use is identified in the rates of both ITE’s automated car wash tunnel land use (LU 948) as well as present and captured within the rate at the observed touchless car washes and therefore included in the overall trip generation estimate for the proposed development.

Touchless Car Wash Trip Generation - Studies were conducted at three existing touchless carwash facilities including:

- Woodinville Aloha Car Wash - 13001 NE 177th Pl, Woodinville, WA 98072
- Mill Creek Aloha Car Wash - 17818 Bothell Everett Hwy, Bothell, WA 98012
- Covington Elephant Car Wash - 27240 168th Pl SE, Covington, WA 98042

All sites are similar to the proposed project with 4-6 touchless carwash bays. Observations at the three sites were conducted during the weekday PM peak period (4-6 p.m.). The observations at the 2 Aloha Car Wash sites were conducted in August 2022 and the Covington observations were conducted in December 2022. The weekday PM peak hour observations are summarized in Table 4.

Table 4. Touchless Carwash Trip Generation Observations

| Site | Date | Weekday PM Peak Hour Trips | | | Percent Inbound | Trip Generation Rate (Trips per bay) |
|-------------------------------------|--------------------|----------------------------|-----|-------|-----------------|---|
| | | In | Out | Total | | |
| Woodinville (4 bays) | Tues - 8/2/2022 | 35 | 34 | 69 | 51% | 17.25 |
| | Wed - 8/3/2022 | 36 | 33 | 69 | 52% | 17.25 |
| Mill Creek (4 bays) | Tues - 8/2/2022 | 32 | 29 | 61 | 52% | 15.25 |
| | Wed - 8/3/2022 | 23 | 26 | 49 | 47% | 12.25 |
| Covington (6 bays) | Wed – 12/14/2022 | 41 | 33 | 74 | 55% | 14.80 |
| | Thurs – 12/15/2022 | 31 | 30 | 61 | 51% | 10.17 |
| Weighted Average¹ | | | | | 51% | 13.68 |

1. Per ITE’s *Trip Generation Manual 11th Edition Desk Reference* (page 16) “the weighted average number of vehicle or person trips entering or exiting a development site per one unit of the independent variable. It is calculated by dividing the sum of all trips for all contributing data point sites by the sum of all independent variable units for all contributing data point sites. The weighted average rate is used rather than the average of the individual rates because of the variance within each data set or generating unit. Data sets with a large variance will over-influence the average rate if they are not weighted. The data plot includes a dashed line corresponding to the weighted average rate, extending between the lowest and highest independent variable values for data points.”

Table 4 shows the observed weekday PM peak hour trips generated by the existing touchless car wash sites and the resulting weighted average trip generation rate of 13.68 trips per bay for the touchless car wash.

Consistent with gas stations and other retail services, pass-by trips are a component of the trip generation. Pass-by trips reflect traffic already on streets in the vicinity of the project site that would visit the project while driving by the site on the way to its final destination. Although, specific car wash pass-by studies were not available, pass-by rates for similar “service” and retail uses were reviewed as available in ITE’s *Trip Generation Manual* (11th Edition). ITE’s retail and service uses (Land Use 821 and 900’s) with studies available show PM peak hour pass-by rates ranging from 35 to 98 percent. Specifically, the Gasoline/Service Station (LU 944) land use description identifies that car washes may be included within the use and has a weekday PM peak hour pass-by rate of 57 percent and Shopping Center (LU 821) which includes a range of general retail land uses has a pass-by rate of 40 percent. Based on the review of available data, the pass-by rate was assumed to be 40 percent, consistent with general retail (LU 821). The shopping center pass-by rate was assumed because it is on the lower end of the range of identified pass-by rates, is less than the pass-by rate for the Gasoline/Service Station (LU 944) land use (providing a conservative estimate as this land use specifically identifies a car wash), and the project is located within the larger White Barn commercial development.

Table 5 summarizes the weekday PM peak hour vehicle trips generated by the proposed project. The detailed trip generation calculations are included in Appendix D.

Table 5. Estimated Weekday PM Peak Hour Vehicle Trip Generation

| Land Use ¹ | Size | Gross Trips | Pass-by | | Net New Trips | | |
|---------------------------------|----------|-------------|---------|-----------|---------------|-----------|-----------|
| | | | % | Trips | In | Out | Total |
| Automated Car Wash (LU 948) | 1 tunnel | 78 | 40% | 32 | 23 | 23 | 46 |
| Touchless Car Wash ² | 5 bays | 68 | 40% | 28 | 21 | 19 | 40 |
| Total | | 146 | | 60 | 44 | 42 | 86 |

Note: sf = square feet

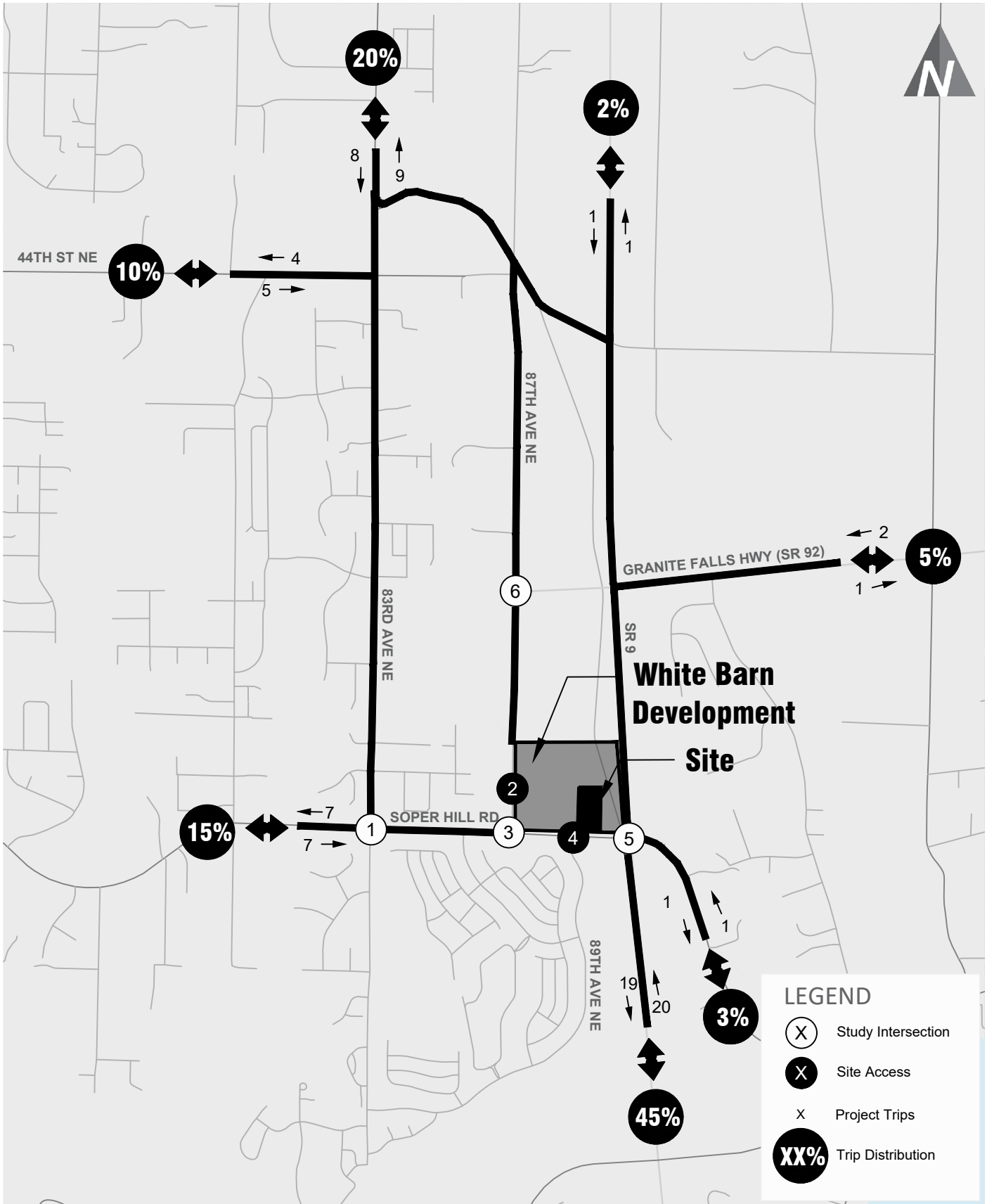
1. Average trip rates from ITE *Trip Generation Manual*, 11th Edition (2021).

2. Based on observations conducted at local touchless car washes with similar sizes.

As shown in Table 5, the proposed project is estimated to generate 86 new trips occurring in the PM peak hour with 146 gross trips at the project driveways.

Trip Distribution & Assignment

The weekday PM peak hour vehicular trips associated with the project were distributed to the roadway network. City of Marysville staff provided distribution patterns for the site vicinity based on their travel demand model. Their model reflected the future connections and planned improvements as identified above and therefore was assumed for the future 2030 project trip distribution. For the future (2024) opening year, the distribution was based on the City’s model with local adjustments to reflect the current roadway network. The project trip distributions and weekday PM peak hour assignment are shown in Figure 6 and Figure 7 for the future 2024 and 2030 years, respectively.



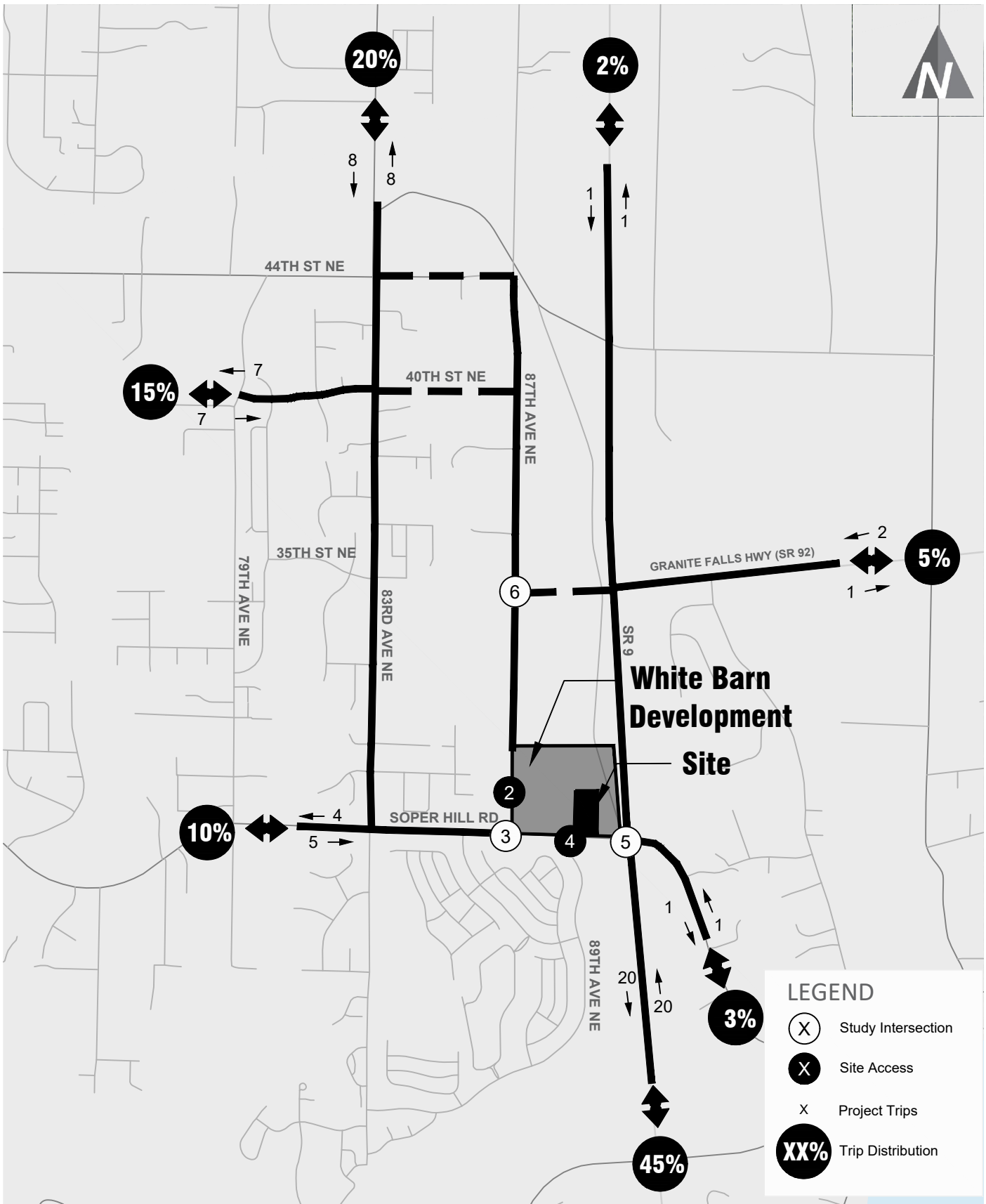
Future (2024) Project Trip Distribution and Assignment

FIGURE

White Barn Brown Bear - Marysville



6



Future (2030) Project Trip Distribution and Assignment

FIGURE

White Barn Brown Bear - Marysville



Traffic Volume Impact

Site generated weekday peak hour traffic volumes were added to future without-project volumes at study intersections. The resulting future (2024 and 2030) with-project peak hour traffic volumes are illustrated in Figure 8 and Figure 9, respectively. Table 6 summarizes the anticipated increase in total entering traffic at the study intersections as well as the percent of future with-project traffic volumes attributable to the proposed project.

Table 6. PM Peak Hour Traffic Volume Impacts at Study Intersections

| Intersection | 2024 TEV | | | 2024 Percent Project Share | 2030 TEV | | | 2030 Percent Project Share |
|--|---------------------|------------------|------------------|-------------------------------------|---------------------|------------------|------------------|-------------------------------------|
| | Without- Project | Project Trips | With- Project | | Without- Project | Project Trips | With- Project | |
| 1. 83rd Ave NE/Soper Hill Rd | 945 | 31 | 976 | 3.2% | 1,155 | 17 | 1,172 | 1.5% |
| 2. 87th Ave NE/Northern Site Access | 280 | 79 | 359 | 22.0% | 460 | 87 | 547 | 15.9% |
| 3. 87th Ave NE/Soper Hill Rd | 950 | 69 | 1,019 | 6.8% | 1,150 | 53 | 1,203 | 4.4% |
| 4. 89th Ave NE/Soper Hill Rd/Site Access | 1,045 | 75 | 1,120 | 6.7% | 1,150 | 65 | 1,215 | 5.3% |
| 5. SR 9/Soper Hill Rd | 3,720 | 45 | 3,765 | 1.2% | 4,665 | 42 | 4,707 | 0.9% |
| 6. 87th Ave NE/35th St NE | 75 | 10 | 85 | 11.8% | 770 | 27 | 797 | 3.4% |
| Not Studied: | | | | | | | | |
| 83rd Ave NE/44th St NE | - | 17 | - | - | - | 16 | - | - |

Note: TEV = Total Entering. Shading indicates not impacted by 25 trips.

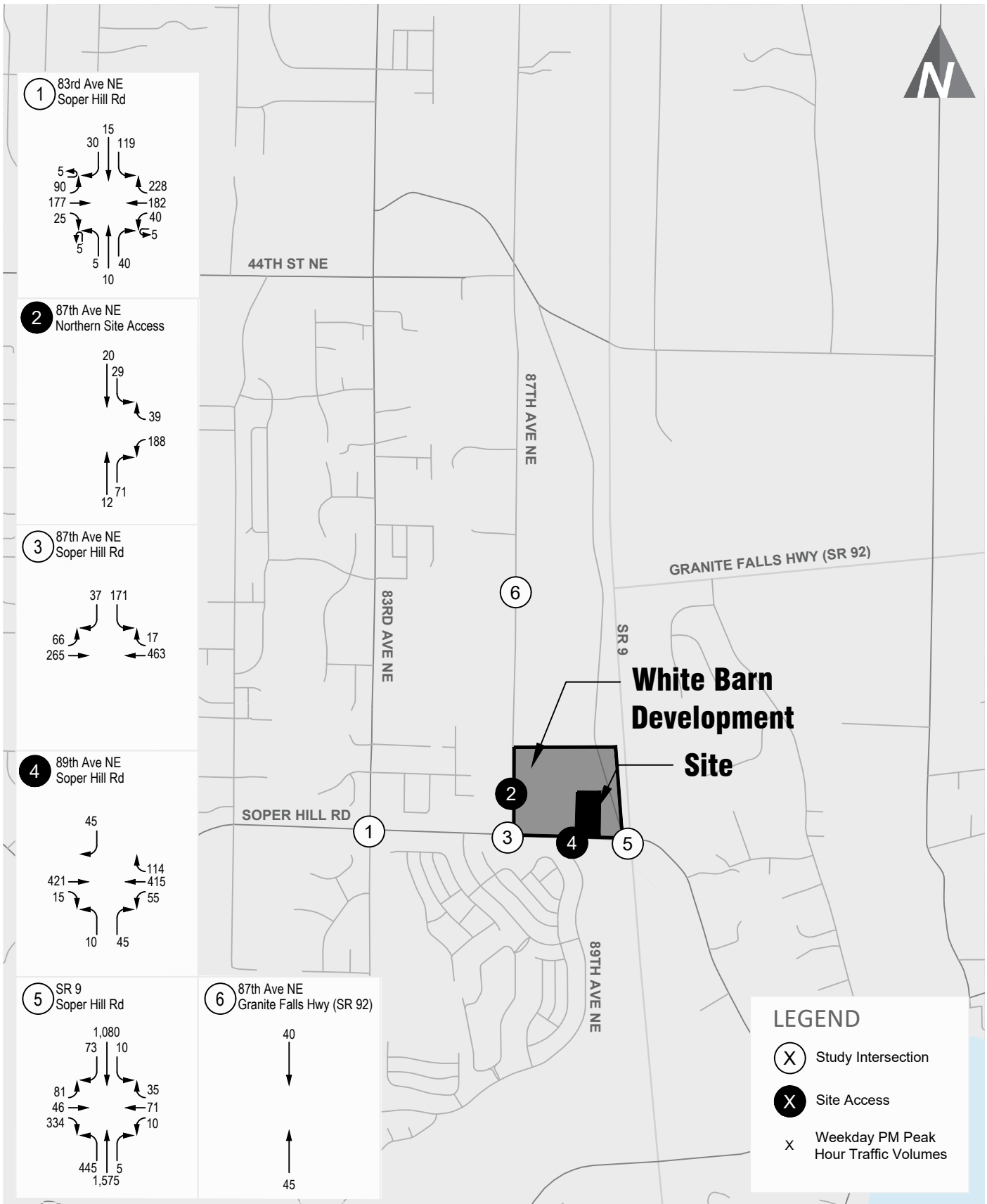
1. LOS = Level of service (A-F), based on 6th Edition Highway Capacity Manual and Highway Capacity Manual 2000 methodology.

2. Delay = Average delay in seconds per vehicle, rounded to the nearest whole second

3. WM = Worst movement or approach reported for stop-controlled intersections

4. Volume-to-capacity ratio reported for signalized intersections and maximum lane group v/c ratio for roundabout intersections.

As shown in Table 6, the project generated traffic volumes are anticipated to be approximately 7 percent or less within the study area during the PM peak hour under the future (2024) opening year with the exception of the site access intersections. With continued future growth in the vicinity of the proposed project by 2030, the project generated traffic volumes are anticipated to decrease to approximately 5 percent or less within the study area during the PM peak hour at the off-site study intersections.



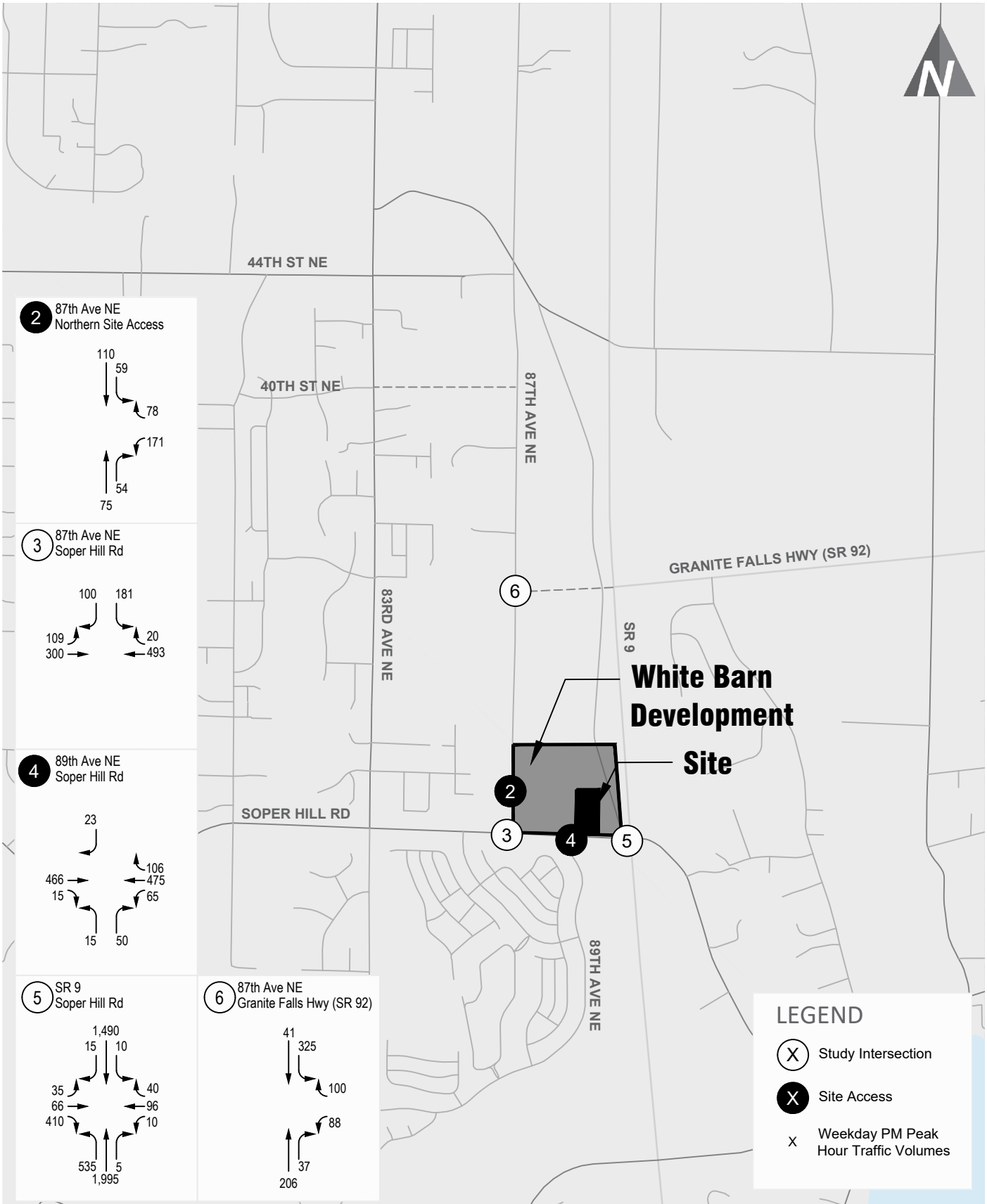
Future (2024) With-Project PM Peak Hour Traffic Volumes

White Barn Brown Bear - Marysville

FIGURE

8





Future (2030) With-Project PM Peak Hour Traffic Volumes

White Barn Brown Bear - Marysville

FIGURE

9

Traffic Operations Impact

The following section summarizes both the future (2024 and 2030) with-project analysis years during the weekday PM peak hour to identify traffic impacts of the proposed project.

The same methodologies were applied as described for future without-project conditions. All intersection parameters such as channelization, intersection control, and signal timing were consistent with those used in the evaluation of future without-project conditions for the respective analysis years. A comparison of future (2024) without-project and with-project weekday PM peak hour traffic operations is summarized in Table 7 and a comparison of the future (2030) without-project and with-project weekday PM peak hour traffic operations is summarized in Table 8. Detailed LOS worksheets are provided in Appendix C.

Note that based on the City's 25 project trip threshold, the 87th Avenue NE/35th Street NE intersection (study intersection 6) and 83rd Avenue NE/Soper Hill Road intersection (study intersection 1) are not evaluated under future (2024) and future (2030) conditions, respectively.

Table 7. Future (2024) Opening Year Weekday Peak Hour LOS Summary

| Intersection | Traffic Control | 2024 Without-Project | | | 2024 With-Project | | |
|--|-----------------|----------------------|--------------------|-----------------|-------------------|-------|------|
| | | LOS ¹ | Delay ² | WM ³ | LOS | Delay | WM |
| 1. 83rd Ave NE/Soper Hill Rd | Roundabout | A | 7 | 0.51 | A | 7 | 0.53 |
| 2. 87th Ave NE/Northern Site Access | TWSC | B | 10 | WB | B | 10 | WB |
| 3. 87th Ave NE/Soper Hill Rd | Roundabout | A | 6 | 0.42 | A | 7 | 0.45 |
| 4. 89th Ave NE/Soper Hill Rd/Site Access | TWSC | B | 13 | NB | B | 14 | NB |
| 5. SR 9/Soper Hill Rd | Traffic Signal | D | 41 | - | D | 44 | - |

Note: TWSC = two-way stop control

1. LOS = Level of service (A-F), based on 6th Edition Highway Capacity Manual at unsignalized intersections and Highway Capacity Manual 2000 methodology at signalized locations.

2. Delay = Average delay in seconds per vehicle, rounded to the nearest whole second

3. WM = Worst movement or approach reported for stop-controlled intersections

4. Volume-to-capacity ratio reported for signalized intersections and maximum lane group v/c ratio for roundabout intersections.

As shown in Table 7, with the addition of project traffic, under future (2024) conditions during the weekday PM peak hour all of the study intersections are forecast to continue operating at LOS D or better and meeting the LOS D standard. Additionally, the roundabouts are forecast to operate with v/c ratios of 0.53 or lower, meeting the recommended v/c ratio.

Table 8. Future (2030) Horizon Year Weekday Peak Hour LOS Summary

| Intersection | Traffic Control | 2030 Without-Project | | | 2030 With-Project | | |
|--|-----------------|----------------------|--------------------|-----------------|-------------------|-------|------|
| | | LOS ¹ | Delay ² | WM ³ | LOS | Delay | WM |
| 2. 87th Ave NE/Northern Site Access | TWSC | B | 12 | WB | B | 13 | WB |
| 3. 87th Ave NE/Soper Hill Rd | Roundabout | A | 7 | 0.46 | A | 8 | 0.49 |
| 4. 89th Ave NE/Soper Hill Rd/Site Access | TWSC | B | 15 | NB | C | 15 | NB |
| 5. SR 9/Soper Hill Rd | Traffic Signal | D | 47 | - | D | 53 | - |
| 6. 87th Ave NE/35th St NE | Roundabout | A | 8 | 0.39 | A | 8 | 0.41 |

Note: TWSC = two-way stop control

1. LOS = Level of service (A-F), based on 6th Edition Highway Capacity Manual and Highway Capacity Manual 2000 methodology.

2. Delay = Average delay in seconds per vehicle, rounded to the nearest whole second

3. WM = Worst movement or approach reported for stop-controlled intersections

4. Volume-to-capacity ratio reported for signalized intersections and maximum lane group v/c ratio for roundabout intersections.

As shown in Table 8, with the addition of project traffic, under future (2030) conditions during the weekday PM peak hour all of the study intersections are forecast to continue operating at LOS D or better and meeting the LOS D standard. Additionally, the roundabouts are forecast to operate with v/c ratios of 0.49 or lower, meeting the recommended v/c ratio.

Site Access Evaluation

As noted above, access for the site is provided via existing connections to Soper Hill Road and 87th Ave NE. The site access operations, on-site queueing, and parking are reviewed in the sections below.

Site Access Traffic Operations

The operations at the driveways were evaluated in the analysis above and are summarized in Tables 7 and 8 for the 2024 and 2030 conditions during the weekday PM peak hour. As shown above, the site accesses are forecast to operate at LOS C with the development of the project during the weekday PM peak hour under both future (2024 and 2030) conditions. This analysis considers full-build-out of the White Barn uses as permitted to date and future uses identified in the original TIA prepared for that project.

Queueing

Queues were evaluated for both the automated car wash tunnel as well as for the touchless car wash bays using a Poisson queuing distribution. Service times for the car wash were observed during the touchless car wash study to be 6 minutes on average. Based on discussions with Brown Bear, the service time for the automated tunnel is less than 6 minutes, such that a service time of 6 minutes for the automated tunnel provides a conservative estimate. The weekday PM peak hour inbound trips were used for the analysis. The analysis parameters assumed for each car wash type are summarized below:

- Touchless Car Wash: 35 vehicles, 5 bays (equivalent of 7 vehicles per bay) 6-minute service time
- Automated Car Wash: 39 vehicles, 1 tunnel, 6-minute service time

Based on the Poisson queuing analysis, each car wash type is estimated to have a 95th percentile queue of 8 vehicles during the PM peak hour. As shown in Figure 2, the automated car wash queuing area can accommodate that estimated queue (showing a queue of greater than 22 vehicles is able to be accommodated). The touchless queue of up to 8 vehicles would reflect 5 vehicles actively using the bays as well as 3 vehicles queued to use the bays at the pay stations. The detailed queuing analysis is provided in Appendix E.

Parking

The proposed project includes 12 on-site parking stalls; however, the parking demand for the proposed development is anticipated to be very limited and predominantly related to on-site employees. The users of the car washes are provided queueing areas as reviewed above. The users of the vacuuming stalls are provided separate stalls from the proposed parking to accommodate their service. The proposed 12 on-site parking stalls is anticipated to accommodate the project's peak parking demands.

Mitigation

The project would pay traffic impact fees to the City of Marysville. The City has identified a traffic impact fee of \$2,220 per PM peak hour trip.⁵ Based on the estimated trip generation above, the project is anticipated to generate 86 new weekday PM peak hour trips, which equates to an estimated traffic impact fee of \$190,920. The City will calculate the final fee at time of permit issuance. The fee will be based on the impact fee rates in effect at the time of building permit issuance.

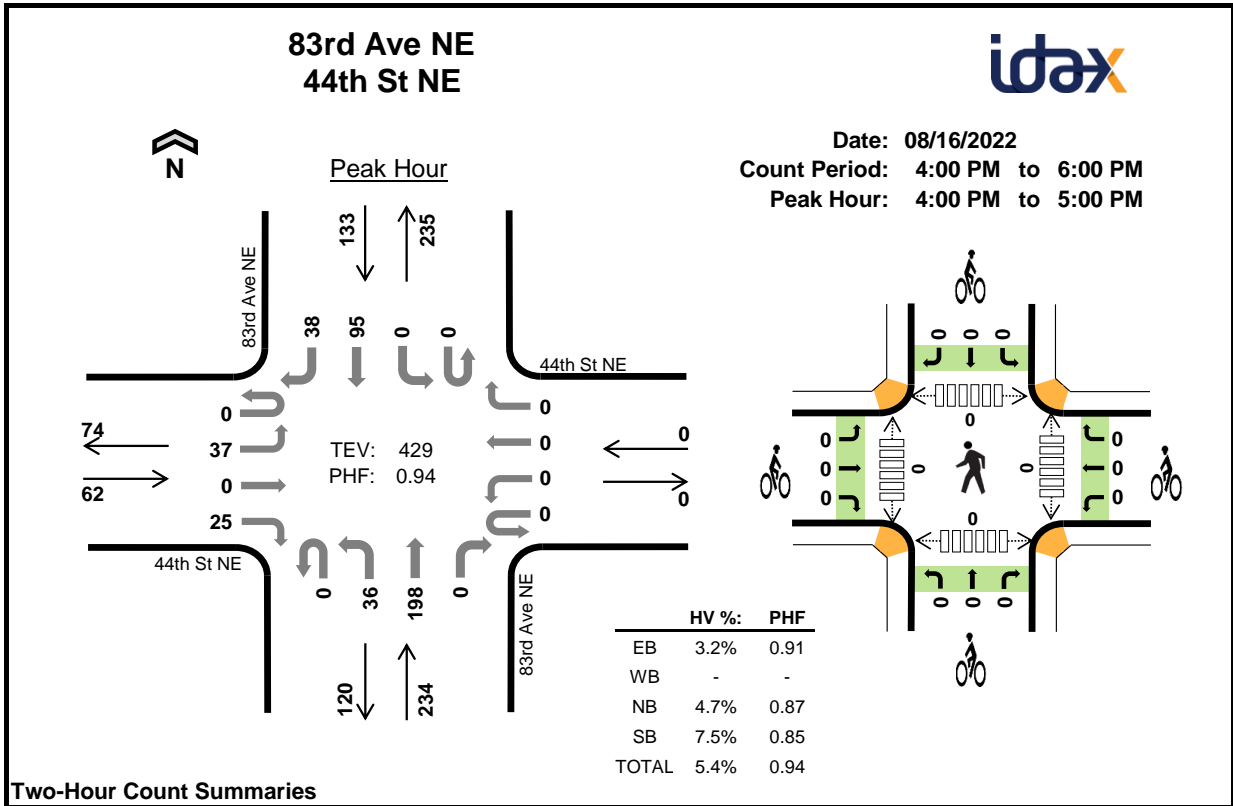
⁵ Traffic impact fee per *City of Marysville Traffic Analysis and Mitigation*

Findings and Recommendations

This traffic impact analysis summarizes the project traffic impacts of the proposed Brown Bear project located within the White Barn development. General findings and recommendations include:

- The proposed project would construct 5 touchless car wash bays, 1 automated tunnel, and 26 vacuuming stalls.
- The development is anticipated to generate approximately 86 new trips during the PM peak hour.
- The off-site intersections and driveways are forecast to operate acceptably at LOS D or better under both existing and future (2024 and 2030) conditions during the weekday PM peak hour, meeting Marysville's LOS D standard.
- Queueing associated with the proposed car wash development is anticipated to be accommodated on-site.
- The City would calculate the final fee for the project at the time of permits being issued. The preliminary traffic fee estimate is \$190,920.

Appendix A: Traffic Counts



Two-Hour Count Summaries

| Interval Start | 44th St NE Eastbound | | | | 44th St NE Westbound | | | | 83rd Ave NE Northbound | | | | 83rd Ave NE Southbound | | | | 15-min Total | Rolling One Hour | |
|----------------|----------------------|----|----|----|----------------------|----|----|----|------------------------|----|-----|-----|------------------------|----|-----|----|--------------|------------------|---|
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | | |
| 4:00 PM | 0 | 11 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 12 | 55 | 0 | 0 | 0 | 24 | 9 | 114 | 0 | |
| 4:15 PM | 0 | 10 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 7 | 51 | 0 | 0 | 0 | 26 | 10 | 109 | 0 | |
| 4:30 PM | 0 | 8 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 8 | 48 | 0 | 0 | 0 | 28 | 11 | 112 | 0 | |
| 4:45 PM | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 9 | 44 | 0 | 0 | 0 | 17 | 8 | 94 | 429 | |
| 5:00 PM | 0 | 16 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 9 | 40 | 0 | 0 | 0 | 28 | 13 | 110 | 425 | |
| 5:15 PM | 0 | 4 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 2 | 54 | 0 | 0 | 0 | 23 | 6 | 95 | 411 | |
| 5:30 PM | 0 | 10 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 6 | 50 | 0 | 0 | 0 | 21 | 10 | 106 | 405 | |
| 5:45 PM | 0 | 9 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 7 | 33 | 1 | 0 | 0 | 23 | 7 | 84 | 395 | |
| Count Total | 0 | 76 | 1 | 47 | 0 | 0 | 0 | 0 | 0 | 60 | 375 | 1 | 0 | 0 | 190 | 74 | 824 | 0 | |
| Peak Hour | All | 0 | 37 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 36 | 198 | 0 | 0 | 0 | 95 | 38 | 429 | 0 |
| | HV | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 6 | 4 | 23 | 0 |
| | HV% | - | 5% | - | 0% | - | - | - | - | - | 3% | 5% | - | - | - | 6% | 11% | 5% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals | | | | | Bicycles | | | | | Pedestrians (Crossing Leg) | | | | |
|----------------|----------------------|----|----|----|-------|----------|----|----|----|-------|----------------------------|------|-------|-------|-------|
| | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 1 | 0 | 3 | 5 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 3 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 1 | 0 | 4 | 2 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 1 | 0 | 1 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 3 | 0 | 15 | 12 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 2 | 0 | 11 | 10 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Two-Hour Count Summaries - Heavy Vehicles | | | | | | | | | | | | | | | | | | | |
|--|------------|----|----|----|------------|----|----|----|-------------|----|----|----|-------------|----|----|----|--------------|------------------|---|
| Interval Start | 44th St NE | | | | 44th St NE | | | | 83rd Ave NE | | | | 83rd Ave NE | | | | 15-min Total | Rolling One Hour | |
| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | | | |
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | | |
| 4:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 3 | 2 | 9 | 0 | |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 1 | 5 | 0 | |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 2 | 7 | 0 | |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 23 | |
| 5:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 4 | 18 | |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 14 | |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | |
| Count Total | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 | 0 | 0 | 0 | 7 | 5 | 30 | 0 |
| Peak Hour | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 6 | 4 | 23 | 0 |

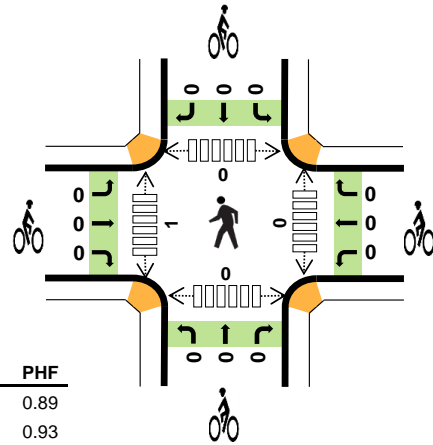
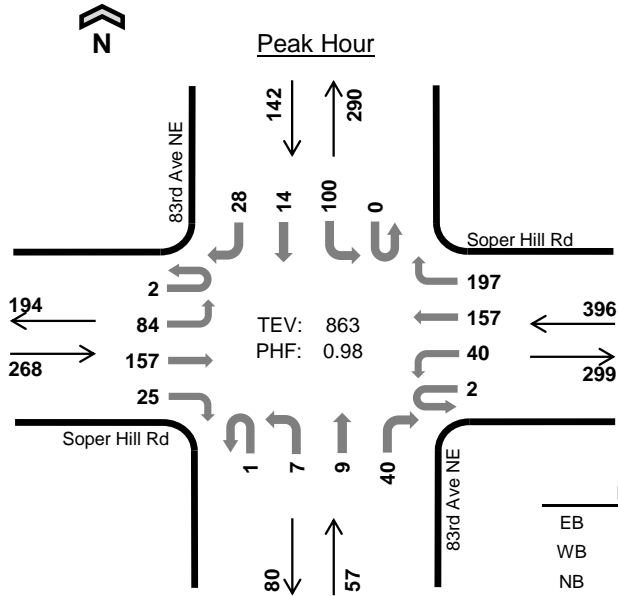
| Two-Hour Count Summaries - Bikes | | | | | | | | | | | | | | | | | | |
|---|------------|----|----|------------|----|----|-------------|----|----|-------------|----|----|--------------|------------------|---|---|---|---|
| Interval Start | 44th St NE | | | 44th St NE | | | 83rd Ave NE | | | 83rd Ave NE | | | 15-min Total | Rolling One Hour | | | | |
| | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | | | | | | |
| | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | | | | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

83rd Ave NE Soper Hill Rd



Date: 08/16/2022
 Count Period: 4:00 PM to 6:00 PM
 Peak Hour: 4:30 PM to 5:30 PM



| | HV %: | PHF |
|-------|-------|------|
| EB | 2.2% | 0.89 |
| WB | 1.3% | 0.93 |
| NB | 3.5% | 0.89 |
| SB | 2.1% | 0.91 |
| TOTAL | 1.9% | 0.98 |

Two-Hour Count Summaries

| Interval Start | Soper Hill Rd Eastbound | | | | Soper Hill Rd Westbound | | | | 83rd Ave NE Northbound | | | | 83rd Ave NE Southbound | | | | 15-min Total | Rolling One Hour | |
|----------------|-------------------------|-----------|-----------|----------|-------------------------|-----------|-----------|-----------|------------------------|----------|----------|----------|------------------------|-----------|----------|----------|--------------|------------------|---|
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | | |
| 4:00 PM | 0 | 33 | 33 | 4 | 0 | 11 | 38 | 52 | 0 | 2 | 0 | 6 | 0 | 29 | 3 | 7 | 218 | 0 | |
| 4:15 PM | 0 | 18 | 27 | 5 | 1 | 6 | 30 | 49 | 0 | 5 | 2 | 6 | 0 | 20 | 3 | 9 | 181 | 0 | |
| 4:30 PM | 0 | 28 | 38 | 9 | 1 | 11 | 36 | 44 | 0 | 2 | 4 | 9 | 0 | 27 | 3 | 9 | 221 | 0 | |
| 4:45 PM | 1 | 18 | 43 | 7 | 1 | 12 | 39 | 55 | 1 | 0 | 0 | 12 | 0 | 24 | 2 | 3 | 218 | 838 | |
| 5:00 PM | 0 | 16 | 43 | 7 | 0 | 7 | 36 | 47 | 0 | 1 | 4 | 8 | 0 | 25 | 3 | 8 | 205 | 825 | |
| 5:15 PM | 1 | 22 | 33 | 2 | 0 | 10 | 46 | 51 | 0 | 4 | 1 | 11 | 0 | 24 | 6 | 8 | 219 | 863 | |
| 5:30 PM | 0 | 21 | 29 | 9 | 0 | 10 | 34 | 54 | 0 | 4 | 1 | 8 | 0 | 36 | 0 | 8 | 214 | 856 | |
| 5:45 PM | 0 | 23 | 28 | 8 | 0 | 8 | 20 | 37 | 0 | 2 | 5 | 5 | 0 | 34 | 3 | 7 | 180 | 818 | |
| Count Total | 2 | 179 | 274 | 51 | 3 | 75 | 279 | 389 | 1 | 20 | 17 | 65 | 0 | 219 | 23 | 59 | 1,656 | 0 | |
| Peak Hour | All | 2 | 84 | 157 | 25 | 2 | 40 | 157 | 197 | 1 | 7 | 9 | 40 | 0 | 100 | 14 | 28 | 863 | 0 |
| | HV | 0 | 3 | 2 | 1 | 0 | 0 | 1 | 4 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 16 | 0 |
| | HV% | 0% | 4% | 1% | 4% | 0% | 0% | 1% | 2% | 0% | 14% | 0% | 3% | - | 0% | 0% | 11% | 2% | 0 |

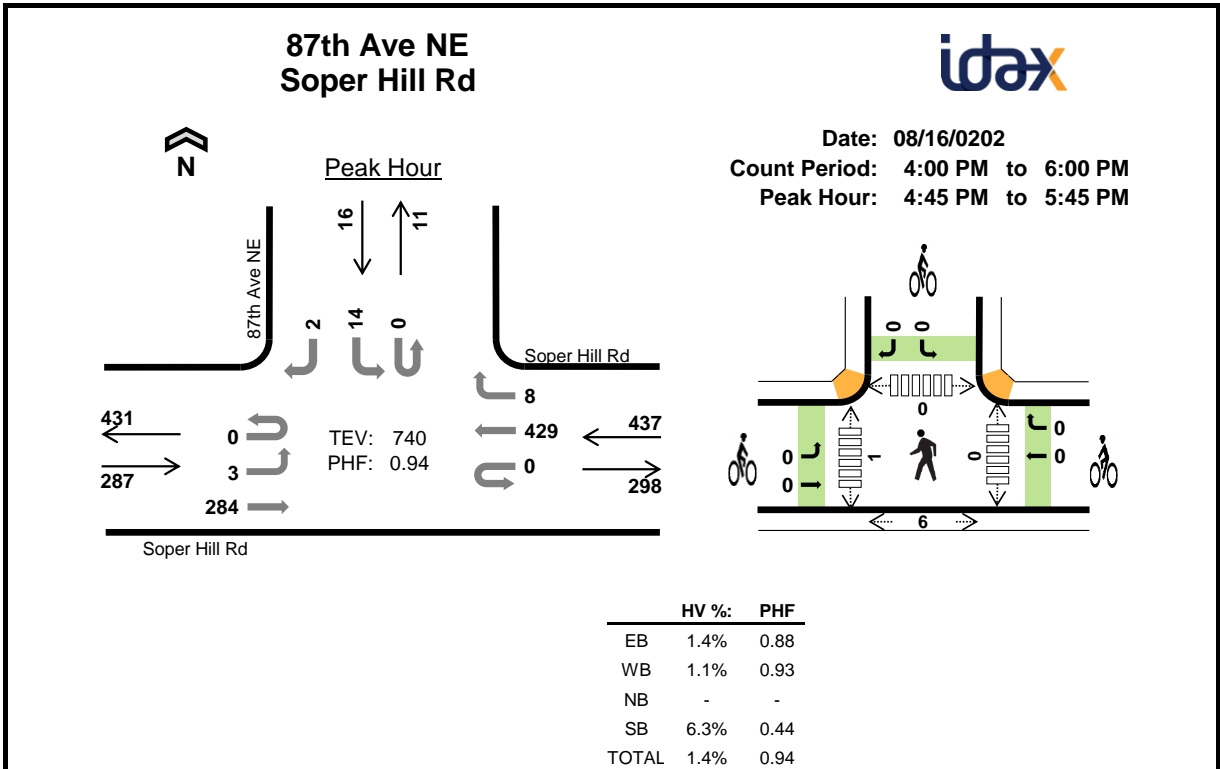
Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals | | | | | Bicycles | | | | | Pedestrians (Crossing Leg) | | | | |
|----------------|----------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------------------------|----------|----------|----------|----------|
| | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 2 | 1 | 1 | 4 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 4 |
| 4:15 PM | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 3 |
| 4:30 PM | 3 | 1 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 2 | 2 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:00 PM | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 2 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 |
| 5:45 PM | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 10 | 7 | 5 | 8 | 30 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 3 | 0 | 10 |
| Peak Hour | 6 | 5 | 2 | 3 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |

| Two-Hour Count Summaries - Heavy Vehicles | | | | | | | | | | | | | | | | | | |
|--|---------------|----------|----------|----------|---------------|----------|----------|----------|-------------|----------|----------|----------|-------------|----------|----------|----------|--------------|------------------|
| Interval Start | Soper Hill Rd | | | | Soper Hill Rd | | | | 83rd Ave NE | | | | 83rd Ave NE | | | | 15-min Total | Rolling One Hour |
| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | | |
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 2 | 8 | 0 |
| 4:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 |
| 4:30 PM | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 |
| 4:45 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 20 |
| 5:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 14 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 16 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 12 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 10 |
| Count Total | 0 | 6 | 3 | 1 | 0 | 1 | 1 | 5 | 0 | 1 | 0 | 4 | 0 | 2 | 0 | 6 | 30 | 0 |
| Peak Hour | 0 | 3 | 2 | 1 | 0 | 0 | 1 | 4 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 16 | 0 |

| Two-Hour Count Summaries - Bikes | | | | | | | | | | | | | | | | | |
|---|---------------|----------|----------|---------------|----------|----------|-------------|----------|----------|-------------|----------|----------|--------------|------------------|----------|----------|----------|
| Interval Start | Soper Hill Rd | | | Soper Hill Rd | | | 83rd Ave NE | | | 83rd Ave NE | | | 15-min Total | Rolling One Hour | | | |
| | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | | | | | |
| | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | | | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.



Two-Hour Count Summaries

| Interval Start | Soper Hill Rd Eastbound | | | | Soper Hill Rd Westbound | | | | 0 Northbound | | | | 87th Ave NE Southbound | | | | 15-min Total | Rolling One Hour | |
|----------------|-------------------------|----|-----|-----|-------------------------|----|-----|-----|--------------|----|----|----|------------------------|----|----|----|--------------|------------------|---|
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | | |
| 4:00 PM | 0 | 0 | 72 | 0 | 0 | 0 | 107 | 5 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 187 | 0 | |
| 4:15 PM | 0 | 1 | 59 | 0 | 0 | 0 | 93 | 2 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 159 | 0 | |
| 4:30 PM | 0 | 0 | 76 | 0 | 0 | 0 | 96 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 178 | 0 | |
| 4:45 PM | 0 | 1 | 81 | 0 | 0 | 0 | 111 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 197 | 721 | |
| 5:00 PM | 0 | 0 | 74 | 0 | 0 | 0 | 92 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 172 | 706 | |
| 5:15 PM | 0 | 1 | 61 | 0 | 0 | 0 | 117 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 183 | 730 | |
| 5:30 PM | 0 | 1 | 68 | 0 | 0 | 0 | 109 | 1 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 1 | 188 | 740 | |
| 5:45 PM | 0 | 0 | 71 | 0 | 0 | 0 | 66 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 141 | 684 | |
| Count Total | 0 | 4 | 562 | 0 | 0 | 0 | 791 | 20 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 4 | 1,405 | 0 | |
| Peak Hour | All | 0 | 3 | 284 | 0 | 0 | 0 | 429 | 8 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 2 | 740 | 0 |
| | HV | 0 | 1 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 | 0 |
| | HV% | - | 33% | 1% | - | - | - | 1% | 0% | - | - | - | - | - | 0% | - | 50% | 1% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals | | | | | Bicycles | | | | | Pedestrians (Crossing Leg) | | | | |
|----------------|----------------------|----|----|----|-------|----------|----|----|----|-------|----------------------------|------|-------|-------|-------|
| | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 2 | 2 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 1 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 4:30 PM | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 4:45 PM | 2 | 3 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 5:15 PM | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 4 |
| 5:45 PM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 8 | 7 | 0 | 5 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 | 9 |
| Peak Hr | 4 | 5 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 7 |

| Two-Hour Count Summaries - Heavy Vehicles | | | | | | | | | | | | | | 15-min Total | Rolling One Hour | | | |
|--|---------------|----------|----------|----------|---------------|----------|----------|----------|------------|----------|----------|----------|-------------|--------------|------------------|----------|----------|-----------|
| Interval Start | Soper Hill Rd | | | | Soper Hill Rd | | | | 0 | | | | 87th Ave NE | | | | | |
| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | | |
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 |
| 4:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| 4:45 PM | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 14 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 5:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 9 |
| 5:30 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 10 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 |
| Count Total | 0 | 1 | 7 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 20 | 0 |
| Peak Hour | 0 | 1 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 10 | 0 |

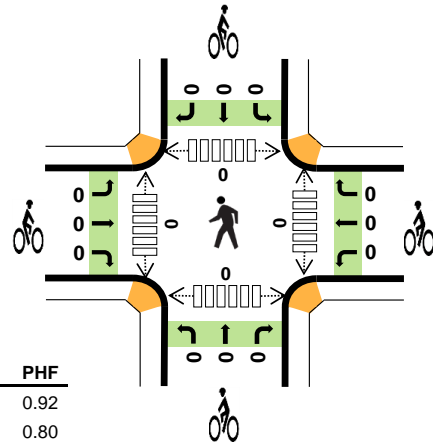
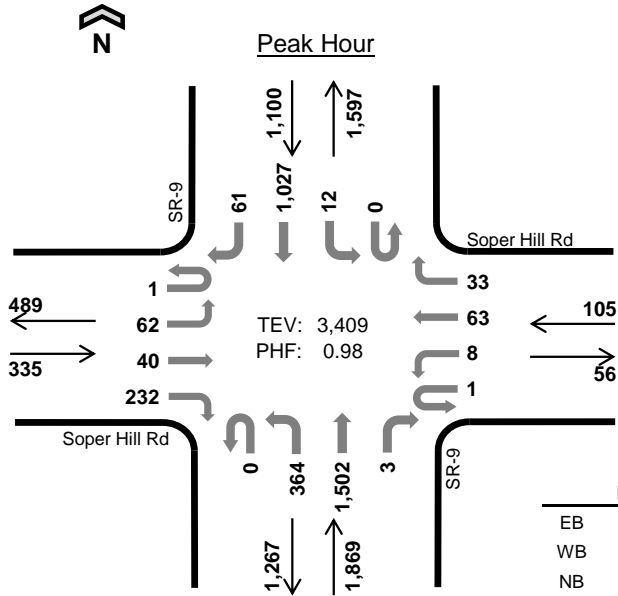
| Two-Hour Count Summaries - Bikes | | | | | | | | | | | | | | 15-min Total | Rolling One Hour |
|---|---------------|----------|----------|---------------|----------|----------|------------|----------|----------|-------------|----------|----------|----------|--------------|------------------|
| Interval Start | Soper Hill Rd | | | Soper Hill Rd | | | 0 | | | 87th Ave NE | | | | | |
| | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | | | |
| | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

SR-9 Soper Hill Rd



Date: 08/16/2022
 Count Period: 4:00 PM to 6:00 PM
 Peak Hour: 4:00 PM to 5:00 PM



| | HV %: | PHF |
|-------|-------|------|
| EB | 3.0% | 0.92 |
| WB | 1.0% | 0.80 |
| NB | 2.7% | 0.97 |
| SB | 4.4% | 0.93 |
| TOTAL | 3.2% | 0.98 |

Two-Hour Count Summaries

| Interval Start | Soper Hill Rd Eastbound | | | | Soper Hill Rd Westbound | | | | SR-9 Northbound | | | | SR-9 Southbound | | | | 15-min Total | Rolling One Hour | |
|----------------|-------------------------|-----|----|-----|-------------------------|----|-----|----|-----------------|-----|-------|-------|-----------------|----|-------|-------|--------------|------------------|---|
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | | |
| 4:00 PM | 1 | 16 | 4 | 63 | 1 | 0 | 23 | 8 | 0 | 84 | 388 | 0 | 0 | 0 | 243 | 21 | 852 | 0 | |
| 4:15 PM | 0 | 13 | 12 | 50 | 0 | 4 | 8 | 10 | 0 | 95 | 385 | 1 | 0 | 2 | 285 | 9 | 874 | 0 | |
| 4:30 PM | 0 | 14 | 14 | 57 | 0 | 4 | 19 | 10 | 0 | 92 | 375 | 1 | 0 | 9 | 243 | 13 | 851 | 0 | |
| 4:45 PM | 0 | 19 | 10 | 62 | 0 | 0 | 13 | 5 | 0 | 93 | 354 | 1 | 0 | 1 | 256 | 18 | 832 | 3,409 | |
| 5:00 PM | 0 | 13 | 11 | 66 | 0 | 0 | 15 | 4 | 0 | 79 | 385 | 1 | 0 | 2 | 248 | 11 | 835 | 3,392 | |
| 5:15 PM | 0 | 8 | 11 | 56 | 0 | 0 | 20 | 3 | 0 | 109 | 395 | 8 | 0 | 6 | 244 | 14 | 874 | 3,392 | |
| 5:30 PM | 0 | 6 | 9 | 64 | 0 | 1 | 13 | 2 | 0 | 89 | 376 | 2 | 0 | 4 | 238 | 12 | 816 | 3,357 | |
| 5:45 PM | 0 | 12 | 6 | 65 | 0 | 0 | 17 | 3 | 0 | 67 | 357 | 0 | 0 | 3 | 202 | 11 | 743 | 3,268 | |
| Count Total | 1 | 101 | 77 | 483 | 1 | 9 | 128 | 45 | 0 | 708 | 3,015 | 14 | 0 | 27 | 1,959 | 109 | 6,677 | 0 | |
| Peak Hour | All | 1 | 62 | 40 | 232 | 1 | 8 | 63 | 33 | 0 | 364 | 1,502 | 3 | 0 | 12 | 1,027 | 61 | 3,409 | 0 |
| | HV | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 5 | 46 | 0 | 0 | 0 | 48 | 0 | 110 | 0 |
| | HV% | 0% | 2% | 0% | 4% | 0% | 0% | 0% | 3% | - | 1% | 3% | 0% | - | 0% | 5% | 0% | 3% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals | | | | | Bicycles | | | | | Pedestrians (Crossing Leg) | | | | |
|----------------|----------------------|----|----|----|-------|----------|----|----|----|-------|----------------------------|------|-------|-------|-------|
| | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 4 | 0 | 19 | 14 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 3 | 0 | 14 | 20 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 1 | 1 | 11 | 8 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 2 | 0 | 7 | 6 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 10 | 11 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 13 | 4 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 1 | 0 | 12 | 6 | 19 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:45 PM | 1 | 0 | 11 | 6 | 18 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| Count Total | 12 | 1 | 97 | 75 | 185 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 |
| Peak Hour | 10 | 1 | 51 | 48 | 110 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Two-Hour Count Summaries - Heavy Vehicles | | | | | | | | | | | | | | | | | | |
|--|---------------|----|----|----|---------------|----|----|----|------------|----|----|----|------------|----|----|----|--------------|------------------|
| Interval Start | Soper Hill Rd | | | | Soper Hill Rd | | | | SR-9 | | | | SR-9 | | | | 15-min Total | Rolling One Hour |
| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | | |
| | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 18 | 0 | 0 | 0 | 14 | 0 | 37 | 0 |
| 4:15 PM | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 0 | 0 | 0 | 20 | 0 | 37 | 0 |
| 4:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 11 | 0 | 0 | 0 | 8 | 0 | 21 | 0 |
| 4:45 PM | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 6 | 0 | 15 | 110 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 11 | 0 | 21 | 94 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 4 | 0 | 17 | 74 |
| 5:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 6 | 0 | 19 | 72 |
| 5:45 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 6 | 0 | 18 | 75 |
| Count Total | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 1 | 0 | 10 | 87 | 0 | 0 | 0 | 75 | 0 | 185 | 0 |
| Peak Hour | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 5 | 46 | 0 | 0 | 0 | 48 | 0 | 110 | 0 |

| Two-Hour Count Summaries - Bikes | | | | | | | | | | | | | | | | | | |
|---|---------------|----|----|---------------|----|----|------------|----|----|------------|----|----|--------------|------------------|---|---|---|---|
| Interval Start | Soper Hill Rd | | | Soper Hill Rd | | | SR-9 | | | SR-9 | | | 15-min Total | Rolling One Hour | | | | |
| | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | | | | | | |
| | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | | | | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

Appendix B: LOS Definitions

Highway Capacity Manual 2010/6th Edition

Signalized intersection level of service (LOS) is defined in terms of a weighted average control delay for the entire intersection. Control delay quantifies the increase in travel time that a vehicle experiences due to the traffic signal control as well as provides a surrogate measure for driver discomfort and fuel consumption. Signalized intersection LOS is stated in terms of average control delay per vehicle (in seconds) during a specified time period (e.g., weekday PM peak hour). Control delay is a complex measure based on many variables, including signal phasing and coordination (i.e., progression of movements through the intersection and along the corridor), signal cycle length, and traffic volumes with respect to intersection capacity and resulting queues. Table 1 summarizes the LOS criteria for signalized intersections, as described in the *Highway Capacity Manual 2010* and 6th Edition (Transportation Research Board, 2010 and 2016, respectively).

Table 1. Level of Service Criteria for Signalized Intersections

| Level of Service | Average Control Delay (seconds/vehicle) | General Description |
|------------------|---|---|
| A | ≤10 | Free Flow |
| B | >10 – 20 | Stable Flow (slight delays) |
| C | >20 – 35 | Stable flow (acceptable delays) |
| D | >35 – 55 | Approaching unstable flow (tolerable delay, occasionally wait through more than one signal cycle before proceeding) |
| E | >55 – 80 | Unstable flow (intolerable delay) |
| F ¹ | >80 | Forced flow (congested and queues fail to clear) |

Source: *Highway Capacity Manual 2010 and 6th Edition*, Transportation Research Board, 2010 and 2016, respectively.

1. If the volume-to-capacity (v/c) ratio for a lane group exceeds 1.0 LOS F is assigned to the individual lane group. LOS for overall approach or intersection is determined solely by the control delay.

Unsignalized intersection LOS criteria can be further reduced into two intersection types: all-way stop and two-way stop control. All-way stop control intersection LOS is expressed in terms of the weighted average control delay of the overall intersection or by approach. Two-way stop-controlled intersection LOS is defined in terms of the average control delay for each minor-street movement (or shared movement) as well as major-street left-turns. This approach is because major-street through vehicles are assumed to experience zero delay, a weighted average of all movements results in very low overall average delay, and this calculated low delay could mask deficiencies of minor movements. Table 2 shows LOS criteria for unsignalized intersections.

Table 2. Level of Service Criteria for Unsignalized Intersections

| Level of Service | Average Control Delay (seconds/vehicle) |
|------------------|---|
| A | 0 – 10 |
| B | >10 – 15 |
| C | >15 – 25 |
| D | >25 – 35 |
| E | >35 – 50 |
| F ¹ | >50 |

Source: *Highway Capacity Manual 2010 and 6th Edition*, Transportation Research Board, 2010 and 2016, respectively.

1. If the volume-to-capacity (v/c) ratio exceeds 1.0, LOS F is assigned an individual lane group for all unsignalized intersections, or minor street approach at two-way stop-controlled intersections. Overall intersection LOS is determined solely by control delay.

Highway Capacity Manual, 2000

Signalized intersection level of service (LOS) is defined in terms of the average total vehicle delay of all movements through an intersection. Vehicle delay is a method of quantifying several intangible factors, including driver discomfort, frustration, and lost travel time. Specifically, LOS criteria are stated in terms of average delay per vehicle during a specified time period (for example, the PM peak hour). Vehicle delay is a complex measure based on many variables, including signal phasing (i.e., progression of movements through the intersection), signal cycle length, and traffic volumes with respect to intersection capacity. Table 1 shows LOS criteria for signalized intersections, as described in the *Highway Capacity Manual* (Transportation Research Board, Special Report 209, 2000).

Table 1. Level of Service Criteria for Signalized Intersections

| Level of Service | Average Control Delay (sec/veh) | General Description (Signalized Intersections) |
|------------------|---------------------------------|---|
| A | ≤10 | Free Flow |
| B | >10 - 20 | Stable Flow (slight delays) |
| C | >20 - 35 | Stable flow (acceptable delays) |
| D | >35 - 55 | Approaching unstable flow (tolerable delay, occasionally wait through more than one signal cycle before proceeding) |
| E | >55 - 80 | Unstable flow (intolerable delay) |
| F | >80 | Forced flow (jammed) |

Source: *Highway Capacity Manual*, Transportation Research Board, Special Report 209, 2000.

Unsignalized intersection LOS criteria can be further reduced into two intersection types: all-way stop-controlled and two-way stop-controlled. All-way, stop-controlled intersection LOS is expressed in terms of the average vehicle delay of all of the movements, much like that of a signalized intersection. Two-way, stop-controlled intersection LOS is defined in terms of the average vehicle delay of an individual movement(s). This is because the performance of a two-way, stop-controlled intersection is more closely reflected in terms of its individual movements, rather than its performance overall. For this reason, LOS for a two-way, stop-controlled intersection is defined in terms of its individual movements. With this in mind, total average vehicle delay (i.e., average delay of all movements) for a two-way, stop-controlled intersection should be viewed with discretion. Table 2 shows LOS criteria for unsignalized intersections (both all-way and two-way, stop-controlled).

Table 2. Level of Service Criteria for Unsignalized Intersections

| Level of Service | Average Control Delay (sec/veh) |
|------------------|---------------------------------|
| A | 0 - 10 |
| B | >10 - 15 |
| C | >15 - 25 |
| D | >25 - 35 |
| E | >35 - 50 |
| F | >50 |

Source: *Highway Capacity Manual*, Transportation Research Board, Special Report 209, 2000.

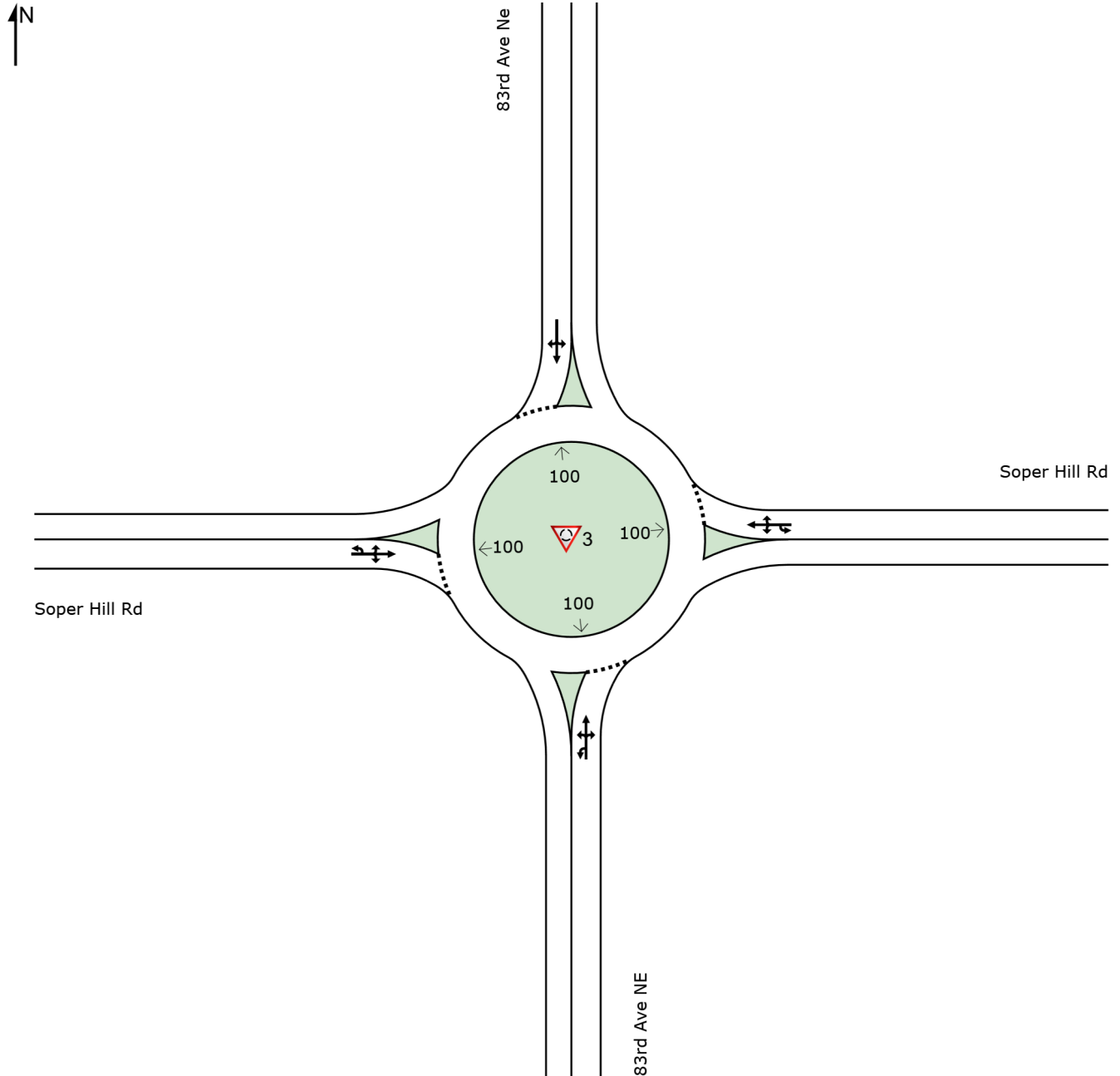
Appendix C: LOS Worksheets

SITE LAYOUT

Site: 3 [1. 83rd Ave NE/Soper Hill Rd Existing (Site Folder: Existing)]

White Barn Brown Bear
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



MOVEMENT SUMMARY

Site: 3 [1. 83rd Ave NE/Soper Hill Rd Existing (Site Folder: Existing)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| South: 83rd Ave NE | | | | | | | | | | | | | | |
| 3u | U | 5 | 4.0 | 5 | 4.0 | 0.091 | 15.0 | LOS B | 0.4 | 10.4 | 0.50 | 0.64 | 0.50 | 36.7 |
| 3 | L2 | 5 | 4.0 | 5 | 4.0 | 0.091 | 12.5 | LOS B | 0.4 | 10.4 | 0.50 | 0.64 | 0.50 | 35.8 |
| 8 | T1 | 10 | 4.0 | 10 | 4.0 | 0.091 | 6.6 | LOS A | 0.4 | 10.4 | 0.50 | 0.64 | 0.50 | 35.7 |
| 18 | R2 | 40 | 4.0 | 41 | 4.0 | 0.091 | 6.7 | LOS A | 0.4 | 10.4 | 0.50 | 0.64 | 0.50 | 34.6 |
| Approach | | 60 | 4.0 | 61 | 4.0 | 0.091 | 7.8 | LOS A | 0.4 | 10.4 | 0.50 | 0.64 | 0.50 | 35.1 |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 1u | U | 5 | 1.0 | 5 | 1.0 | 0.465 | 13.5 | LOS B | 3.1 | 78.0 | 0.43 | 0.54 | 0.43 | 37.5 |
| 1 | L2 | 40 | 1.0 | 41 | 1.0 | 0.465 | 11.1 | LOS B | 3.1 | 78.0 | 0.43 | 0.54 | 0.43 | 36.6 |
| 6 | T1 | 160 | 1.0 | 163 | 1.0 | 0.465 | 5.1 | LOS A | 3.1 | 78.0 | 0.43 | 0.54 | 0.43 | 36.5 |
| 16 | R2 | 200 | 1.0 | 204 | 1.0 | 0.465 | 5.2 | LOS A | 3.1 | 78.0 | 0.43 | 0.54 | 0.43 | 35.4 |
| Approach | | 405 | 1.0 | 413 | 1.0 | 0.465 | 5.8 | LOS A | 3.1 | 78.0 | 0.43 | 0.54 | 0.43 | 35.9 |
| North: 83rd Ave Ne | | | | | | | | | | | | | | |
| 7 | L2 | 100 | 2.0 | 102 | 2.0 | 0.189 | 11.6 | LOS B | 0.9 | 23.2 | 0.44 | 0.67 | 0.44 | 34.9 |
| 4 | T1 | 15 | 2.0 | 15 | 2.0 | 0.189 | 5.6 | LOS A | 0.9 | 23.2 | 0.44 | 0.67 | 0.44 | 34.8 |
| 14 | R2 | 30 | 2.0 | 31 | 2.0 | 0.189 | 5.7 | LOS A | 0.9 | 23.2 | 0.44 | 0.67 | 0.44 | 33.8 |
| Approach | | 145 | 2.0 | 148 | 2.0 | 0.189 | 9.7 | LOS A | 0.9 | 23.2 | 0.44 | 0.67 | 0.44 | 34.6 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5u | U | 5 | 2.0 | 5 | 2.0 | 0.338 | 13.8 | LOS B | 1.9 | 47.3 | 0.44 | 0.60 | 0.44 | 36.7 |
| 5 | L2 | 85 | 2.0 | 87 | 2.0 | 0.338 | 11.4 | LOS B | 1.9 | 47.3 | 0.44 | 0.60 | 0.44 | 35.8 |
| 2 | T1 | 160 | 2.0 | 163 | 2.0 | 0.338 | 5.4 | LOS A | 1.9 | 47.3 | 0.44 | 0.60 | 0.44 | 35.7 |
| 12 | R2 | 25 | 2.0 | 26 | 2.0 | 0.338 | 5.5 | LOS A | 1.9 | 47.3 | 0.44 | 0.60 | 0.44 | 34.6 |
| Approach | | 275 | 2.0 | 281 | 2.0 | 0.338 | 7.4 | LOS A | 1.9 | 47.3 | 0.44 | 0.60 | 0.44 | 35.6 |
| All Vehicles | | 885 | 1.7 | 903 | 1.7 | 0.465 | 7.1 | LOS A | 3.1 | 78.0 | 0.44 | 0.58 | 0.44 | 35.6 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

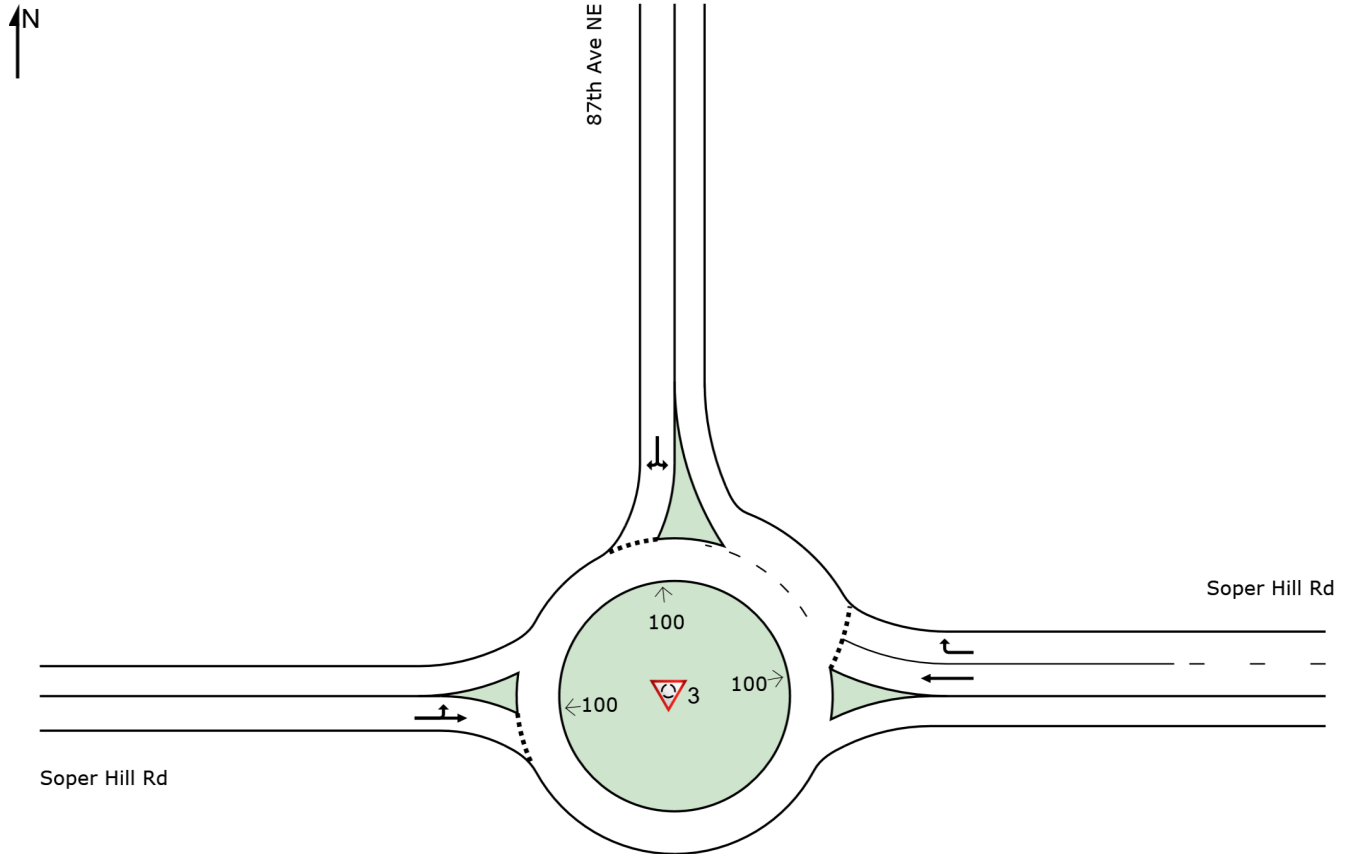
HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SITE LAYOUT

Site: 3 [3. 87th Ave NE/Soper Hill Existing (Site Folder: Existing)]

White Barn Brown Bear
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



MOVEMENT SUMMARY

Site: 3 [3. 87th Ave NE/Soper Hill Existing (Site Folder: Existing)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 6 | T1 | 440 | 1.0 | 468 | 1.0 | 0.399 | 3.7 | LOS A | 2.7 | 67.3 | 0.07 | 0.36 | 0.07 | 38.1 |
| 16 | R2 | 10 | 1.0 | 11 | 1.0 | 0.015 | 4.0 | LOS A | 0.1 | 1.3 | 0.05 | 0.46 | 0.05 | 36.6 |
| Approach | | 450 | 1.0 | 479 | 1.0 | 0.399 | 3.7 | LOS A | 2.7 | 67.3 | 0.07 | 0.36 | 0.07 | 38.1 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 15 | 6.0 | 16 | 6.0 | 0.035 | 13.3 | LOS B | 0.1 | 3.8 | 0.52 | 0.70 | 0.52 | 33.7 |
| 14 | R2 | 5 | 6.0 | 5 | 6.0 | 0.035 | 7.4 | LOS A | 0.1 | 3.8 | 0.52 | 0.70 | 0.52 | 32.8 |
| Approach | | 20 | 6.0 | 21 | 6.0 | 0.035 | 11.8 | LOS B | 0.1 | 3.8 | 0.52 | 0.70 | 0.52 | 33.4 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5 | L2 | 5 | 1.0 | 5 | 1.0 | 0.319 | 9.9 | LOS A | 2.0 | 49.2 | 0.14 | 0.38 | 0.14 | 37.7 |
| 2 | T1 | 290 | 1.0 | 309 | 1.0 | 0.319 | 4.1 | LOS A | 2.0 | 49.2 | 0.14 | 0.38 | 0.14 | 37.5 |
| Approach | | 295 | 1.0 | 314 | 1.0 | 0.319 | 4.2 | LOS A | 2.0 | 49.2 | 0.14 | 0.38 | 0.14 | 37.5 |
| All Vehicles | | 765 | 1.1 | 814 | 1.1 | 0.399 | 4.1 | LOS A | 2.7 | 67.3 | 0.11 | 0.38 | 0.11 | 37.7 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 1.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↻ | | ↻ | ↻ | | | ↻ | | | | ↻ |
| Traffic Vol, veh/h | 0 | 300 | 5 | 55 | 440 | 0 | 5 | 0 | 45 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 300 | 5 | 55 | 440 | 0 | 5 | 0 | 45 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | 100 | - | - | - | - | - | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 319 | 5 | 59 | 468 | 0 | 5 | 0 | 48 | 0 | 0 | 0 |
























| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|---------|---|---|--------|-------|-------|--------|---|-------|
| Conflicting Flow All | - | 0 | 0 | 324 | 0 | 0 | 674 | 908 | 322 | - | - | 234 |
| Stage 1 | - | - | - | - | - | - | 322 | 322 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 352 | 586 | - | - | - | - |
| Critical Hdwy | - | - | - | 4.115 | - | - | 7.33 | 6.53 | 6.23 | - | - | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.13 | 5.53 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.53 | 5.53 | - | - | - | - |
| Follow-up Hdwy | - | - | - | -2.2095 | - | - | 3.519 | 4.019 | 3.319 | - | - | 3.319 |
| Pot Cap-1 Maneuver | 0 | - | - | 1241 | - | - | 354 | 275 | 718 | 0 | 0 | 769 |
| Stage 1 | 0 | - | - | - | - | - | 689 | 650 | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | - | - | - | 639 | 496 | - | 0 | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | 1241 | - | - | 341 | 262 | 718 | - | - | 769 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 341 | 262 | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | 689 | 650 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 609 | 472 | - | - | - | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|----------------------|----|--|--|-----|--|--|------|--|--|----|--|--|
| HCM Control Delay, s | 0 | | | 0.9 | | | 11.1 | | | 0 | | |
| HCM LOS | | | | | | | B | | | A | | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 647 | - | - | 1241 | - | - | - |
| HCM Lane V/C Ratio | 0.082 | - | - | 0.047 | - | - | - |
| HCM Control Delay (s) | 11.1 | - | - | 8 | - | - | 0 |
| HCM Lane LOS | B | - | - | A | - | - | A |
| HCM 95th %tile Q(veh) | 0.3 | - | - | 0.1 | - | - | - |

HCM Signalized Intersection Capacity Analysis
5: SR 9 & Soper Hill Rd

White Barn Brown Bear - Marysville
Existing Weekday PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 65 | 40 | 235 | 10 | 65 | 35 | 370 | 1530 | 5 | 10 | 1050 | 60 |
| Future Volume (vph) | 65 | 40 | 235 | 10 | 65 | 35 | 370 | 1530 | 5 | 10 | 1050 | 60 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Lane Util. Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1789 | 1568 | 1787 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Flt Permitted | | 0.77 | 1.00 | 0.69 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1427 | 1568 | 1294 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 66 | 41 | 240 | 10 | 66 | 36 | 378 | 1561 | 5 | 10 | 1071 | 61 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 31 |
| Lane Group Flow (vph) | 0 | 107 | 240 | 10 | 66 | 8 | 378 | 1566 | 0 | 10 | 1071 | 30 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 1% | 1% | 1% | 3% | 3% | 3% | 4% | 4% | 4% |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | | Prot | NA | Prot |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | | 24.5 | 24.5 | 25.5 | 25.5 | 25.5 | 14.7 | 71.5 | | 1.1 | 57.9 | 57.9 |
| Effective Green, g (s) | | 24.5 | 24.5 | 25.5 | 25.5 | 25.5 | 14.7 | 71.5 | | 1.1 | 57.9 | 57.9 |
| Actuated g/C Ratio | | 0.21 | 0.21 | 0.22 | 0.22 | 0.22 | 0.13 | 0.62 | | 0.01 | 0.50 | 0.50 |
| Clearance Time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.5 | | 2.0 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | | 300 | 330 | 283 | 412 | 350 | 430 | 2155 | | 16 | 1729 | 773 |
| v/s Ratio Prot | | | | | 0.04 | | c0.11 | c0.45 | | 0.01 | 0.31 | 0.02 |
| v/s Ratio Perm | | 0.07 | c0.15 | 0.01 | | 0.00 | | | | | | |
| v/c Ratio | | 0.36 | 0.73 | 0.04 | 0.16 | 0.02 | 0.88 | 0.73 | | 0.62 | 0.62 | 0.04 |
| Uniform Delay, d1 | | 39.1 | 42.7 | 35.7 | 36.7 | 35.6 | 49.9 | 15.6 | | 57.3 | 21.2 | 14.9 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.0 | 8.3 | 0.0 | 0.1 | 0.0 | 17.6 | 1.4 | | 44.0 | 0.9 | 0.0 |
| Delay (s) | | 40.1 | 51.0 | 35.7 | 36.8 | 35.6 | 67.5 | 17.0 | | 101.4 | 22.0 | 15.0 |
| Level of Service | | D | D | D | D | D | E | B | | F | C | B |
| Approach Delay (s) | | 47.7 | | | 36.3 | | | 26.8 | | | 22.3 | |
| Approach LOS | | D | | | D | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 27.7 | | | | HCM 2000 Level of Service | | | C | | |
| HCM 2000 Volume to Capacity ratio | | | 0.81 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 116.2 | | | | Sum of lost time (s) | | | 24.2 | | |
| Intersection Capacity Utilization | | | 74.1% | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

MOVEMENT SUMMARY

Site: 3 [1. 83rd Ave NE/Soper Hill Rd WoP 2024 (Site Folder: Future WoP 2024)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| South: 83rd Ave NE | | | | | | | | | | | | | | |
| 3u | U | 5 | 4.0 | 5 | 4.0 | 0.094 | 15.2 | LOS B | 0.4 | 10.8 | 0.52 | 0.66 | 0.52 | 36.6 |
| 3 | L2 | 5 | 4.0 | 5 | 4.0 | 0.094 | 12.8 | LOS B | 0.4 | 10.8 | 0.52 | 0.66 | 0.52 | 35.7 |
| 8 | T1 | 10 | 4.0 | 10 | 4.0 | 0.094 | 6.8 | LOS A | 0.4 | 10.8 | 0.52 | 0.66 | 0.52 | 35.6 |
| 18 | R2 | 40 | 4.0 | 41 | 4.0 | 0.094 | 6.9 | LOS A | 0.4 | 10.8 | 0.52 | 0.66 | 0.52 | 34.5 |
| Approach | | 60 | 4.0 | 61 | 4.0 | 0.094 | 8.0 | LOS A | 0.4 | 10.8 | 0.52 | 0.66 | 0.52 | 35.0 |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 1u | U | 5 | 1.0 | 5 | 1.0 | 0.508 | 13.6 | LOS B | 3.6 | 90.5 | 0.46 | 0.55 | 0.46 | 37.4 |
| 1 | L2 | 40 | 1.0 | 41 | 1.0 | 0.508 | 11.2 | LOS B | 3.6 | 90.5 | 0.46 | 0.55 | 0.46 | 36.5 |
| 6 | T1 | 175 | 1.0 | 179 | 1.0 | 0.508 | 5.3 | LOS A | 3.6 | 90.5 | 0.46 | 0.55 | 0.46 | 36.4 |
| 16 | R2 | 220 | 1.0 | 224 | 1.0 | 0.508 | 5.3 | LOS A | 3.6 | 90.5 | 0.46 | 0.55 | 0.46 | 35.3 |
| Approach | | 440 | 1.0 | 449 | 1.0 | 0.508 | 5.9 | LOS A | 3.6 | 90.5 | 0.46 | 0.55 | 0.46 | 35.8 |
| North: 83rd Ave Ne | | | | | | | | | | | | | | |
| 7 | L2 | 110 | 2.0 | 112 | 2.0 | 0.206 | 11.7 | LOS B | 1.0 | 25.7 | 0.46 | 0.68 | 0.46 | 34.7 |
| 4 | T1 | 15 | 2.0 | 15 | 2.0 | 0.206 | 5.8 | LOS A | 1.0 | 25.7 | 0.46 | 0.68 | 0.46 | 34.7 |
| 14 | R2 | 30 | 2.0 | 31 | 2.0 | 0.206 | 5.8 | LOS A | 1.0 | 25.7 | 0.46 | 0.68 | 0.46 | 33.7 |
| Approach | | 155 | 2.0 | 158 | 2.0 | 0.206 | 10.0 | LOS A | 1.0 | 25.7 | 0.46 | 0.68 | 0.46 | 34.5 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5u | U | 5 | 2.0 | 5 | 2.0 | 0.361 | 14.0 | LOS B | 2.0 | 51.6 | 0.46 | 0.61 | 0.46 | 36.6 |
| 5 | L2 | 90 | 2.0 | 92 | 2.0 | 0.361 | 11.5 | LOS B | 2.0 | 51.6 | 0.46 | 0.61 | 0.46 | 35.7 |
| 2 | T1 | 170 | 2.0 | 173 | 2.0 | 0.361 | 5.6 | LOS A | 2.0 | 51.6 | 0.46 | 0.61 | 0.46 | 35.6 |
| 12 | R2 | 25 | 2.0 | 26 | 2.0 | 0.361 | 5.6 | LOS A | 2.0 | 51.6 | 0.46 | 0.61 | 0.46 | 34.5 |
| Approach | | 290 | 2.0 | 296 | 2.0 | 0.361 | 7.6 | LOS A | 2.0 | 51.6 | 0.46 | 0.61 | 0.46 | 35.6 |
| All Vehicles | | 945 | 1.7 | 964 | 1.7 | 0.508 | 7.2 | LOS A | 3.6 | 90.5 | 0.47 | 0.60 | 0.47 | 35.5 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 7.3 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 150 | 35 | 10 | 40 | 25 | 20 |
| Future Vol, veh/h | 150 | 35 | 10 | 40 | 25 | 20 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 160 | 37 | 11 | 43 | 27 | 21 |

| Major/Minor | Minor1 | Major1 | Major2 | | |
|----------------------|--------|--------|--------|---|-------|
| Conflicting Flow All | 108 | 33 | 0 | 0 | 54 |
| Stage 1 | 33 | - | - | - | - |
| Stage 2 | 75 | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.16 |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.254 |
| Pot Cap-1 Maneuver | 889 | 1041 | - | - | 1526 |
| Stage 1 | 989 | - | - | - | - |
| Stage 2 | 948 | - | - | - | - |
| Platoon blocked, % | | | - | - | - |
| Mov Cap-1 Maneuver | 873 | 1041 | - | - | 1526 |
| Mov Cap-2 Maneuver | 873 | - | - | - | - |
| Stage 1 | 989 | - | - | - | - |
| Stage 2 | 931 | - | - | - | - |

| Approach | WB | NB | SB |
|----------------------|------|----|-----|
| HCM Control Delay, s | 10.1 | 0 | 4.1 |
| HCM LOS | B | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
|-----------------------|-----|----------|-------|-------|
| Capacity (veh/h) | - | - | 900 | 1526 |
| HCM Lane V/C Ratio | - | - | 0.219 | 0.017 |
| HCM Control Delay (s) | - | - | 10.1 | 7.4 |
| HCM Lane LOS | - | - | B | A |
| HCM 95th %tile Q(veh) | - | - | 0.8 | 0.1 |

MOVEMENT SUMMARY

Site: 3 [3. 87th Ave NE/Soper Hill Rd WoP 2024 (Site Folder: Future WoP 2024)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 6 | T1 | 450 | 1.0 | 479 | 1.0 | 0.423 | 4.0 | LOS A | 3.2 | 79.6 | 0.24 | 0.37 | 0.24 | 37.4 |
| 16 | R2 | 15 | 1.0 | 16 | 1.0 | 0.023 | 4.4 | LOS A | 0.1 | 2.3 | 0.17 | 0.46 | 0.17 | 36.3 |
| Approach | | 465 | 1.0 | 495 | 1.0 | 0.423 | 4.0 | LOS A | 3.2 | 79.6 | 0.23 | 0.38 | 0.23 | 37.4 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 135 | 6.0 | 144 | 6.0 | 0.306 | 14.4 | LOS B | 1.5 | 40.2 | 0.63 | 0.84 | 0.63 | 33.1 |
| 14 | R2 | 35 | 6.0 | 37 | 6.0 | 0.306 | 8.5 | LOS A | 1.5 | 40.2 | 0.63 | 0.84 | 0.63 | 32.2 |
| Approach | | 170 | 6.0 | 181 | 6.0 | 0.306 | 13.2 | LOS B | 1.5 | 40.2 | 0.63 | 0.84 | 0.63 | 32.9 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5 | L2 | 35 | 1.0 | 37 | 1.0 | 0.399 | 11.3 | LOS B | 2.5 | 63.5 | 0.47 | 0.55 | 0.47 | 36.2 |
| 2 | T1 | 280 | 1.0 | 298 | 1.0 | 0.399 | 5.5 | LOS A | 2.5 | 63.5 | 0.47 | 0.55 | 0.47 | 36.0 |
| Approach | | 315 | 1.0 | 335 | 1.0 | 0.399 | 6.1 | LOS A | 2.5 | 63.5 | 0.47 | 0.55 | 0.47 | 36.1 |
| All Vehicles | | 950 | 1.9 | 1011 | 1.9 | 0.423 | 6.3 | LOS A | 3.2 | 79.6 | 0.38 | 0.52 | 0.38 | 36.1 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 1.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↗ | | ↖ | ↗ | ↖ | | ↕ | | | | ↖ |
| Traffic Vol, veh/h | 0 | 400 | 15 | 55 | 430 | 75 | 10 | 0 | 45 | 0 | 0 | 15 |
| Future Vol, veh/h | 0 | 400 | 15 | 55 | 430 | 75 | 10 | 0 | 45 | 0 | 0 | 15 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | 100 | - | - | - | - | - | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 426 | 16 | 59 | 457 | 80 | 11 | 0 | 48 | 0 | 0 | 16 |
























| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | |
|----------------------|--------|---|--------|---------|--------|---|--------|-------|-------|---|---|-------|
| Conflicting Flow All | - | 0 | 0 | 442 | 0 | 0 | 781 | 1089 | 434 | - | - | 269 |
| Stage 1 | - | - | - | - | - | - | 434 | 434 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 347 | 655 | - | - | - | - |
| Critical Hdwy | - | - | - | 4.115 | - | - | 7.33 | 6.53 | 6.23 | - | - | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.13 | 5.53 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.53 | 5.53 | - | - | - | - |
| Follow-up Hdwy | - | - | - | -2.2095 | - | - | 3.519 | 4.019 | 3.319 | - | - | 3.319 |
| Pot Cap-1 Maneuver | 0 | - | - | 1122 | - | - | 298 | 215 | 621 | 0 | 0 | 730 |
| Stage 1 | 0 | - | - | - | - | - | 600 | 580 | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | - | - | - | 643 | 462 | - | 0 | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | 1122 | - | - | 280 | 204 | 621 | - | - | 730 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 280 | 204 | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | 600 | 580 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 596 | 438 | - | - | - | - |

| Approach | EB | WB | NB | SB |
|----------------------|----|-----|----|----|
| HCM Control Delay, s | 0 | 0.8 | 13 | 10 |
| HCM LOS | | | B | B |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 508 | - | - | 1122 | - | - | 730 |
| HCM Lane V/C Ratio | 0.115 | - | - | 0.052 | - | - | 0.022 |
| HCM Control Delay (s) | 13 | - | - | 8.4 | - | - | 10 |
| HCM Lane LOS | B | - | - | A | - | - | B |
| HCM 95th %tile Q(veh) | 0.4 | - | - | 0.2 | - | - | 0.1 |

HCM Signalized Intersection Capacity Analysis
5: SR 9 & Soper Hill Rd

White Barn Brown Bear - Marysville
Future (2024) Without-Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 80 | 45 | 315 | 10 | 70 | 35 | 425 | 1575 | 5 | 10 | 1080 | 70 |
| Future Volume (vph) | 80 | 45 | 315 | 10 | 70 | 35 | 425 | 1575 | 5 | 10 | 1080 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Lane Util. Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1787 | 1568 | 1787 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Flt Permitted | | 0.77 | 1.00 | 0.66 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1411 | 1568 | 1233 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 82 | 46 | 321 | 10 | 71 | 36 | 434 | 1607 | 5 | 10 | 1102 | 71 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 38 |
| Lane Group Flow (vph) | 0 | 128 | 321 | 10 | 71 | 10 | 434 | 1612 | 0 | 10 | 1102 | 33 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 1% | 1% | 1% | 3% | 3% | 3% | 4% | 4% | 4% |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | | Prot | NA | Prot |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | | 33.7 | 33.7 | 34.7 | 34.7 | 34.7 | 14.6 | 72.4 | | 1.2 | 59.0 | 59.0 |
| Effective Green, g (s) | | 33.7 | 33.7 | 34.7 | 34.7 | 34.7 | 14.6 | 72.4 | | 1.2 | 59.0 | 59.0 |
| Actuated g/C Ratio | | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | 0.12 | 0.57 | | 0.01 | 0.47 | 0.47 |
| Clearance Time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.5 | | 2.0 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | | 376 | 418 | 338 | 516 | 438 | 392 | 2006 | | 16 | 1620 | 724 |
| v/s Ratio Prot | | | | | 0.04 | | c0.13 | c0.46 | | 0.01 | 0.32 | 0.02 |
| v/s Ratio Perm | | 0.09 | c0.20 | 0.01 | | 0.01 | | | | | | |
| v/c Ratio | | 0.34 | 0.77 | 0.03 | 0.14 | 0.02 | 1.11 | 0.80 | | 0.62 | 0.68 | 0.05 |
| Uniform Delay, d1 | | 37.4 | 42.7 | 33.5 | 34.6 | 33.5 | 55.9 | 21.4 | | 62.4 | 26.3 | 18.4 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.7 | 8.7 | 0.0 | 0.0 | 0.0 | 77.7 | 2.7 | | 44.0 | 1.4 | 0.0 |
| Delay (s) | | 38.1 | 51.5 | 33.5 | 34.6 | 33.5 | 133.6 | 24.1 | | 106.4 | 27.7 | 18.4 |
| Level of Service | | D | D | C | C | C | F | C | | F | C | B |
| Approach Delay (s) | | 47.7 | | | 34.2 | | | 47.3 | | | 27.8 | |
| Approach LOS | | D | | | C | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 40.9 | | | | HCM 2000 Level of Service | | | | D | |
| HCM 2000 Volume to Capacity ratio | | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 126.4 | | | | Sum of lost time (s) | | | 24.2 | | |
| Intersection Capacity Utilization | | | 76.4% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c | Critical Lane Group | | | | | | | | | | | |

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 5.8 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ↔ | | ↑ | ↗ | ↖ | ↑ |
| Traffic Vol, veh/h | 135 | 65 | 75 | 30 | 45 | 110 |
| Future Vol, veh/h | 135 | 65 | 75 | 30 | 45 | 110 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 0 | 0 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 144 | 69 | 80 | 32 | 48 | 117 |

| Major/Minor | Minor1 | Major1 | Major2 | | |
|----------------------|--------|--------|--------|---|-------|
| Conflicting Flow All | 293 | 80 | 0 | 0 | 112 |
| Stage 1 | 80 | - | - | - | - |
| Stage 2 | 213 | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.16 |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.254 |
| Pot Cap-1 Maneuver | 698 | 980 | - | - | 1453 |
| Stage 1 | 943 | - | - | - | - |
| Stage 2 | 823 | - | - | - | - |
| Platoon blocked, % | | | - | - | - |
| Mov Cap-1 Maneuver | 675 | 980 | - | - | 1453 |
| Mov Cap-2 Maneuver | 675 | - | - | - | - |
| Stage 1 | 943 | - | - | - | - |
| Stage 2 | 796 | - | - | - | - |

| Approach | WB | NB | SB |
|----------------------|------|----|-----|
| HCM Control Delay, s | 11.7 | 0 | 2.2 |
| HCM LOS | B | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
|-----------------------|-----|----------|-------|-------|
| Capacity (veh/h) | - | - | 751 | 1453 |
| HCM Lane V/C Ratio | - | - | 0.283 | 0.033 |
| HCM Control Delay (s) | - | - | 11.7 | 7.6 |
| HCM Lane LOS | - | - | B | A |
| HCM 95th %tile Q(veh) | - | - | 1.2 | 0.1 |

MOVEMENT SUMMARY

Site: 3 [3. 87th Ave NE/Soper Hill Rd WoP 2030 (Site Folder: Future WoP 2030)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 6 | T1 | 485 | 1.0 | 516 | 1.0 | 0.435 | 4.4 | LOS A | 3.2 | 81.5 | 0.37 | 0.43 | 0.37 | 37.0 |
| 16 | R2 | 20 | 1.0 | 21 | 1.0 | 0.029 | 5.0 | LOS A | 0.1 | 3.4 | 0.29 | 0.48 | 0.29 | 36.0 |
| Approach | | 505 | 1.0 | 537 | 1.0 | 0.435 | 4.4 | LOS A | 3.2 | 81.5 | 0.36 | 0.43 | 0.36 | 36.9 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 145 | 6.0 | 154 | 6.0 | 0.403 | 14.5 | LOS B | 2.4 | 61.6 | 0.70 | 0.86 | 0.72 | 33.5 |
| 14 | R2 | 100 | 6.0 | 106 | 6.0 | 0.403 | 8.7 | LOS A | 2.4 | 61.6 | 0.70 | 0.86 | 0.72 | 32.6 |
| Approach | | 245 | 6.0 | 261 | 6.0 | 0.403 | 12.1 | LOS B | 2.4 | 61.6 | 0.70 | 0.86 | 0.72 | 33.1 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5 | L2 | 85 | 1.0 | 90 | 1.0 | 0.461 | 11.2 | LOS B | 3.2 | 80.7 | 0.51 | 0.58 | 0.51 | 35.8 |
| 2 | T1 | 315 | 1.0 | 335 | 1.0 | 0.461 | 5.4 | LOS A | 3.2 | 80.7 | 0.51 | 0.58 | 0.51 | 35.7 |
| Approach | | 400 | 1.0 | 426 | 1.0 | 0.461 | 6.6 | LOS A | 3.2 | 80.7 | 0.51 | 0.58 | 0.51 | 35.7 |
| All Vehicles | | 1150 | 2.1 | 1223 | 2.1 | 0.461 | 6.8 | LOS A | 3.2 | 81.5 | 0.48 | 0.57 | 0.49 | 35.6 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 1.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↻ | | ↻ | ↻ | ↻ | | ↻ | | | | ↻ |
| Traffic Vol, veh/h | 0 | 445 | 15 | 65 | 490 | 70 | 15 | 0 | 50 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 445 | 15 | 65 | 490 | 70 | 15 | 0 | 50 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 473 | 16 | 69 | 521 | 74 | 16 | 0 | 53 | 0 | 0 | 0 |

























| Major/Minor | Major1 | | Major2 | | Minor1 | | | Minor2 | | | | |
|----------------------|--------|---|--------|---------|--------|---|-------|--------|-------|---|---|-------|
| Conflicting Flow All | - | 0 | 0 | 489 | 0 | 0 | 880 | 1214 | 481 | - | - | 298 |
| Stage 1 | - | - | - | - | - | - | 481 | 481 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 399 | 733 | - | - | - | - |
| Critical Hdwy | - | - | - | 4.115 | - | - | 7.33 | 6.53 | 6.23 | - | - | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.13 | 5.53 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.53 | 5.53 | - | - | - | - |
| Follow-up Hdwy | - | - | - | -2.2095 | - | - | 3.519 | 4.019 | 3.319 | - | - | 3.319 |
| Pot Cap-1 Maneuver | 0 | - | - | 1078 | - | - | 254 | 181 | 584 | 0 | 0 | 699 |
| Stage 1 | 0 | - | - | - | - | - | 565 | 553 | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | - | - | - | 599 | 425 | - | 0 | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | 1078 | - | - | 235 | 163 | 584 | - | - | 699 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 235 | 163 | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | 565 | 553 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 541 | 384 | - | - | - | - |

| Approach | EB | | WB | | NB | | SB | |
|----------------------|----|--|-----|--|------|--|----|--|
| HCM Control Delay, s | 0 | | 1.1 | | 14.8 | | 0 | |
| HCM LOS | | | | | B | | A | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 435 | - | - | 1078 | - | - | - |
| HCM Lane V/C Ratio | 0.159 | - | - | 0.064 | - | - | - |
| HCM Control Delay (s) | 14.8 | - | - | 8.6 | 0.3 | - | 0 |
| HCM Lane LOS | B | - | - | A | A | - | A |
| HCM 95th %tile Q(veh) | 0.6 | - | - | 0.2 | - | - | - |

HCM Signalized Intersection Capacity Analysis
5: SR 9 & Soper Hill Rd

White Barn Brown Bear - Marysville
Future (2030) Without-Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 35 | 65 | 390 | 10 | 95 | 40 | 515 | 1995 | 5 | 10 | 1490 | 15 |
| Future Volume (vph) | 35 | 65 | 390 | 10 | 95 | 40 | 515 | 1995 | 5 | 10 | 1490 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.1 | 6.1 | 5.5 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1752 | 1845 | 1568 | 1787 | 1881 | 1599 | 3400 | 3504 | | 1736 | 3471 | 1553 |
| Flt Permitted | 0.63 | 1.00 | 1.00 | 0.71 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1158 | 1845 | 1568 | 1343 | 1881 | 1599 | 3400 | 3504 | | 1736 | 3471 | 1553 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 36 | 66 | 398 | 10 | 97 | 41 | 526 | 2036 | 5 | 10 | 1520 | 15 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 36 | 66 | 398 | 10 | 97 | 4 | 526 | 2041 | 0 | 10 | 1520 | 9 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 1% | 1% | 1% | 3% | 3% | 3% | 4% | 4% | 4% |
| Turn Type | Perm | NA | pm+ov | Perm | NA | Perm | Prot | NA | | Prot | NA | Prot |
| Protected Phases | | 4 | 5 | | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | 10.6 | 10.6 | 25.2 | 11.6 | 11.6 | 11.6 | 14.6 | 88.0 | | 1.2 | 74.6 | 74.6 |
| Effective Green, g (s) | 10.6 | 10.6 | 25.2 | 11.6 | 11.6 | 11.6 | 14.6 | 88.0 | | 1.2 | 74.6 | 74.6 |
| Actuated g/C Ratio | 0.09 | 0.09 | 0.21 | 0.10 | 0.10 | 0.10 | 0.12 | 0.74 | | 0.01 | 0.63 | 0.63 |
| Clearance Time (s) | 6.1 | 6.1 | 5.5 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.5 | | 2.0 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | 103 | 164 | 332 | 131 | 183 | 156 | 417 | 2593 | | 17 | 2177 | 974 |
| v/s Ratio Prot | | 0.04 | c0.15 | | 0.05 | | c0.15 | c0.58 | | 0.01 | 0.44 | 0.01 |
| v/s Ratio Perm | 0.03 | | 0.11 | 0.01 | | 0.00 | | | | | | |
| v/c Ratio | 0.35 | 0.40 | 1.20 | 0.08 | 0.53 | 0.03 | 1.26 | 0.79 | | 0.59 | 0.70 | 0.01 |
| Uniform Delay, d1 | 50.9 | 51.2 | 46.9 | 48.8 | 51.1 | 48.5 | 52.2 | 9.6 | | 58.6 | 14.7 | 8.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.8 | 2.2 | 114.9 | 0.1 | 1.5 | 0.0 | 135.7 | 1.8 | | 29.3 | 1.2 | 0.0 |
| Delay (s) | 53.7 | 53.4 | 161.8 | 48.9 | 52.5 | 48.6 | 187.8 | 11.5 | | 87.9 | 15.8 | 8.3 |
| Level of Service | D | D | F | D | D | D | F | B | | F | B | A |
| Approach Delay (s) | | 139.7 | | | 51.2 | | | 47.6 | | | 16.2 | |
| Approach LOS | | F | | | D | | | D | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 47.2 | | | | HCM 2000 Level of Service | | | D | | |
| HCM 2000 Volume to Capacity ratio | | | 0.97 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 118.9 | | | | Sum of lost time (s) | | 24.2 | | | |
| Intersection Capacity Utilization | | | 84.6% | | | | ICU Level of Service | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

MOVEMENT SUMMARY

Site: 3 [6. 87th Ave NE/35th St NE WoP 2030 (Site Folder: Future WoP 2030)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| South: RoadName | | | | | | | | | | | | | | |
| 8 | T1 | 195 | 2.0 | 207 | 2.0 | 0.249 | 5.3 | LOS A | 1.1 | 29.0 | 0.45 | 0.54 | 0.45 | 36.6 |
| 18 | R2 | 35 | 2.0 | 37 | 2.0 | 0.249 | 5.4 | LOS A | 1.1 | 29.0 | 0.45 | 0.54 | 0.45 | 35.5 |
| Approach | | 230 | 2.0 | 245 | 2.0 | 0.249 | 5.3 | LOS A | 1.1 | 29.0 | 0.45 | 0.54 | 0.45 | 36.4 |
| East: 35th St NE | | | | | | | | | | | | | | |
| 1 | L2 | 85 | 2.0 | 90 | 2.0 | 0.089 | 10.8 | LOS B | 0.4 | 11.3 | 0.39 | 0.64 | 0.39 | 34.0 |
| 16 | R2 | 100 | 2.0 | 106 | 2.0 | 0.102 | 5.1 | LOS A | 0.5 | 13.1 | 0.39 | 0.53 | 0.39 | 35.6 |
| Approach | | 185 | 2.0 | 197 | 2.0 | 0.102 | 7.8 | LOS A | 0.5 | 13.1 | 0.39 | 0.58 | 0.39 | 34.8 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 325 | 6.0 | 346 | 6.0 | 0.393 | 10.7 | LOS B | 2.5 | 64.4 | 0.35 | 0.62 | 0.35 | 34.3 |
| 4 | T1 | 30 | 6.0 | 32 | 6.0 | 0.393 | 4.7 | LOS A | 2.5 | 64.4 | 0.35 | 0.62 | 0.35 | 34.2 |
| Approach | | 355 | 6.0 | 378 | 6.0 | 0.393 | 10.2 | LOS B | 2.5 | 64.4 | 0.35 | 0.62 | 0.35 | 34.3 |
| All Vehicles | | 770 | 3.8 | 819 | 3.8 | 0.393 | 8.1 | LOS A | 2.5 | 64.4 | 0.39 | 0.59 | 0.39 | 35.0 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 3 [1. 83rd Ave NE/Soper Hill Rd WP 2024 (Site Folder: Future WP 2024)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| South: 83rd Ave NE | | | | | | | | | | | | | | |
| 3u | U | 5 | 4.0 | 5 | 4.0 | 0.095 | 15.3 | LOS B | 0.4 | 11.0 | 0.53 | 0.67 | 0.53 | 36.5 |
| 3 | L2 | 5 | 4.0 | 5 | 4.0 | 0.095 | 12.9 | LOS B | 0.4 | 11.0 | 0.53 | 0.67 | 0.53 | 35.6 |
| 8 | T1 | 10 | 4.0 | 10 | 4.0 | 0.095 | 6.9 | LOS A | 0.4 | 11.0 | 0.53 | 0.67 | 0.53 | 35.5 |
| 18 | R2 | 40 | 4.0 | 41 | 4.0 | 0.095 | 7.0 | LOS A | 0.4 | 11.0 | 0.53 | 0.67 | 0.53 | 34.5 |
| Approach | | 60 | 4.0 | 61 | 4.0 | 0.095 | 8.2 | LOS A | 0.4 | 11.0 | 0.53 | 0.67 | 0.53 | 34.9 |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 1u | U | 5 | 1.0 | 5 | 1.0 | 0.526 | 13.7 | LOS B | 3.8 | 96.3 | 0.48 | 0.55 | 0.48 | 37.4 |
| 1 | L2 | 40 | 1.0 | 41 | 1.0 | 0.526 | 11.2 | LOS B | 3.8 | 96.3 | 0.48 | 0.55 | 0.48 | 36.5 |
| 6 | T1 | 182 | 1.0 | 186 | 1.0 | 0.526 | 5.3 | LOS A | 3.8 | 96.3 | 0.48 | 0.55 | 0.48 | 36.4 |
| 16 | R2 | 228 | 1.0 | 233 | 1.0 | 0.526 | 5.4 | LOS A | 3.8 | 96.3 | 0.48 | 0.55 | 0.48 | 35.2 |
| Approach | | 455 | 1.0 | 464 | 1.0 | 0.526 | 5.9 | LOS A | 3.8 | 96.3 | 0.48 | 0.55 | 0.48 | 35.8 |
| North: 83rd Ave Ne | | | | | | | | | | | | | | |
| 7 | L2 | 119 | 2.0 | 121 | 2.0 | 0.219 | 11.8 | LOS B | 1.1 | 27.8 | 0.47 | 0.69 | 0.47 | 34.6 |
| 4 | T1 | 15 | 2.0 | 15 | 2.0 | 0.219 | 5.8 | LOS A | 1.1 | 27.8 | 0.47 | 0.69 | 0.47 | 34.6 |
| 14 | R2 | 30 | 2.0 | 31 | 2.0 | 0.219 | 5.9 | LOS A | 1.1 | 27.8 | 0.47 | 0.69 | 0.47 | 33.6 |
| Approach | | 164 | 2.0 | 167 | 2.0 | 0.219 | 10.2 | LOS B | 1.1 | 27.8 | 0.47 | 0.69 | 0.47 | 34.4 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5u | U | 5 | 2.0 | 5 | 2.0 | 0.373 | 14.1 | LOS B | 2.1 | 54.1 | 0.48 | 0.62 | 0.48 | 36.5 |
| 5 | L2 | 90 | 2.0 | 92 | 2.0 | 0.373 | 11.6 | LOS B | 2.1 | 54.1 | 0.48 | 0.62 | 0.48 | 35.7 |
| 2 | T1 | 177 | 2.0 | 181 | 2.0 | 0.373 | 5.7 | LOS A | 2.1 | 54.1 | 0.48 | 0.62 | 0.48 | 35.6 |
| 12 | R2 | 25 | 2.0 | 26 | 2.0 | 0.373 | 5.7 | LOS A | 2.1 | 54.1 | 0.48 | 0.62 | 0.48 | 34.5 |
| Approach | | 297 | 2.0 | 303 | 2.0 | 0.373 | 7.6 | LOS A | 2.1 | 54.1 | 0.48 | 0.62 | 0.48 | 35.5 |
| All Vehicles | | 976 | 1.7 | 996 | 1.7 | 0.526 | 7.3 | LOS A | 3.8 | 96.3 | 0.48 | 0.60 | 0.48 | 35.4 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 7.2 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ↘↗ | | ↑ | ↗↘ | ↘↗ | ↑ |
| Traffic Vol, veh/h | 188 | 39 | 12 | 71 | 29 | 20 |
| Future Vol, veh/h | 188 | 39 | 12 | 71 | 29 | 20 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 0 | 0 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 200 | 41 | 13 | 76 | 31 | 21 |

| Major/Minor | Minor1 | Major1 | Major2 | | |
|----------------------|--------|--------|--------|---|-------|
| Conflicting Flow All | 96 | 13 | 0 | 0 | 89 |
| Stage 1 | 13 | - | - | - | - |
| Stage 2 | 83 | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.16 |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.254 |
| Pot Cap-1 Maneuver | 903 | 1067 | - | - | 1482 |
| Stage 1 | 1010 | - | - | - | - |
| Stage 2 | 940 | - | - | - | - |
| Platoon blocked, % | | | | | |
| Mov Cap-1 Maneuver | 884 | 1067 | - | - | 1482 |
| Mov Cap-2 Maneuver | 884 | - | - | - | - |
| Stage 1 | 1010 | - | - | - | - |
| Stage 2 | 920 | - | - | - | - |

| Approach | WB | NB | SB |
|----------------------|------|----|-----|
| HCM Control Delay, s | 10.4 | 0 | 4.4 |
| HCM LOS | B | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
|-----------------------|-----|----------|-------|-------|
| Capacity (veh/h) | - | - | 911 | 1482 |
| HCM Lane V/C Ratio | - | - | 0.265 | 0.021 |
| HCM Control Delay (s) | - | - | 10.4 | 7.5 |
| HCM Lane LOS | - | - | B | A |
| HCM 95th %tile Q(veh) | - | - | 1.1 | 0.1 |

MOVEMENT SUMMARY

Site: 3 [3. 87th Ave NE/Soper Hill Rd WP 2024 (Site Folder: Future WP 2024)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 6 | T1 | 463 | 1.0 | 493 | 1.0 | 0.452 | 4.3 | LOS A | 3.5 | 87.4 | 0.35 | 0.41 | 0.35 | 37.0 |
| 16 | R2 | 17 | 1.0 | 18 | 1.0 | 0.027 | 4.8 | LOS A | 0.1 | 2.8 | 0.24 | 0.47 | 0.24 | 36.1 |
| Approach | | 480 | 1.0 | 511 | 1.0 | 0.452 | 4.3 | LOS A | 3.5 | 87.4 | 0.34 | 0.42 | 0.34 | 37.0 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 171 | 6.0 | 182 | 6.0 | 0.386 | 15.0 | LOS B | 2.1 | 55.5 | 0.69 | 0.88 | 0.71 | 32.7 |
| 14 | R2 | 37 | 6.0 | 39 | 6.0 | 0.386 | 9.1 | LOS A | 2.1 | 55.5 | 0.69 | 0.88 | 0.71 | 31.8 |
| Approach | | 208 | 6.0 | 221 | 6.0 | 0.386 | 13.9 | LOS B | 2.1 | 55.5 | 0.69 | 0.88 | 0.71 | 32.5 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5 | L2 | 66 | 1.0 | 70 | 1.0 | 0.441 | 11.8 | LOS B | 2.9 | 72.1 | 0.54 | 0.62 | 0.54 | 35.7 |
| 2 | T1 | 265 | 1.0 | 282 | 1.0 | 0.441 | 5.9 | LOS A | 2.9 | 72.1 | 0.54 | 0.62 | 0.54 | 35.6 |
| Approach | | 331 | 1.0 | 352 | 1.0 | 0.441 | 7.1 | LOS A | 2.9 | 72.1 | 0.54 | 0.62 | 0.54 | 35.6 |
| All Vehicles | | 1019 | 2.0 | 1084 | 2.0 | 0.452 | 7.2 | LOS A | 3.5 | 87.4 | 0.48 | 0.58 | 0.48 | 35.5 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 1.6 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↻ | | | ↻↻ | | | ↻ | | | | ↻ |
| Traffic Vol, veh/h | 0 | 421 | 15 | 55 | 415 | 114 | 10 | 0 | 45 | 0 | 0 | 45 |
| Future Vol, veh/h | 0 | 421 | 15 | 55 | 415 | 114 | 10 | 0 | 45 | 0 | 0 | 45 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 448 | 16 | 59 | 441 | 121 | 11 | 0 | 48 | 0 | 0 | 48 |
























| Major/Minor | Major1 | | Major2 | | Minor1 | | Minor2 | | | | | |
|----------------------|--------|---|--------|---------|--------|---|--------|-------|-------|---|---|-------|
| Conflicting Flow All | - | 0 | 0 | 464 | 0 | 0 | 795 | 1136 | 456 | - | - | 281 |
| Stage 1 | - | - | - | - | - | - | 456 | 456 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 339 | 680 | - | - | - | - |
| Critical Hdwy | - | - | - | 4.115 | - | - | 7.33 | 6.53 | 6.23 | - | - | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.13 | 5.53 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.53 | 5.53 | - | - | - | - |
| Follow-up Hdwy | - | - | - | -2.2095 | - | - | 3.519 | 4.019 | 3.319 | - | - | 3.319 |
| Pot Cap-1 Maneuver | 0 | - | - | 1102 | - | - | 292 | 201 | 603 | 0 | 0 | 717 |
| Stage 1 | 0 | - | - | - | - | - | 583 | 567 | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | - | - | - | 650 | 450 | - | 0 | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | 1102 | - | - | 256 | 185 | 603 | - | - | 717 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 256 | 185 | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | 583 | 567 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 559 | 414 | - | - | - | - |

| Approach | EB | WB | NB | SB |
|----------------------|----|----|------|------|
| HCM Control Delay, s | 0 | 1 | 13.5 | 10.4 |
| HCM LOS | | | B | B |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 484 | - | - | 1102 | - | - | 717 |
| HCM Lane V/C Ratio | 0.121 | - | - | 0.053 | - | - | 0.067 |
| HCM Control Delay (s) | 13.5 | - | - | 8.4 | 0.3 | - | 10.4 |
| HCM Lane LOS | B | - | - | A | A | - | B |
| HCM 95th %tile Q(veh) | 0.4 | - | - | 0.2 | - | - | 0.2 |

HCM Signalized Intersection Capacity Analysis
5: SR 9 & Soper Hill Rd

White Barn Brown Bear - Marysville
Future (2024) With-Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 81 | 46 | 334 | 10 | 71 | 35 | 445 | 1575 | 5 | 10 | 1080 | 73 |
| Future Volume (vph) | 81 | 46 | 334 | 10 | 71 | 35 | 445 | 1575 | 5 | 10 | 1080 | 73 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Lane Util. Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1788 | 1568 | 1787 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Flt Permitted | | 0.76 | 1.00 | 0.65 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1411 | 1568 | 1227 | 1881 | 1599 | 3400 | 3503 | | 1736 | 3471 | 1553 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 83 | 47 | 341 | 10 | 72 | 36 | 454 | 1607 | 5 | 10 | 1102 | 74 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 40 |
| Lane Group Flow (vph) | 0 | 130 | 341 | 10 | 72 | 10 | 454 | 1612 | 0 | 10 | 1102 | 34 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 1% | 1% | 1% | 3% | 3% | 3% | 4% | 4% | 4% |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | | Prot | NA | Prot |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | | 34.0 | 34.0 | 35.0 | 35.0 | 35.0 | 14.6 | 72.4 | | 1.2 | 59.0 | 59.0 |
| Effective Green, g (s) | | 34.0 | 34.0 | 35.0 | 35.0 | 35.0 | 14.6 | 72.4 | | 1.2 | 59.0 | 59.0 |
| Actuated g/C Ratio | | 0.27 | 0.27 | 0.28 | 0.28 | 0.28 | 0.12 | 0.57 | | 0.01 | 0.47 | 0.47 |
| Clearance Time (s) | | 6.1 | 6.1 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.5 | | 2.0 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | | 378 | 420 | 338 | 519 | 441 | 391 | 2001 | | 16 | 1616 | 723 |
| v/s Ratio Prot | | | | | 0.04 | | c0.13 | c0.46 | | 0.01 | 0.32 | 0.02 |
| v/s Ratio Perm | | 0.09 | c0.22 | 0.01 | | 0.01 | | | | | | |
| v/c Ratio | | 0.34 | 0.81 | 0.03 | 0.14 | 0.02 | 1.16 | 0.81 | | 0.62 | 0.68 | 0.05 |
| Uniform Delay, d1 | | 37.4 | 43.4 | 33.5 | 34.5 | 33.4 | 56.1 | 21.6 | | 62.5 | 26.5 | 18.5 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.7 | 11.9 | 0.0 | 0.0 | 0.0 | 97.2 | 2.7 | | 44.0 | 1.4 | 0.0 |
| Delay (s) | | 38.1 | 55.3 | 33.5 | 34.6 | 33.4 | 153.3 | 24.3 | | 106.5 | 27.9 | 18.5 |
| Level of Service | | D | E | C | C | C | F | C | | F | C | B |
| Approach Delay (s) | | 50.5 | | | 34.1 | | | 52.7 | | | 28.0 | |
| Approach LOS | | D | | | C | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 44.2 | | | | HCM 2000 Level of Service | | | | D | |
| HCM 2000 Volume to Capacity ratio | | | 0.92 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 126.7 | | | | Sum of lost time (s) | | | 24.2 | | |
| Intersection Capacity Utilization | | | 76.5% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 6.7 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | | ↑ | ↑ | ↑ | ↑ |
| Traffic Vol, veh/h | 171 | 78 | 75 | 54 | 59 | 110 |
| Future Vol, veh/h | 171 | 78 | 75 | 54 | 59 | 110 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 0 | 0 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 6 | 6 |
| Mvmt Flow | 182 | 83 | 80 | 57 | 63 | 117 |

| Major/Minor | Minor1 | Major1 | Major2 | | |
|----------------------|--------|--------|--------|---|-------|
| Conflicting Flow All | 323 | 80 | 0 | 0 | 137 |
| Stage 1 | 80 | - | - | - | - |
| Stage 2 | 243 | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.16 |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.254 |
| Pot Cap-1 Maneuver | 671 | 980 | - | - | 1423 |
| Stage 1 | 943 | - | - | - | - |
| Stage 2 | 797 | - | - | - | - |
| Platoon blocked, % | | | - | - | - |
| Mov Cap-1 Maneuver | 641 | 980 | - | - | 1423 |
| Mov Cap-2 Maneuver | 641 | - | - | - | - |
| Stage 1 | 943 | - | - | - | - |
| Stage 2 | 762 | - | - | - | - |

| Approach | WB | NB | SB |
|----------------------|------|----|-----|
| HCM Control Delay, s | 12.9 | 0 | 2.7 |
| HCM LOS | B | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
|-----------------------|-----|----------|-------|-------|
| Capacity (veh/h) | - | - | 719 | 1423 |
| HCM Lane V/C Ratio | - | - | 0.368 | 0.044 |
| HCM Control Delay (s) | - | - | 12.9 | 7.6 |
| HCM Lane LOS | - | - | B | A |
| HCM 95th %tile Q(veh) | - | - | 1.7 | 0.1 |

MOVEMENT SUMMARY

Site: 3 [3. 87th Ave NE/Soper Hill Rd WP 2030 (Site Folder: Future WP 2030)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|---------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist ft | | | | |
| East: Soper Hill Rd | | | | | | | | | | | | | | |
| 6 | T1 | 493 | 1.0 | 524 | 1.0 | 0.454 | 4.6 | LOS A | 3.4 | 86.9 | 0.43 | 0.46 | 0.43 | 36.7 |
| 16 | R2 | 20 | 1.0 | 21 | 1.0 | 0.030 | 5.2 | LOS A | 0.1 | 3.5 | 0.34 | 0.49 | 0.34 | 35.9 |
| Approach | | 513 | 1.0 | 546 | 1.0 | 0.454 | 4.6 | LOS A | 3.4 | 86.9 | 0.42 | 0.46 | 0.42 | 36.7 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 181 | 6.0 | 193 | 6.0 | 0.470 | 15.5 | LOS B | 3.1 | 81.3 | 0.74 | 0.92 | 0.83 | 32.9 |
| 14 | R2 | 100 | 6.0 | 106 | 6.0 | 0.470 | 9.6 | LOS A | 3.1 | 81.3 | 0.74 | 0.92 | 0.83 | 32.0 |
| Approach | | 281 | 6.0 | 299 | 6.0 | 0.470 | 13.4 | LOS B | 3.1 | 81.3 | 0.74 | 0.92 | 0.83 | 32.6 |
| West: Soper Hill Rd | | | | | | | | | | | | | | |
| 5 | L2 | 109 | 1.0 | 116 | 1.0 | 0.491 | 11.6 | LOS B | 3.5 | 87.8 | 0.58 | 0.62 | 0.58 | 35.5 |
| 2 | T1 | 300 | 1.0 | 319 | 1.0 | 0.491 | 5.8 | LOS A | 3.5 | 87.8 | 0.58 | 0.62 | 0.58 | 35.3 |
| Approach | | 409 | 1.0 | 435 | 1.0 | 0.491 | 7.4 | LOS A | 3.5 | 87.8 | 0.58 | 0.62 | 0.58 | 35.4 |
| All Vehicles | | 1203 | 2.2 | 1280 | 2.2 | 0.491 | 7.6 | LOS A | 3.5 | 87.8 | 0.55 | 0.62 | 0.57 | 35.2 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 1.6 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↗ | | | ↖↗ | | | ↖↗ | | | | ↖ |
| Traffic Vol, veh/h | 0 | 466 | 15 | 65 | 475 | 106 | 15 | 0 | 50 | 0 | 0 | 23 |
| Future Vol, veh/h | 0 | 466 | 15 | 65 | 475 | 106 | 15 | 0 | 50 | 0 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | 0 |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 496 | 16 | 69 | 505 | 113 | 16 | 0 | 53 | 0 | 0 | 24 |

| Major/Minor | Major1 | | | Major2 | | | Minor1 | | | Minor2 | | |
|----------------------|--------|---|---|---------|---|---|--------|-------|-------|--------|---|-------|
| Conflicting Flow All | - | 0 | 0 | 512 | 0 | 0 | 895 | 1260 | 504 | - | - | 309 |
| Stage 1 | - | - | - | - | - | - | 504 | 504 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 391 | 756 | - | - | - | - |
| Critical Hdwy | - | - | - | 4.115 | - | - | 7.33 | 6.53 | 6.23 | - | - | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.13 | 5.53 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.53 | 5.53 | - | - | - | - |
| Follow-up Hdwy | - | - | - | -2.2095 | - | - | 3.519 | 4.019 | 3.319 | - | - | 3.319 |
| Pot Cap-1 Maneuver | 0 | - | - | 1058 | - | - | 248 | 170 | 567 | 0 | 0 | 688 |
| Stage 1 | 0 | - | - | - | - | - | 549 | 540 | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | - | - | - | 606 | 415 | - | 0 | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | 1058 | - | - | 221 | 153 | 567 | - | - | 688 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 221 | 153 | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | 549 | 540 | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | 525 | 373 | - | - | - | - |

| Approach | EB | | | WB | | | NB | | | SB | | |
|----------------------|----|--|--|-----|--|--|------|--|--|------|--|--|
| HCM Control Delay, s | 0 | | | 1.1 | | | 15.3 | | | 10.4 | | |
| HCM LOS | | | | | | | C | | | B | | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | WBR | SBLn1 |
|-----------------------|-------|-----|-----|-------|-----|-----|-------|
| Capacity (veh/h) | 417 | - | - | 1058 | - | - | 688 |
| HCM Lane V/C Ratio | 0.166 | - | - | 0.065 | - | - | 0.036 |
| HCM Control Delay (s) | 15.3 | - | - | 8.6 | 0.3 | - | 10.4 |
| HCM Lane LOS | C | - | - | A | A | - | B |
| HCM 95th %tile Q(veh) | 0.6 | - | - | 0.2 | - | - | 0.1 |

HCM Signalized Intersection Capacity Analysis
5: SR 9 & Soper Hill Rd

White Barn Brown Bear - Marysville
Future (2030) With-Project PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
|-----------------------------------|------|-------|-------|------|------|------|-------|-------|------|------|------|---------------------------|------|
| Lane Configurations | | | | | | | | | | | | | |
| Traffic Volume (vph) | 35 | 66 | 410 | 10 | 96 | 40 | 535 | 1995 | 5 | 10 | 1490 | 15 | |
| Future Volume (vph) | 35 | 66 | 410 | 10 | 96 | 40 | 535 | 1995 | 5 | 10 | 1490 | 15 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 6.1 | 6.1 | 5.5 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1752 | 1845 | 1568 | 1787 | 1881 | 1599 | 3400 | 3504 | | 1736 | 3471 | 1553 | |
| Flt Permitted | 0.62 | 1.00 | 1.00 | 0.71 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1151 | 1845 | 1568 | 1342 | 1881 | 1599 | 3400 | 3504 | | 1736 | 3471 | 1553 | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | |
| Adj. Flow (vph) | 36 | 67 | 418 | 10 | 98 | 41 | 546 | 2036 | 5 | 10 | 1520 | 15 | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 6 | |
| Lane Group Flow (vph) | 36 | 67 | 418 | 10 | 98 | 4 | 546 | 2041 | 0 | 10 | 1520 | 9 | |
| Heavy Vehicles (%) | 3% | 3% | 3% | 1% | 1% | 1% | 3% | 3% | 3% | 4% | 4% | 4% | |
| Turn Type | Perm | NA | pm+ov | Perm | NA | Perm | Prot | NA | | Prot | NA | Prot | |
| Protected Phases | | 4 | 5 | | 8 | | 5 | 2 | | 1 | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | | |
| Actuated Green, G (s) | 10.7 | 10.7 | 25.3 | 11.7 | 11.7 | 11.7 | 14.6 | 88.0 | | 1.2 | 74.6 | 74.6 | |
| Effective Green, g (s) | 10.7 | 10.7 | 25.3 | 11.7 | 11.7 | 11.7 | 14.6 | 88.0 | | 1.2 | 74.6 | 74.6 | |
| Actuated g/C Ratio | 0.09 | 0.09 | 0.21 | 0.10 | 0.10 | 0.10 | 0.12 | 0.74 | | 0.01 | 0.63 | 0.63 | |
| Clearance Time (s) | 6.1 | 6.1 | 5.5 | 5.1 | 5.1 | 5.1 | 5.5 | 7.5 | | 5.5 | 7.5 | 7.5 | |
| Vehicle Extension (s) | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.5 | | 2.0 | 4.5 | 4.5 | |
| Lane Grp Cap (vph) | 103 | 165 | 333 | 131 | 184 | 157 | 417 | 2591 | | 17 | 2175 | 973 | |
| v/s Ratio Prot | | 0.04 | c0.15 | | 0.05 | | c0.16 | c0.58 | | 0.01 | 0.44 | 0.01 | |
| v/s Ratio Perm | 0.03 | | 0.11 | 0.01 | | 0.00 | | | | | | | |
| v/c Ratio | 0.35 | 0.41 | 1.26 | 0.08 | 0.53 | 0.03 | 1.31 | 0.79 | | 0.59 | 0.70 | 0.01 | |
| Uniform Delay, d1 | 50.9 | 51.1 | 46.9 | 48.7 | 51.0 | 48.5 | 52.2 | 9.7 | | 58.7 | 14.7 | 8.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.8 | 2.2 | 137.1 | 0.1 | 1.5 | 0.0 | 155.6 | 1.9 | | 29.3 | 1.2 | 0.0 | |
| Delay (s) | 53.7 | 53.4 | 184.0 | 48.8 | 52.5 | 48.5 | 207.8 | 11.5 | | 87.9 | 15.9 | 8.3 | |
| Level of Service | D | D | F | D | D | D | F | B | | F | B | A | |
| Approach Delay (s) | | 158.2 | | | 51.2 | | | 52.9 | | | 16.3 | | |
| Approach LOS | | F | | | D | | | D | | | B | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 52.5 | | | | | | | | | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | | | 0.98 | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 119.0 | | | | | | | | | Sum of lost time (s) | 24.2 |
| Intersection Capacity Utilization | | | 85.8% | | | | | | | | | ICU Level of Service | E |
| Analysis Period (min) | | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | | |

MOVEMENT SUMMARY

Site: 3 [6. 87th Ave NE/35th St NE WP 2030 (Site Folder: Future WP 2030)]

White Barn Brown Bear
 Site Category: (None)
 Roundabout

| Vehicle Movement Performance | | | | | | | | | | | | | | |
|------------------------------|------|---------------|------|---------------|------|-----------|-------------|------------------|-------------------|-----------|-----------|---------------------|------------------|-------------|
| Mov ID | Turn | INPUT VOLUMES | | DEMAND FLOWS | | Deg. Satn | Aver. Delay | Level of Service | 95% BACK OF QUEUE | | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| | | [Total veh/h | HV % | [Total veh/h | HV % | | | | [Veh. veh | Dist] ft | | | | |
| South: 87th Ave NE | | | | | | | | | | | | | | |
| 8 | T1 | 206 | 2.0 | 219 | 2.0 | 0.263 | 5.3 | LOS A | 1.2 | 31.1 | 0.46 | 0.55 | 0.46 | 36.6 |
| 18 | R2 | 37 | 2.0 | 39 | 2.0 | 0.263 | 5.4 | LOS A | 1.2 | 31.1 | 0.46 | 0.55 | 0.46 | 35.5 |
| Approach | | 243 | 2.0 | 259 | 2.0 | 0.263 | 5.3 | LOS A | 1.2 | 31.1 | 0.46 | 0.55 | 0.46 | 36.4 |
| East: 35th St NE | | | | | | | | | | | | | | |
| 1 | L2 | 88 | 2.0 | 94 | 2.0 | 0.092 | 10.9 | LOS B | 0.5 | 11.8 | 0.40 | 0.65 | 0.40 | 34.0 |
| 16 | R2 | 100 | 2.0 | 106 | 2.0 | 0.103 | 5.2 | LOS A | 0.5 | 13.3 | 0.40 | 0.54 | 0.40 | 35.6 |
| Approach | | 188 | 2.0 | 200 | 2.0 | 0.103 | 7.9 | LOS A | 0.5 | 13.3 | 0.40 | 0.59 | 0.40 | 34.8 |
| North: 87th Ave NE | | | | | | | | | | | | | | |
| 7 | L2 | 325 | 6.0 | 346 | 6.0 | 0.407 | 10.7 | LOS B | 2.6 | 67.8 | 0.36 | 0.62 | 0.36 | 34.3 |
| 4 | T1 | 41 | 6.0 | 44 | 6.0 | 0.407 | 4.8 | LOS A | 2.6 | 67.8 | 0.36 | 0.62 | 0.36 | 34.3 |
| Approach | | 366 | 6.0 | 389 | 6.0 | 0.407 | 10.1 | LOS B | 2.6 | 67.8 | 0.36 | 0.62 | 0.36 | 34.3 |
| All Vehicles | | 797 | 3.8 | 848 | 3.8 | 0.407 | 8.1 | LOS A | 2.6 | 67.8 | 0.40 | 0.59 | 0.40 | 35.0 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Appendix D: Detailed Trip Generation

Marysville Brown Bear - White Barn

| <i>Proposed Use</i> | | | | | | | | | | | | | | | | | | | |
|----------------------------|----------------------------|------------------------|------|-----------|-------|------|-------|------------|-------------|----------|----------|---------|-----|-----|---------------|---------|----------|-------|----|
| Land Use (LU) | ITE LU Number ¹ | Setting | Size | Units | Model | Rate | Units | Inbound % | Gross Trips | | | Pass-By | | | Total Net New | | | | |
| | | | | | | | | | Inbound | Outbound | Subtotal | % | In | Out | Total | Inbound | Outbound | Total | |
| Automated Car Wash | 948 | General Urban/Suburban | | 1 tunnels | | Rate | 77.50 | per tunnel | 50% | 39 | 39 | 78 | 40% | 16 | 16 | 32 | 23 | 23 | 46 |
| PM Peak Hour | | | | | | | | | | | | | | | | | | | |
| Touchless Car Wash | Observations ² | General Urban/Suburban | | 5 bays | | Rate | 13.68 | per bay | 51% | 35 | 33 | 68 | 40% | 14 | 14 | 28 | 21 | 19 | 40 |
| PM Peak Hour | | | | | | | | | | | | | | | | | | | |
| <u>Subtotal</u> | | | | | | | | | | 74 | 72 | 146 | | 30 | 30 | 60 | 44 | 42 | 86 |

Notes:

1. Trip rates based on Institute of Transportation Engineers' (ITE) *Trip Generation* 11th Edition equation and average trip rate as shown above.

2. Trip rates based on observations at existing touchless car washes in the area as touchless car washes are not consistent with uses available in ITE. Observations were completed in 2022 at 3 different facilities during the PM peak period (4-6pm) for 2 mid-weekdays.

Appendix E: Poisson Queuing Analysis

Poisson Queuing - PM Peak Hour (Tunnel)

| | | |
|------------------------------------|-------|---------------------------|
| Number of Service Channels (lanes) | 1 | |
| Hourly Flow Rate (vph) | 39 | per channel |
| Total Hourly Flow Rate | 39 | vehicles per hour |
| Average Stopped Time | 6:00 | (mm:ss) |
| Average arrival rate | 3.900 | vehicles per stopped time |

| Probability of <i>(n)</i> or more vehicles in System | Vehicles <i>(n)</i> | 50th-Percentil | 85th-Percentil | 95th-Percentil |
|--|---------------------|----------------|----------------|----------------|
| 0.980 | 0 | | | |
| 0.980 | 1 | | | |
| 0.901 | 2 | | | |
| 0.747 | 3 | | | |
| 0.547 | 4 | | | |
| 0.352 | 5 | 5 veh | | |
| 0.199 | 6 | | | |
| 0.101 | 7 | | 7 veh | |
| 0.045 | 8 | | | 8 veh |
| 0.019 | 9 | | | |
| 0.007 | 10 | | | |
| 0.002 | 11 | | | |
| 0.001 | 12 | | | |
| 0.000 | 13 | | | |
| 0.000 | 14 | | | |
| 0.000 | 15 | | | |
| 0.000 | 16 | | | |
| 0.000 | 17 | | | |
| 0.000 | 18 | | | |
| 0.000 | 19 | | | |
| 0.000 | 20 | | | |
| 0.000 | 21 | | | |
| 0.000 | 22 | | | |
| 0.000 | 23 | | | |
| 0.000 | 24 | | | |
| 0.000 | 25 | | | |

Poisson Queuing - PM Peak Hour (Touchless)

| | | |
|------------------------------------|-------|-------------------------------------|
| Number of Service Channels (lanes) | 5 | |
| Hourly Flow Rate (vph) | 6.84 | per channel (<i>INBOUND ONLY</i>) |
| Total Hourly Flow Rate | 34 | vehicles per hour |
| Average Stopped Time | 6:00 | (mm:ss) |
| Average arrival rate | 3.400 | vehicles per stopped time |

| Probability of <i>(n)</i> or more vehicles in System | Vehicles <i>(n)</i> | 50th-Percentile | 85th-Percentil | 95th-Percentil |
|--|---------------------|-----------------|----------------|----------------|
| 0.967 | 0 | | | |
| 0.967 | 1 | | | |
| 0.853 | 2 | | | |
| 0.660 | 3 | | | |
| 0.442 | 4 | 4 veh | | |
| 0.256 | 5 | | | |
| 0.129 | 6 | | 6 veh | |
| 0.058 | 7 | | | |
| 0.023 | 8 | | | 8 veh |
| 0.008 | 9 | | | |
| 0.003 | 10 | | | |
| 0.001 | 11 | | | |
| 0.000 | 12 | | | |
| 0.000 | 13 | | | |
| 0.000 | 14 | | | |
| 0.000 | 15 | | | |
| 0.000 | 16 | | | |
| 0.000 | 17 | | | |
| 0.000 | 18 | | | |
| 0.000 | 19 | | | |
| 0.000 | 20 | | | |
| 0.000 | 21 | | | |
| 0.000 | 22 | | | |
| 0.000 | 23 | | | |
| 0.000 | 24 | | | |
| 0.000 | 25 | | | |