# English Crossing <br> Marysville, WA 

## UPDATED

Traffic Impact Analysis
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## FINDINGS/CONCLUSIONS

This updated traffic impact analysis (TIA) has been prepared for the proposed English Crossing project in the Lakewood area of the City of Marysville, WA. This study has been updated based on comments received from the City of Marysville dated June 20, 2023 in response to review of the initial TIA dated April 24, 2023.

Project Proposal. The proposed English Crossing project site is located west of 19th Ave NE and north of $172^{\text {nd }}$ Street NE. The proposed project will include up to 250 Single-Family Attached townhome units on a site that is currently vacant.

Vehicular access to the site would be provided be provided via a new site access roadway connection to 19th Ave NE, aligned with $174^{\text {th }}$ Street NE. Secondary access for emergency vehicles only would be provided north of $174^{\text {th }}$ Street NE via another new site access roadway connection to $19^{\text {th }}$ Ave NE.

Trip Generation. The English Crossing project is estimated to generate 1,855 new weekday daily trips, with 124 new trips ( 31 in, 93 out) occurring during the AM peak hour and 146 new trips ( 86 in, 60 out) occurring during the PM peak hour.

Intersection Level of Service (LOS). The LOS analyses documented in this report were assessed during the weekday PM peak hour at seven (7) off-site study intersections. The City of Marysville and WSDOT LOS standard at all study intersections is LOS D with one exception, as noted in the City of Marysville Traffic Impact Analysis Guidelines, which state that intersections on the $172^{\text {nd }}$ Street NE (SR 531 ) corridor that have an existing LOS E prior to development submittal shall only be required to mitigate upon falling below LOS E.

All study intersections are anticipated to operate at LOS D or better in 2026 (buildout year) and 2032 (horizon year) during the weekday PM peak hour without or with the proposed project with one exception: the intersection of $27^{\text {th }}$ Avenue NE / $172^{\text {nd }}$ Street NE which is anticipated to operate at LOS E in 2026 and LOS F in 2032 (without or with the proposed project).
The City's long-term plan for addressing this future LOS condition at the $27^{\text {th }}$ Avenue NE/172nd Street NE intersection is the $156^{\text {th }}$ Street NE Interchange project planned by WSDOT (TIP \#61). The $156^{\text {th }}$ Street NE interchange with $1-5$ is expected to shift some traffic away from the $27^{\text {th }}$ Avenue NE/172 nd Street NE intersection, reducing demand on the $172^{\text {nd }}$ Street NE corridor and improving LOS at this intersection and other intersections along the $172^{\text {nd }}$ Street corridor. Until funding is identified for the $156^{\text {th }}$ Street NE interchange, the $27^{\text {th }}$ Avenue $\mathrm{NE} / 172^{\text {nd }}$ Street NE intersection is anticipated to function at LOS E or F during peak hours in the future with or without this project.
Additionally, and in response to City comments, several transportation improvement options were considered at the $27^{\text {th }}$ Avenue NE/172 ${ }^{\text {nd }}$ Street NE intersection in 2032 with the proposed English Crossing project such as eastbound and southbound rightturn lanes, a dual northbound right-turn lane, and a two-lane roundabout. Based on this preliminary alternative analysis, it is anticipated that adding a second northbound right-turn lane (resulting in dual northbound right-turn lanes) would be the most optimal improvement to reduce delay at the $27^{\text {th }}$ Avenue NE/172nd Street NE intersection. To accomplish this improvement, the City would have to provide sufficient right of way for the second turn lane.

Site Access Evaluation. The LOS results indicate that the individual movements at the proposed site access intersection are expected to operate at LOS B or better with minimal queuing during the weekday PM peak hour in 2026 (buildout year) and 2032 (horizon year).

Future City Road Plans. The City of Marysville has identified several future road improvements and connections in the vicinity of the project site. These connector roads are identified on the City's Comprehensive Plan, City's Lakewood Neighborhood Plan, the City's six-year 2023-2028 Transportation Improvement Plan (TIP), and/or the City's traffic impact fee program. The following eight (8) City planned road improvements were identified in the study area.

- $172^{\text {nd }}$ Street NE $/ 1^{\text {th }}$ Avenue NE Roundabout - construct new roundabout at $19^{\text {th }}$ Avenue NE / 172 ${ }^{\text {nd }}$ Street NE (Marysville TIP Project \#24)
- $172^{\text {nd }}$ Street NE $/ 11^{\text {th }}$ Avenue NE Roundabout - construct new roundabout at $11^{\text {th }}$ Avenue NE / 172nd Street NE (Marysville TIP Project \#25)
- $172^{\text {nd }}$ Street NE from $27^{\text {th }}$ Avenue NE to $19^{\text {th }}$ Avenue NE - widen to a $4 / 5$-lane section with pedestrian and bicycle facilities between $27^{\text {th }}$ Avenue NE and $19^{\text {th }}$ Avenue NE. (Marysville TIP Project \#30)
- $172^{\text {nd }}$ Street NW from $19^{\text {th }}$ Drive NE to $11^{\text {th }}$ Avenue NE - widen to a 3-lane section with pedestrian and bicycle facilities between 19th Drive NE and $11^{\text {th }}$ Avenue NE. (Marysville TIP Project \#31)
- $172^{\text {nd }}$ Street NE Railroad Crossing - widen to a 3-lane section with pedestrian and bicycle facilities and railroad crossing improvements; this project is unfunded. (Marysville TIP Project \#36)
- New 19th Avenue NE Extension - construct new 3-lane roadway between $156^{\text {th }}$ Street NE and $172^{\text {nd }}$ Street NE that would include pedestrian and bicycle facilities. (Marysville TIP Project \#5 1)
- $156^{\text {th }}$ Street NE Interchange - convert existing overcrossing to a full single-point urban interchange (SPUI) with Interstate 5. (Marysville TIP Project \#61)
- New 23rd Avenue NE and $169^{\text {th }}$ Street NE - construct new 3-lane roadways connecting to the existing street network at the existing roundabout at $23^{\text {rd }}$ Avenue NE / $172^{\text {nd }}$ Street NE and the existing western terminus of 169th Street NE. (Marysville TIP Project \#48)

Note that portions of some of these City improvements would be completed by the English Crossing project as mitigation, which is further described in the Mitigation section next.

Mitigation. The following measures have been identified to mitigate traffic impacts of the proposed English Crossing project.

- City of Marysville Traffic Impact Fees. The City of Marysville requires payment of transportation impact fees to help fund planned roadway improvements throughout the City. Transportation impact fees for the proposed English Crossing project were calculated based on the trip generation estimate documented in this TIA and the City of Marysville's currently adopted transportation impact fee rate of $\$ 6,300$ per PM peak hour trip.
The proposed English Crossing project is estimated to generate 146 new PM peak hour trips. As a result, the estimated City of Marysville transportation impact fee is $\$ 919,8001 \$ 6,300 \mathrm{X}$ 146 PM peak hour trips). Actual impact fees will be calculated by the City at the time of building permit issuance.
- $27^{\text {th }}$ Ave NE/172nd Street NE Intersection. This intersection is anticipated to operate at LOS F in the future 2032 horizon year PM peak hour as a result of the funding loss for the 156 th Street NE interchange with 1-5. A couple options that should be considered by the City include: (1) adding a $2^{\text {nd }}$ northbound right-turn lane, and/or (2) allowing the intersection operation to exceed the LOS threshold until funding for the $156^{\text {th }}$ Street NE interchange is funded.
- Snohomish County Mitigation. The City of Marysville and Snohomish County have adopted an interlocal agreement whereby developments in Marysville must assess potential mitigation for impacts on Snohomish County roadway facilities. Mitigation fees to Snohomish County are based on predetermined distribution percentages according to location or specific project impacts to planned roadway improvements.

Mitigation fees to Snohomish County were based on the use of the standard distribution percentage based on the project location (20\%) multiplied by the daily trip generation (1,855 new daily project trips) and adopted cost per ADT ( $\$ 185$ for residential developments within TSA A and the UGA). The resulting Snohomish County transportation impact fee is $\$ 68,635$. A mitigation offer form to Snohomish County will be submitted separately.

- Future City Road Plans. The English Crossing project would build a portion of the following City planned roadway improvements:
- Construct and dedicate right-of-way for the western half-street of a 3-lane section on 19th Avenue NE from 172 ${ }^{\text {nd }}$ Street NE to the northern site property line.
- Construct and dedicate right-of-way for the northern half-street of a 3-lane section on $172^{\text {nd }}$ Street NE from $19^{\text {th }}$ Avenue NE to the western site property line.
- Construct a new roundabout (or a portion of a new roundabout) at 19th Avenue NE / $172^{\text {nd }}$ Street NE if not already completed by other development.

It should be noted that it is anticipated the applicant would receive transportation impact fee credit for construction and ROW dedication of these roadway construction projects as confirmed by the City.

## INTRODUCTION

This updated traffic impact analysis (TIA) has been prepared for the proposed Eng/ish Crossing project located in the Lakewood area of the City of Marysville, WA. The proposed project will include up to 250 SingleFamily Attached townhome units on a currently vacant site. A site vicinity map is provided in Figure 1. This study has been updated based on comments received from the City of Marysville dated June 20, 2023 in response to review of the initial TIA dated April 24, 2023.

## Project Description

The proposed project will include up to 250 Single-Family Attached townhome units on a currently vacant site. Vehicular access to the site would be provided be provided via a new site access roadway connection to $19^{\text {th }}$ Ave NE, aligned with $174^{\text {th }}$ Street NE. Secondary access for emergency vehicles only would be provided north of $174^{\text {th }}$ Street NE via another new site access roadway connection to $19^{\text {th }}$ Ave NE. A preliminary site plan is shown in Figure 2.

## Traffic Scoping \& Study Area

The scope of work for this Traffic Impact Analysis was prepared consistent with City of Maryville's adopted Traffic Impact Analysis guidelines (December 2021) and confirmed by the City during the scoping process. A total of seven (7) off-site study intersections were identified for evaluation during future weekday PM peak hour conditions in 2026 (buildout year) and 2032 (horizon year):

1. $11^{\text {th }}$ Ave NE $/ 172^{\text {nd }}$ St NE
2. $19^{\text {th }}$ Dr NE / $172^{\text {nd }} \mathrm{St} \mathrm{NE}$
3. $19^{\text {th }}$ Ave NE / 172nd St NE
4. $23^{\text {rd }}$ Ave NE $/ 172^{\text {nd }} \mathrm{St} \mathrm{NE}$
5. $27^{\text {th }}$ Ave NE $/ 172^{\text {nd }} \mathrm{St}$ NE
6. $1-5$ SB Ramps $/ 172^{\text {nd }}$ St NE
7. $1-5$ NB Ramps $/ 172^{\text {nd }} \mathrm{St} \mathrm{NE}$

## Project Approach

To analyze the traffic impacts of the English Crossing development, the following tasks were undertaken:

- Assessment of existing conditions through field reconnaissance and review of existing planning documents.
- Estimation of weekday vehicular AM peak hour, PM peak hour, and weekday daily trips generated by the development.
- Evaluation of weekday PM peak hour level of service (LOS) at seven (7) off-site study intersections.
- Analyzed the weekday PM peak hour operations at the proposed site access intersection including LOS and queues. Review of City planning documents to evaluate long-term road improvements plans in project vicinity.
- Documentation of trip impacts at Snohomish Countr Key Intersections.
- Summary of mitigation including transportation impact fees to City of Marysville and Snohomish Countr, and construction of local roadway improvements adjacent to the site.


## Primary Data and Information Sources

- Institute of Transportation Engineers (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition, 2021.
- City of Marysville Traffic Impact Analysis Guidelines, December 22, 2021.
- Highway Capacity Manual (HCM 6 Edition), 2016.
- 2022 and 2023 weekday PM peak period traffic counts, All Traffic Data (ATD).
- City of Marysville 2023-2028 Six Year Transportation Improvement Plan (TIP).
- City of Marysville Comprehensive Plan - Transportation Element, 2015.
- Snohomish County Traffic Worksheet and Traffic Study Requirements for Developments in the City of Marysville, October 2015.


Figure 1: Project Site Vicinity


## EXISTING CONDITIONS

This section describes existing transportation system conditions in the study area. Existing conditions described include an inventory of existing roadways, public transportation services, non-motorized transportation facilities, existing traffic volumes, and intersection levels of service (LOS).

## Roadway Network

The existing street characteristics in the vicinity of the proposed English Crossing project are described below in Table 1.

## Table 1 <br> Existing Roadway Network Summary - Project Site Vicinity

| Roadway | Orientation | Classification | Speed Limit | Number of Travel Lanes | Street <br> Parking | Sidewalks | Bicycle Facilities |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 172^{\text {nd }} \text { St NE } \\ \text { (SR 531) } \end{gathered}$ | East-West | State Highway | 35 mph | 3-4 | None | Intermittent | Intermittent Bike Lanes |
| 19 ${ }^{\text {th }}$ Ave NE | North-South | Collector Arterial | 35 mph | 2 | None | None | None |
| $23{ }^{\text {rd }}$ Ave NE | North-South | Minor Arterial | 25 mph | 2 | None | Both Sides | None |
| $27^{\text {th }}$ Ave NE | North-South | Minor Arterial | 25 mph | 2 | None | None | None |

## Transit Service

Transit service in the project site vicinity is provided by Community Transit. The closest bus stops are located on $172^{\text {nd }}$ Street NE at $19^{\text {th }}$ Drive NE and $23^{\text {rd }}$ Ave NE. The bus stops provide access to Community Transit Route 240 which provides service between Stanwood Downtown Park \& Ride and Smokey Point Transit Center throughout the day with approximately 1 -hour headways.

## Non-motorized Transportation Facilities

Non-motorized transportation facilities in the project site vicinity include a mix of sidewalks and paved shoulders. Existing pedestrian activity is minimal in the project vicinity based on recent PM peak period traffic counts.

## Collision History

Historical collisions at the seven (7) off-site study intersections and seven (7) roadway segments were analyzed for the four-year period from 2019 to 2022. Collision data was provided by WSDOT. Summaries of the total and yearly average collisions during this period at the off-site study intersections are provided in Table 2. Summaries of collisions by type at the off-site study intersections are provided in Table 3. Summaries of the total and yearly average collisions along the roadway segments are provided in Table 4.
The detailed collision history is included in Appendix A.

Table 2
Collision Data Summary, January 1, 2019, to December 31, 2022

| Roadway Segment | $\frac{a}{o}$ | 웅 | N্N | N N | 4-Year Total Collisions | Avg. <br> Annual Collisions | Est. AWDT ${ }^{1}$ | Collisions per $M E V^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1) $11^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 0 | 1 | 2 | 1 | 4 | 1.00 | 7,030 | 0.39 |
| 2) $19^{\text {th }} \mathrm{Dr} \mathrm{NE} / 172^{\text {nd }} \mathrm{St}$ NE | 1 | 2 | 1 | 0 | 4 | 1.00 | 8,090 | 0.34 |
| 3) $19^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 0 | 2 | 3 | 2 | 7 | 1.75 | 8,360 | 0.57 |
| 4) $23^{\text {rd }}$ Ave NE / $172^{\text {nd }}$ St NE | 0 | 1 | 2 | 3 | 6 | 1.50 | 15,420 | 0.27 |
| 5) $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 7 | 5 | 7 | 4 | 23 | 5.75 | 35,750 | 0.44 |
| 6) I-5 SB Ramps / $172^{\text {nd }}$ St NE | 8 | 4 | 7 | 8 | 27 | 6.75 | 39,750 | 0.46 |
| 7) I-5 NB Ramps / 172 ${ }^{\text {nd }}$ St NE | 5 | 6 | 3 | 7 | 21 | 5.25 | 44,570 | 0.32 |

Source: WSDOT Collision Records.
${ }^{1}$ AWDT = Average Weekday Daily Traffic. Estimated daily volumes are based on 2022/2023 PM volumes and a K-factor of 10. ${ }^{2}$ MEV $=$ Million Entering Vehicles.

Table 3
Collision Data Summary by Type, January 1, 2019 to December 31, 2022

| Intersection | Collision Type |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ㄷ $\frac{5}{0}$ $\frac{0}{0}$ $\frac{4}{4}$ $\frac{0}{0}$ $\frac{0}{0}$ $\frac{\square}{4}$ $\frac{1}{4}$ | $E$ $\frac{0}{0}$ $\frac{C}{4}$ | $\begin{aligned} & \text { ᄃ } \\ & \text { ì } \\ & \frac{1}{0} \\ & 0 \\ & \hline 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \bar{\oplus} \\ & \stackrel{1}{5} \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \underset{O}{\bar{O}} \\ & \stackrel{1}{0} \\ & \overline{0} \\ & \mathbb{D} \end{aligned}$ | 0 .0 3 0 0 0 0 |
| 1) $11^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2) $19^{\text {th }} \mathrm{Dr} \mathrm{NE} / 172^{\text {nd }}$ St NE | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3) $19^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4) $23^{\text {rd }}$ Ave NE / $172^{\text {nd }}$ St NE | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 5) $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | 1 | 1 | 0 | 0 | 0 | 0 | 3 | 0 |
| 6) I-5 SB Ramps / $172{ }^{\text {nd }}$ St NE | 3 | 0 | 0 | 0 | 0 | 0 | 4 | 1 |
| 7) I-5 NB Ramps / 172 ${ }^{\text {nd }}$ St NE | 3 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |

[^0]
## Table 4

Collision Data Summary, January 1, 2019, to December 31, 2022

| Roadway Segment | $\frac{\alpha}{\circ}$ | 응 | 드N | N্N | 4-Year Total Collisions | Avg. <br> Annual Collisions | Est. AWDT ${ }^{1}$ | Collisions per MEV ${ }^{2}$ | Collisions per MVM ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $172^{\text {nd }}$ St NE between |  |  |  |  |  |  |  |  |  |
| $11^{\text {th }}$ Ave NE and $19^{\text {th }}$ Dr NE | 5 | 0 | 0 | 0 | 5 | 1.25 | 7,100 | 0.48 | 1.30 |
| $19^{\text {th }}$ Dr NE and $19^{\text {th }}$ Ave NE | 2 | 3 | 2 | 0 | 7 | 1.75 | 8,040 | 0.60 | 4.97 |
| $19^{\text {th }}$ Ave NE and $23{ }^{\text {rd }}$ Ave NE | 3 | 5 | 3 | 1 | 12 | 3.00 | 9,800 | 0.84 | 3.35 |
| $23^{\text {rd }}$ Ave NE and $27^{\text {th }}$ Ave NE | 5 | 3 | 8 | 3 | 19 | 4.75 | 14,680 | 0.89 | 3.55 |
| $27^{\text {th }}$ Ave NE and l-5 SB Ramps | 5 | 3 | 5 | 5 | 18 | 4.50 | 30,590 | 0.40 | 3.10 |
| I-5 SB Ramps and l-5 NB Ramps | 0 | 3 | 11 | 7 | 30 | 7.50 | 32,310 | 0.64 | 3.74 |
| $19^{\text {th }}$ Ave NE between |  |  |  |  |  |  |  |  |  |
| $174^{\text {th }}$ Street NE and $172^{\text {nd }}$ St NE | 0 | 0 | 0 | 0 | 0 | 0.00 | 920 | 0.00 | 0.00 |

Source: WSDOT Collision Records.
${ }^{1}$ AWDT = Average Weekday Daily Traffic. Estimated daily volumes are based on 2022/2023 PM volumes and a K-factor of 10.
${ }^{2} \mathrm{MEV}=$ Million Entering Vehicles.
${ }^{3} \mathrm{MVM}=$ Million Vehicle Miles.
Per the City of Marysville's Traffic Impact Analysis Guidelines (December 2021) intersection collision rates over 1.0 collision per MEV and roadway segment collision rates over 10.0 collisions per MEV generally warrant further review to determine if any patterns exist. Based on the collision data, none of the seven (7) off-site study intersections have rates that exceed 1.0 collision per MEV. Additionally, none of the seven (7) roadway segments have rates that exceed 10.0 collisions per MEV or 10.0 collisions per MVM.

## Traffic Volumes

Existing weekday PM peak hour traffic volumes at the seven (7) off-site study intersections were based on counts conducted by All Traffic Data in 2022 and 2023. The PM peak hour represents the highest one-hour time period between 4:00 and 6:00 PM. To estimate existing 2023 traffic volumes, a three (3) percent annual growth rate was applied to the 2022 traffic volumes, consistent with City of Marysville guidelines. Figure 3 illustrates the estimated 2023 existing weekday PM peak hour traffic volumes at the seven (7) offsite study intersections. Appendix B includes the PM peak hour traffic count data sheets.


Figure 3: 2023 Existing PM Peak Hour Traffic Volumes

## Intersection Levels of Service

LOS generally refers to the degree of congestion on a roadway or intersection. It is a measure of vehicle operating speed, travel time, travel delays, and driving comfort. A letter scale from A to F generally describes intersection LOS. At signalized intersections, LOS A represents free-flow conditions (motorists experience little or no delays), and LOS F represents forced-flow conditions where motorists experience an average delay in excess of 80 seconds per vehicle.

The LOS reported for signalized intersections represents the average control delay (sec/veh) and can be reported for the overall intersection, for each approach, and for each lane group (additional v/c ratio criteria apply to lane group LOS only).

The LOS reported at stop-controlled intersections is based on the average control delay and can be reported for each controlled minor approach, controlled minor lane group, and controlled major-street movement land for the overall intersection at all-way stop controlled intersections. Additional v/c ratio criteria apply to lane group or movement LOS only). Table 5 outlines the current HCM $6^{\text {th }}$ Edition LOS criteria for signalized and stop-controlled intersections based on these methodologies.

## Table 5

LOS Criteria for Signalized and Two-Way Stop Controlled Intersections ${ }^{1}$

| SIGNALIZED INTERSECTIONS |  |  | UNSGINALIZED INTERSECTIONS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS by Volume-to Capacity (V/C) Ratio ${ }^{2}$ |  |  | LOS by Volume-to Capacity (V/C) Ratio ${ }^{3}$ |  |
| Control Delay (sec/veh) | $\leq 1.0$ | > 1.0 | Control Delay (sec/veh) | $\leq 1.0$ | > 1.0 |
| $\leq 10$ | A | F | $\leq 10$ | A | F |
| $>10$ to $\leq 20$ | B | F | $>10$ to $\leq 15$ | B | F |
| $>20$ to $\leq 35$ | C | F | $>15$ to $\leq 25$ | C | F |
| $>35$ to $\leq 55$ | D | F | $>25$ to $\leq 35$ | D | F |
| $>55$ to $\leq 80$ | E | F | $>35$ to $\leq 50$ | E | F |
| $>80$ | F | F | $>50$ | F | F |

${ }^{1}$ Source: Highway Capacity Manual (6 $6^{\text {th }}$ Edition), Transportation Research Board, 2016.
${ }^{2}$ For approach-based and intersection-wide assessments at signals, LOS is defined solely by control delay.
${ }^{3}$ For two-way stop controlled intersections, the LOS criteria apply to each lane on a given approach and to each approach on the minor street. LOS is not calculated for major-street approaches or for the intersection as a whole at two-way stop controlled intersections. For approach-based and intersection-wide assessments at all-way stop controlled intersections, LOS is solely defined by control delay.

Level of service calculations for signalized and stop-controlled study intersections were based on methodology and procedures outlined in the latest Highway Capacity Manual (6th Edition) using Synchro 77 traffic analysis software. Existing signal timing was provided by WSDOT and City of Marysville at the signalized study intersections. Level of service calculations for the roundabout study intersections were based on WSDOT methodology and procedures outlined in the WSDOT Sidra Policy Settings document using Sidra 9 traffic analysis software. The existing LOS results at the seven (7) off-site study intersections are summarized in Table 6. Detailed LOS summary worksheets are provided in Appendix C.

Table 6
2023 Existing Weekday PM Peak Hour LOS Summary
Study Intersection / Movement LOS Delay (sec)

Stop-Controlled Intersections:

1) $11^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE

Eastbound Left-Turn A 8.1
Westbound Left-Turn A 7.8
Northbound Approach B 11.6
Southbound Approach B 13.8
2) $19^{\text {th }} \operatorname{Dr~NE} / 172^{\text {nd }}$ St NE

Westbound Left-Turn A 8.0
Northbound Approach B 10.6
3) $19^{\text {th }}$ Ave NE $/ 172^{\text {nd }}$ St NE

Eastbound Left-Turn A 8.7
Southbound Approach B 14.1
Roundabout:
4) $23^{\text {rd }}$ Ave NE / $172^{\text {nd }}$ St NE A 4.3

Signalized Intersections:
5) $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE E 63.4
6) $1-5$ SB $/ 172^{\text {nd }}$ St NE A 6.9
7) I-5 NB / $172^{\text {nd }} S+$ NE C 21.2

As shown in Table 6, all study intersections operate at LOS C or better during the weekday PM peak hour under 2023 existing conditions with the exception of the following intersection:

The City of Marysville and WSDOT LOS standard at intersections is LOS D with one exception. The City of Marysville Traffic Impact Analysis Guidelines state that intersections on the 172nd Street NE (SR 531 ) corridor which have an existing LOS E prior to development submittal shall only be required to mitigate upon falling below LOS E. Currently the $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE intersection operates at LOS E, which applies to this statement.

## FUTURE CONDITIONS \& PROJECT IMPACTS

This section of the report describes the traffic impacts of the proposed English Crossing project on the surrounding and adjacent road network, and at identified off-site study intersections in the project site vicinity. The analysis of traffic impacts includes a trip generation estimate, distribution/assignment of project trips, and PM peak hour LOS evaluation at the seven (7) off-site study intersections and the site access. Consideration of future planned roadway projects identified by the City of Marysville is also documented and considered in the evaluation of intersection LOS.

## Future Planned Roadway Improvements

## Marysville Comprehensive Plan

The Transportation Element of the City of Marysville Comprehensive Plan 2015 includes a depiction of the functional classification of existing and planned future roadways within the City limits and adjacent jurisdictions. The planned roadways are intended to serve anticipated growth in Marysville and the surrounding area through 2035.

## Marysville's Lakewood Neighborhood Master Plan

The City's Lakewood Neighborhood Master Plan (dated March 2017) cites that it is "consistent with the Marysville Comprehensive Plan and provides additional detail for the Lakewood Neighborhood. This plan focuses on the infrastructure and urban design aspects of the neighborhood."
The Neighborhood Roadways section of the Plan identifies roadway improvements to support growth in vehicular and non-motorized demand. The Plan further states that the neighborhood roads create network of minor and collector arterials that create a secondary network to provide alternate routes to $172^{\text {nd }}$ Street NE and $27^{\text {th }}$ Ave NE, and also supports the City's vision of a second $1-5$ interchange at $156^{\text {th }}$ Street NE.

The Lakewood Neighborhood Master Plan identifies a similar system of north-south and east-west arterials (collector and minor) that were also identified in the City's Comprehensive Plan Transportation Element.
It should be noted that the roadway alignments shown in the Lakewood Neighborhood Master Plan and the City's Comprehensive Plan are intended to represent a planned roadway connection and not necessarily the exact alignment for a planned future roadway. The City's six-year Transportation Improvement Plan (TIP), which is typically adopted annually, implements the elements of the City Comprehensive Plan and Lakewood Neighborhood Plan; that plan is described next.

## Marysville Transportation Improvement Plan

The City's plan for funding and implementing new roadway and intersection improvement projects that come out of the Comprehensive Plan and Neighborhood Master Plans is administered through a six-year Transportation Improvement Plan which is typically adopted and updated annually.
Based on review of the currently adopted City of Marysville 2023-2028 Six Year Transportation Improvement Plan (TIP), there are eight (8) planned improvements in the vicinity of the English Crossing project that impact the off-site study intersections or connectivity of the adjacent street network.
Most of these projects are included in the City's Transportation Element of the Comprehensive Plan, the City's Lakewood Neighborhood Master Plan, and the City's Traffic Impact Fee program.

The eight (8) planned improvements in the vicinity of the English Crossing project that impact the off-site study intersections or connectivity of the adjacent street network are as-follows:

- Marysville TIP \#24-172nd Street NE / 19 th Avenue NE Roundabout - construct new roundabout at the $19^{\text {th }}$ Avenue NE / $172^{\text {nd }}$ Street NE intersection. The project is anticipated to be funded by new development in the vicinity.

Note: this improvement is required as a condition of approval for the Lodge Apartments project and is expected to be a condition of approval for English Crossing. As such, this improvement is assumed to be completed in the 2026 No Action and 2026 With Project scenarios.

- Marysville TIP \#25-172nd Street NE / $11^{\text {th }}$ Avenue NE Roundabout - construct new roundabout at the $11^{\text {th }}$ Avenue NE / $172^{\text {nd }}$ Street NE intersection. The project is anticipated to be funded by new development in the vicinity.
Note: this project is not yet a condition of approval of any development and is not otherwise funded. Therefore, this improvement is not assumed in the future roadway network or traffic analysis herein.
- Marysville TIP \#30 - 172 nd Street NE: 27 ${ }^{\text {th }}$ Avenue NE to $19^{\text {th }}$ Avenue NE - widen $172^{\text {nd }}$ Street NE from a 3-lane section to a 4/5-lane section with pedestrian and bicycle facilities between $27^{\text {th }}$ Avenue NE and $19^{\text {th }}$ Avenue NE. The project is anticipated to be funded by new development in the vicinity.
Note: this improvement is assumed to be completed in the 2032 No Action and 2032 With Project scenarios only.
- Marysville TIP \#31-172nd Street NE: $11^{\text {th }}$ Avenue NE to $19^{\text {th }}$ Drive NE - widen $172^{\text {nd }}$ Street NE from a 2 -lane section to a 3 -lane section with pedestrian and bicycle facilities between $11^{\mathrm{th}}$ Avenue NE and 19ih Drive NE. The project is anticipated to be funded by new development in the vicinity. Note: this improvement is assumed to be completed along the English Crossing project frontage in the 2032 No Action and 2032 With Project scenarios only.
- Marysville TIP \#36-172 ${ }^{\text {nd }}$ Street NE Railroad Crossing Improvements - widen 172 ${ }^{\text {nd }}$ Street NE from a 2-lane section to a 3-lane section with pedestrian and bicycle facilities and provide railroad crossing improvements.

Note: this project is not yet a condition of approval of any development and is not otherwise funded. Therefore, this improvement is not assumed in the future roadway network.

- TIP \#48-23rd Avenue NE \& 169th Street NE - construct new 3-lane roadways including pedestrian and bicycle facilities. Connections to the existing street network would be provided at the existing roundabout at $23^{\text {rd }}$ Avenue NE / 172 ${ }^{\text {nd }}$ Street NE and the existing western terminus of 169th Street NE. The project is anticipated to be funded by new development in the vicinity.
Note: this project is not yet a condition of approval of any development and is not otherwise funded. Therefore, this improvement is not assumed in the future roadway network or traffic analysis herein.
- TIP \#51 - $19^{\text {th }}$ Avenue NE Extension from $156^{\text {th }}$ Street NE to $172^{\text {nd }}$ Street NE - construct new 3lane roadway between $156^{\text {th }}$ Street NE and $172^{\text {nd }}$ Street NE that would include pedestrian and bicycle facilities. The project is anticipated to be funded by new development in the vicinity.
Note: this improvement is assumed to be completed in the 2032 No Action and 2032 With Project scenarios only.
- TIP \#61 - 156 th Street NE Interchange - convert the existing road overcrossing at $156^{\text {th }}$ Street NE and Interstate 5 to a full single-point urban interchange (SPUI). The project is funded under Connecting Washington and WSDOT is the lead agency.
Note: the recent Washington State transportation budget delays the start of construction of the $156^{\text {th }}$ Street NE Interchange project indefinitely past 2030. Therefore, this improvement is not assumed in the future roadway network or traffic analysis herein although it is still in the City's current TIP list.


## Project Trip Generation

Trip generation estimates associated with full buildout of the proposed English Crossing project for weekday daily, AM peak hour, and PM peak hour were based on methodology documented in the Institute of Transportation Engineers (ITE) Trip Generation Manual, 11 th Edition for Land Use Code (LUC) 215 (SingleFamily Attached Housing). Table 7 summarizes the net new weekday daily, AM peak hour, and PM peak hour trip generation. Detailed trip generation estimates are provided in Appendix D.

Table 7
English Crossing - Trip Generation Summary

|  | New Trips Generated |  |  |
| :--- | :---: | :---: | :---: |
| Time Period | In | Out | Total |
| Weekday Daily | 927 | 928 | 1,855 |
| Weekday AM Peak Hour | 31 | 93 | 124 |
| Weekday PM Peak Hour | 86 | 60 | 146 |

## Project Trip Distribution and Assignment

The distribution of project-generated trips during the weekday PM peak hour was estimated based on traffic model distribution figures provided by the City of Marysville. These figures are included in Appendix E. The model distribution was used to assign the new weekday PM peak hour (86 inbound and 60 outbound) trips generated by the English Crossing project to the adjacent street network. Based on the trip distribution percentages, new PM peak hour project trips were assigned through the study intersections. The distribution and assignment of the new weekday PM peak hour trips through study intersections are shown in Figure 4.

## Future Traffic Volumes

Future year 2026 and 2032 No Action PM peak hour traffic volumes were estimated by applying a three (3) percent annual growth rate to the existing traffic counts, consistent with City of Marysville guidelines. No additional pipeline projects were included in the 2026 and 2032 No Action volumes since a three (3) percent annual growth rate was used, which is also consistent with City of Marysville guidelines.

It should be noted that based on City comments reviewing the prior TIA, no future adjustments to baseline traffic volumes were made to account for the future planned $156^{\text {th }}$ Street interchange with $1-5$ since it is not currently funded. The resulting future 2026 (buildout year) and 2032 horizon year No Action PM peak hour traffic volumes at the seven (7) off-site study intersections are shown in Figures 5 and 7, respectively. The 2026 and 2032 With Project traffic volumes were determined by adding the trip assignment from the


Figure 4: Weekday PM Peak Hour Project Trip Distribution and Assignment


Figure 5: 2026 No Action Weekday PM Peak Hour Traffic Volumes (Buildout)


Figure 6: 2026 With Project Weekday PM Peak Hour Traffic Volumes (Buildout)


Figure 7: 2032 No Action Weekday PM Peak Hour Traffic Volumes (Horizon Year)


Figure 8: 2032 With Project Weekday PM Peak Hour Traffic Volumes (Horizon Year)

## Intersection LOS Analysis

Future intersection LOS analyses during the weekday PM peak hour were evaluated at the seven (7) off-site study intersections for future year 2026 (buildout year) and 2032 (horizon year) conditions with and without the English Crossing project. Off-site study intersections were identified based on the City of Marysville's Traffic Impact Analysis Guidelines (December 2021), and confirmed through the traffic scoping process. The signal timing data used at the off-site signalized study intersections were based on data provided by the City of Marysville and WSDOT.

The 2026 and 2032 roadway networks assumed in the future LOS analyses were based on existing intersection geometry, plus at least partial completion of the following City planned improvements:

- $172^{\text {nd }}$ Street NE $/ 19^{\text {th }}$ Avenue NE Roundabout - construct new roundabout at the $19^{\text {th }}$ Avenue NE / 172 ${ }^{\text {nd }}$ Street NE intersection. (Marysville TIP Project \#24)
Note: this improvement is required as a condition of approval for the Lodge Apartments project and is expected to be a condition of approval for English Crossing. As such, this improvement is assumed to be completed in the 2026 No Action and 2026 With Project scenarios.
- 172nd Street NE from $27^{\text {th }}$ Avenue NE to $19^{\text {th }}$ Avenue NE - widen to a 4/5-lane section with pedestrian and bicycle facilities between $27^{\text {th }}$ Avenue NE and $19^{\text {th }}$ Avenue NE. (Marysville TIP 30)
Note: this improvement is assumed to be completed in the 2032 No Action and 2032 With Project scenarios as development is completed along the corridor.
- $172^{\text {nd }}$ Street NW from $19^{\text {th }}$ Drive NE to $11^{\text {th }}$ Avenue NE - widen to a 3 -lane section with pedestrian and bicycle facilities between $19^{\text {th }}$ Drive NE and $11^{\text {th }}$ Avenue NE.
Note: this improvement is assumed to be completed in the 2032 No Action and 2032 With Project scenarios as development is completed along the corridor but does not change roadway geometry at any of the off-site intersections.
- New 19th Avenue NE Extension - construct new 3-lane roadway between $156^{\text {th }}$ Street NE and $172^{\text {nd }}$ Street NE that would include pedestrian and bicycle facilities. (Marysville TIP \#5 1)
Note: this improvement is assumed to be completed in the 2032 No Action and 2032 With Project scenarios as development is completed along the corridor.
The intersection LOS results are summarized in Tables 8 and 9 and detailed LOS worksheets are provided in Appendix C.


## Table 8

2026 Buildout Year - Weekday PM Peak Hour LOS Summary

| Study Intersection / Movement | No Action |  | With Project |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay (sec) | LOS | Delay (sec) |
| Stop-Controlled Intersections: |  |  |  |  |
| 1) $11^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE |  |  |  |  |
| Eastbound Left-Turn | A | 8.2 | A | 8.3 |
| Westbound Left-Turn | A | 7.9 | A | 7.9 |
| Northbound Approach | B | 12.0 | B | 12.1 |
| Southbound Approach | B | 14.9 | C | 15.2 |
| 2) $19^{\text {th }} \mathrm{Dr}$ NE / $172^{\text {nd }}$ St NE |  |  |  |  |
| Westbound Left-Turn | A | 8.1 | A | 8.1 |
| Northbound Approach | B | 10.8 | B | 10.9 |
| Roundabouts: |  |  |  |  |
| 3) $19^{\text {th }}$ Ave NE / $1722^{\text {nd }}$ St NE | A | 3.9 | A | 4.3 |
| 4) $23^{\text {rd }}$ Ave NE / $1722^{\text {nd }}$ St NE | A | 4.5 | A | 4.5 |
| Signalized Intersections: |  |  |  |  |
| 5) $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE | E | 68.2 | E | 66.3 |
| 6) l-5 SB / $172^{\text {nd }} \mathrm{St} \mathrm{NE}$ | A | 6.8 | A | 6.7 |
| 7) I-5 NB / $172^{\text {nd }}$ St NE | C | 24.8 | C | 26.1 |

## Table 9

2032 Horizon Year - Weekday PM Peak Hour LOS Summary

|  | No Action |  | With Project |  |
| :---: | :---: | :---: | :---: | :---: |
| Study Intersection / Movement |  | Delay |  | Delay |
|  | LOS | (sec) | LOS | (sec) |

Stop-Controlled Intersections:

1) $11^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE

| Eastbound Left-Turn | A | 8.5 | A | 8.5 |
| ---: | :---: | :---: | :---: | :---: |
| Westbound Left-Turn | A | 8.1 | A | 8.1 |
| Northbound Approach | B | 13.8 | B | 14.0 |
| Southbound Approach | C | 17.1 | C | 17.4 |

2) $19^{\text {th }} \mathrm{Dr} \mathrm{NE} / 172^{\text {nd }} \mathrm{St} \mathrm{NE}$

| Westbound Left-Turn | A | 8.3 | A | 8.3 |
| ---: | :---: | :---: | :---: | :---: |
| Northbound Approach | B | 11.6 | B | 11.8 |

Roundabouts:
3) $19^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE
4) $23^{\text {rd }}$ Ave NE / $172^{\text {nd }}$ St NE

| A | 3.3 | A | 3.8 |
| :--- | :--- | :--- | :--- |

Signalized Intersections:
5) $27^{\text {th }}$ Ave NE / $172^{\text {nd }}$ St NE F $\quad 92.5 \quad$ F 90.4
6) I-5 SB / $172^{\text {nd }}$ St NE A $\quad$ 6.5 $\quad$ A 6.4
7) I-5 NB / $172^{\text {nd }} S t$ NE $\quad$ D $44.5 \quad$ D 49.0

As shown in Table 8, at the time of anticipated project opening (year 2026), all off-site study intersections are expected to meet the applicable LOS standards during the weekday PM peak hour in year 2026 without or with the proposed project. This includes the $27^{\text {th }}$ Ave NE / 172 ${ }^{\text {nd }}$ St NE intersection since it currently operates at LOS E and will remain at LOS E in 2026.

As shown in Table 9, by 2032, all off-site study intersections are expected to meet the applicable level of service standards during the weekday PM peak hour without or with the proposed project with one exception. The intersection of $27^{\text {th }}$ Avenue NE/ $172^{\text {nd }}$ Street NE is anticipated to operate at LOS F during the weekday PM peak hour under the 2032 No Action and 2032 With Project scenarios.

The City of Marysville and WSDOT LOS standard at intersections is LOS D with one exception. The City of Marysville Traffic Impact Analysis Guidelines state that intersections on the 172nd Street NE (SR 531 ) corridor which have an existing LOS E prior to development submittal shall only be required to mitigate upon falling below LOS E. This applies to the $27^{\text {th }}$ Ave NE / $172^{\text {nd }} \mathrm{St}$ NE intersection for the buildout year 2026 analysis. However, for the 2032 horizon year analysis, this intersection is anticipated to operate at LOS F with or without the project.
The City's long-term plan for addressing this anticipated LOS F condition at the $27^{\text {th }}$ Avenue NE/172nd Street NE intersection is the $156^{\text {th }}$ Street NE Interchange project planned by WSDOT (TIP \#61). The $156^{\text {th }}$ Street NE interchange with $1-5$ is expected to shift some traffic away from the $27^{\text {th }}$ Avenue NE/172nd Street NE intersection, also reducing demand on the $172^{\text {nd }}$ Street NE corridor and improving LOS at this and other intersection. Until funding is identified for the new interchange, it is expected that the $27^{\text {th }}$ Avenue NE / $172^{\text {nd }}$ Street NE intersection in the future will function at LOS E/F during peak hours.

Additionally, and in response to City comments, several transportation improvement options were evaluated at the $27^{\text {th }}$ Avenue NE/172 nd Street NE intersection in 2032 with the proposed English Crossing project such as eastbound and southbound right-turn lanes, a dual northbound right-turn lane, and a two-lane roundabout. Based on this preliminary alternative analysis, the improvement that would be anticipated to improve operations at the $27^{\text {th }}$ Avenue $N E / 172^{\text {nd }}$ Street $N E$ to level of service (LOS) $D$ is adding a second northbound right-turn lane which would result in dual right-turn lanes.

It should also be noted that the addition of project traffic to intersections \#5 and \#6 results in a decrease (improvement) in the overall average intersection delay during the weekday PM peak hour. This occurs because the project adds trips to non-critical movements instead of movements with higher levels of delay. While counterintuitive, this phenomenon results in a decrease in the average delay for the entire intersection.

## Site Access Evaluation

Vehicular access to the site would be provided be provided via a new site access roadway connection to $19^{\text {th }}$ Ave NE, aligned with $174^{\text {th }}$ Street NE. Secondary access for emergency vehicles only would be provided north of $174^{\text {th }}$ Street NE via another new site access roadway connection to $19^{\text {th }}$ Ave NE. To evaluate the operations of the site access intersection, a level of service (LOS) and queue analysis was completed. The weekday PM peak hour LOS and queue analysis at the site access intersection was based on the methodology outined in the $6^{\text {th }}$ Edition of the Highway Capacity Manual using Synchro 11 software.

Table 10
PM Peak Hour Site Access LOS and Queuing

| Controlled Movements | 2026 With Project |  |  | 2032 With Project |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $95^{\text {th }} \%$ |  |  | $95^{\text {th }} \%$ |
|  | LOS ${ }^{1}$ | Delay | Queve <br> $(\mathrm{ft})^{3}$ | LOS ${ }^{1}$ | Delay | Queve $(\mathrm{ft})^{3}$ |
| A. $19^{\text {th }}$ Ave NE / $174^{\text {th }}$ St NE / Site Access |  |  |  |  |  |  |
| Eastbound Approach | A | 9.5 | <25' | A | 9.6 | <25' |
| Westbound Approach | B | 10.2 | <25' | B | 10.4 | <25' |
| Northbound Left-Turn | A | 7.5 | <25' | A | 7.5 | <25' |
| Southbound Left-Turn | A | 7.4 | <25' | A | 7.5 | <25' |

1. LOS = Level of Service
2. Delay refers to average control delay expressed in seconds per vehicle.
3. Queues are $95^{\text {th }}$ Percentile queves. $<25^{\prime}$ indicates $95^{\text {th }}$ Percentile queue statistically less than 1 vehicle.

Table 9 summarizes the calculated LOS and the $95^{\text {th }}$ percentile queves of the controlled movements at the site access intersection during the weekday PM peak hour in 2026 (buildout year) and 2032 (horizon year) with the proposed project. The reported $95^{\text {th }}$ percentile queues represent a condition that is exceeded only 5 percent of the time. Detailed LOS and queve calculation worksheets are included in Appendix C.

## Snohomish County Key Intersections

In accordance with the Snohomish County Traffic Worksheet and Traffic Study Requirements for Developments in the City of Marysville, project trip impacts at Snohomish County key intersections were identified. Weekday AM and PM peak hour Trip Distribution and Assignment figures and tables were prepared consistent with these guidelines and are included in Appendix F.

## MITIGATION

The following measures have been identified to mitigate traffic impacts of the proposed English Crossing project.

City of Marysville Traffic Impact Fees. The City of Marysville requires payment of transportation impact fees to help fund planned roadway improvements throughout the City. Transportation impact fees for the proposed English Crossing project were calculated based on the trip generation estimate documented in this TIA and the City of Marysville's currently adopted transportation impact fee rate of $\$ 6,300$ per PM peak hour trip. The proposed English Crossing project is estimated to generate 250 new PM peak hour trips. As a result, the estimated City of Marysville transportation impact fee is $\$ 919,800(\$ 6,300 \times 146$ PM peak hour trips). Actual impact fees will be calculated by the City at the time of building permit issuance.
$27^{\text {th }}$ Ave NE/ $172^{\text {nd }}$ Street NE Intersection. This intersection is anticipated to operate at LOS F in the future 2032 horizon year PM peak hour as a result of the funding loss for the $156^{\text {th }}$ Street NE interchange with $1-$ 5. A couple options that should be considered by the City include: (1) adding a $2^{\text {nd }}$ northbound right-turn lane, and/or (2) allowing the intersection operation to exceed the LOS threshold until funding for the $156^{\text {th }}$ Street NE interchange is funded.
Snohomish County Mitigation. The City of Marysville and Snohomish County have adopted an interlocal agreement whereby developments in Marysville must assess potential mitigation for impacts on Snohomish County roadway facilities. Mitigation fees to Snohomish County are based on predetermined distribution percentages according to location or specific project impacts to planned roadway improvements. Mitigation fees to Snohomish County were based on the use of the standard distribution percentage based on the project location $(20 \%)$ multiplied by the daily trip generation ( 1,855 new daily project trips) and adopted cost per ADT ( $\$ 185$ for residential developments within TSA A and the UGA). The resulting Snohomish County transportation impact fee is $\$ 68,635$. A mitigation offer form to Snohomish County will be submitted separately and is included in Appendix G.
Future City Road Plans. The English Crossing project would build a portion of the following City planned roadway improvements:

- Construct and dedicate right-of-way for the western half-street of a 3-lane section on 19th Avenue NE from $172^{\text {nd }}$ Street NE to the northern site property line.
- Construct and dedicate right-of-way for the northern half-street of a 3-lane section on 172nd Street NE from $19^{\text {th }}$ Avenue NE to the western site property line.
- Construct a new roundabout (or a portion of a new roundabout) at $19^{\text {th }}$ Avenue NE / 172 ${ }^{\text {nd }}$ Street NE if not already completed by other development.

It should be noted that it is anticipated the applicant would receive transportation impact fee credit for construction and ROW dedication of all of these roadway construction projects as confirmed by the City.

## Appendix A

Crash Data

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| Sate Route |  | Atirigeo |  |  |  |  |  |  |  |  | 09903／2021 | 1 No Apparent lijury |  |  |  |  | Makkeg left Turn | Soing Straibt Ahead | North | East |  |  |
| State Route |  | Aringon | 31 |  |  |  |  |  |  | ${ }^{6.22}$ | $05 / 22 / 2020$ | Apparent inury |  |  |  |  | oing straigh Ahead | topped at Stigal or Stiop |  |  |  | le Stopped |
| State Route | SnotomI | Atirigton | ${ }^{31}$ |  |  |  |  |  |  | ${ }_{6}^{62}$ | ${ }^{\text {04，} 93012022}$ | 2 No Apparent tiulur |  |  |  |  | Soing staight Ahead | Making left Turn | East | West | North |  |
| $\frac{\text { sate Roure }}{\text { State }}$ |  | Alinimbon | ${ }_{531}^{531}$ |  |  |  |  |  |  | 6． 6.28 | ${ }^{007 / 26 / 2022}$ | 2 No Appareret Injur |  |  |  |  | Soin straigh thead | Makne Left turn | $\underbrace{\text { cest }}_{\text {cest }}$ | West | Venicle stoped | vehice Stopped |
| Sate Route | Snohomishan | Afinigion | ${ }^{531}$ |  |  |  |  |  |  | 6.28 | 02／07／2019 | Posstibe Inuy |  |  |  |  | Soine Straibht Ahead | Stopeed at Signalo 0 Stop St | deast | west | venicie stoped | vehicie stopeed |
|  | ohome | Afiligton |  |  |  |  |  |  |  | 6.29 | 03／17／2018 | 3 No Apparent hive |  |  |  |  | Changig lanes | Going Strajht Ah |  | Northu |  |  |
| State Route | stohom | Arington | 31 |  |  |  |  |  |  | ${ }^{6} 3$. | 01300／2022 | $2{ }^{\text {Posstil inuyy }}$ |  |  |  |  | Changing Lanes | Gong Straigh Anead | West | East |  |  |
| State Route | ohom | Arington | ${ }^{531}$ |  |  |  |  |  |  | 6.32 | 08100／2018 | N No Apparent tiulur |  |  |  |  | song Straightahead | Sowng | ast | West | ast |  |
| State Route |  |  | ${ }_{531}^{531}$ |  |  |  |  |  |  | ${ }_{6}^{6.35}$ | ${ }^{\text {O5 }} 504 / 2 / 2021818$ | 3 No Apparent tiur |  |  |  |  | Soine straibit Anead | Shanging Lenes | East | West | Ventice stoped | Ventice Stoped |
| Sate Route | Snohomisha | Afiligton 5 | ${ }^{531}$ |  |  |  |  |  |  | 6.35 | 01／15／2022 | INo Apparent thiur |  | 0 |  |  | Going Straight Ahead | Stopeed for Trafic | East | west | venicie stopped | venicie stopeed |
| State Route | Snohomis 4 A | Arington | ${ }^{31}$ |  |  |  |  |  |  | 6.36 | 01／33／2019 | ．No Apparent tiury |  |  |  |  | Changig lanes | Going Strieitht Ahead | ast | West | ${ }^{\text {ast }}$ |  |
| State Route |  |  | ${ }_{531}^{531}$ |  |  |  |  |  |  |  | ${ }^{\text {O }}$ O5／29／2020 | Noostio enluy |  | $\bigcirc$ |  |  | Changin lones |  | finest | ${ }_{\text {Esest }}$ West | Lest | Veest venie stoped |
| State Route | Snotomishal | Afiligeton | ${ }^{531}$ |  |  |  |  |  |  | 6.37 | 02／33／2019 | TNo Apparent liury |  | 。 |  |  | Soing Straight Ahead | Stoped tor Trafic | Est | west | venicle stoped | venicle stoped |
| State Route | Snohomish ${ }^{\text {a }}$ | Arington | ${ }^{531}$ |  |  |  |  |  |  | 6.38 | 111／7／2018 | 8No Apparent lijur |  | 。 |  |  | Thangig Lanes | Going Straight Ahead | Est | West |  |  |
| Sate Route | Snohomis | Aringoon | ${ }^{31}$ |  |  |  |  |  |  | ${ }^{6.39}$ | 10／28／2021 | 1 Posstibe lijur |  |  |  |  | Soing Stright Ahead | Solown | west | East | west | ast |
|  | ， | Airingion | ${ }^{51}$ |  |  |  |  |  |  | 6.40 | 12／33／2021 | No Apparenet tiulur |  |  |  |  | Sing strieght Ahead |  |  |  |  |  |
| State Route | Snohomis Smomem |  | ${ }_{531}^{531}$ |  |  |  |  |  |  |  | ${ }^{\text {04／1／62022 }}$ | 2．No Appareent tijur |  | $\bigcirc$ |  |  | Staring ir Trific lane |  | ${ }_{\text {Esst }}^{\text {Est }}$ | ${ }^{\text {west }}$ | ${ }_{\text {Esast }}^{\text {East }}$ | west |
| State Route | Se | Ariniogion | ${ }_{531}$ |  |  |  |  |  |  | 6.41 | 01／25／2022 | No Apparent tiury |  | 0 |  |  | oing Sraight Ahead | Stoped for Traffic | west | ， | west |  |
| State Route | nohomista | Arington | ${ }^{531}$ |  |  |  |  |  |  | 6.42 | 03／14／220 | ono Apparent liulur |  |  |  |  | Soing Straight Ahead | Soing Straitht Ahead | ast | west |  | Nort |
| Sate Route | Snotomi | Arivegion | 31 |  |  |  |  |  |  | 6.42 | 03／66／2018 | 8 Possibil Inuy |  | 。 |  |  | oing straight Ahead | Making Letef Tum | West | East | south |  |
| ate Route | Soromist $A$ | Aringion ${ }^{\text {a }}$ | ${ }^{31}$ |  |  |  |  |  |  | ${ }_{6}^{6.42}$ | 05531／2021 | 1 No Apparenet tiury |  |  |  |  | Straight Ahead | Stopeed at Sisal or sop |  | North | Ehicle soon | ehice stopeed |
| Sate Route | Snohomis | Aririgion | 31 |  |  |  |  |  |  | 6.42 | 10122／2020 | －No Apparent tijury |  |  |  |  | soing Straight Ahead | Making Letet Tum | West | West |  | vest |
| State Route | nohomis | Arivigion | 31 |  |  |  |  |  |  | 6.42 | 10／31／2018 | 8 No Apparent triury |  |  |  |  | Soing Straight Ahead | Going Straight Ahead | West | East |  |  |
| State Route | ohomis | Arimgaton | ${ }^{31}$ |  |  |  |  |  |  | 6.42 | 01／08／2018 | 8 No Apparenent lijury |  |  |  |  | Soing Straight Ahead | Making Letet Tum | west | Esast |  |  |
| State Route |  | ${ }^{\text {Afiligition }}$ A | ${ }_{531}^{531}$ |  |  |  |  |  |  | $\frac{6.42}{6.42}$ | －08／142022 | 2 Possibe lijury |  | 。 |  | $\frac{0 \mathrm{~m}}{0 \mathrm{ma}}$ | Maxing Left turn | $\frac{\text { Soing Straje }}{\text { Stophead }}$ Stad | South | ${ }_{\text {west }}$ west | West ${ }^{\text {venicle stoped }}$ | vericies stoped |
| Sate Route | Snotomishal | Afiringon | ${ }^{531}$ |  |  |  |  |  |  | 6.42 | 10／20／2018 | 8 No Apparent tiulur |  | 0 |  |  | Going Straight Ahead | Maxin Left Tum | West | Esat | South | west |
| State Route | homisha | Afiniogion | ${ }^{31}$ |  |  |  |  |  |  | ${ }_{6.4}$ | 09／23／2021 | 1 No Apparent triury |  |  |  |  | Making UTum | Going Sraight Ahe | West | est |  |  |
| State Route | notomis | Arlingon | ${ }^{31}$ |  |  |  |  |  |  | ${ }_{6}^{6.42}$ | 07731／220 | －No Apparent tijury |  |  |  |  | Soing Straight Ahead | Making Letet Tum | west | East | North | St |
| State Route | thohomis | Atirigeo | ${ }^{531}$ |  |  |  |  |  |  | ${ }_{6}^{6.42}$ | 05／05／2019 | No Apparent tiviur |  |  |  |  | oing Striait A Ahead |  |  | South |  |  |
| State Route |  | ${ }^{\text {Aringigion }}$ A | ${ }_{531}^{531}$ |  |  |  |  |  |  | 6．622 | ${ }_{\text {－}}^{\text {12／24／2020 }}$ | No Apparent tiviur |  |  |  | O | Goin Straib thead | Msking Left Turn | west | Esat | South |  |
| State Route | Snohomish ${ }^{\text {a }}$ | Afingeon | 531 |  |  |  |  |  |  | ${ }_{6.4}^{6}$ | 11／10／2／220 | Noo Apparentit inury |  | 。 |  |  | luakre Left Turn | Makingelet Turn | South | west | South |  |
| State Route | Iohomis | Afingen | ${ }^{531}$ |  |  |  |  |  |  | ${ }_{6.4}$ | 09／13／2019 | uspected Minor hly |  |  |  |  | Sings staight Ahead | Going Straight Ahead | West | East |  | North |
| State Rove | Snohomis ${ }^{\text {a }}$ | Afingon | 531 |  |  |  |  |  |  | 6.42 | 10／21／2022 | 2 No Apparent tiury | － | － |  |  | Soing Straight Ahead | Maxkin Left Turn | West | East | South | west |
| State Roure |  | AAlingon | ${ }_{531}^{531}$ |  |  |  |  |  |  | $\frac{6.42}{6.42}$ | ${ }^{11 / 1 / 550222}$ | 2 Possbie Inury |  | ， |  |  | Soins staigh A head | Makng Left Tum | ${ }_{\text {West }}$ | ${ }_{\text {cost }}^{\text {cast }}$ East |  |  |
| Slate Route | Snohomishan | Afingeo | ${ }^{531}$ |  |  |  |  |  |  | ${ }_{6.4}$ | 05／13／2021 | uspected Minor roij |  |  |  |  | Going Strieht Ahead | Making elet Tum | Nest | East | th | west |
|  |  |  |  |  |  |  |  |  |  |  | Sh32018 | No Apparent liuiur |  | － |  |  | Going Straight Ahead | gleft |  |  | 迷 |  |
| $\frac{\text { sate Route }}{\text { State }}$ | Snohomis ${ }^{\text {a }}$ | Atingon | ${ }_{5}^{531}$ |  |  |  |  |  |  | 6.42 | 01／2／2／019 | Possibe Ijury |  |  |  |  | Soing Strieit Ahead | Making Left tur | west | ${ }_{\text {East }}$ |  |  |
| State foute | Snothomish | Aninioston | 531 |  |  |  |  |  |  | ${ }_{6}^{6.43}$ | 11／1882019 | 9，No popparenert tiur |  |  |  |  | charging lanes | Sopes sraight Ahead | Esast | Southw | East | West |
| State Route | Snohomis | Aringson | ${ }^{531}$ |  |  |  |  |  |  | ${ }_{6}^{6.43}$ | 12／14／2018 | 8 No Apparent thiur |  |  |  |  | Soing staight Ah | topped for Trafic | ast | West | ed | Venicle stopeed |
| State Route |  |  | ${ }^{531}$ |  |  |  |  |  |  |  | 07／25／2019 | Q No Apareent liury |  |  |  |  | Soing Straight Ahead |  |  | East |  |  |
| $\frac{\text { sate Route }}{\text { State }}$ | Snotemis | ${ }^{\text {Alingion }}$ A | ${ }_{5}^{531}$ |  |  |  |  |  |  | 6．44 | ${ }^{12 / 7 / 192019}$ | No Apaperestiur |  | － |  |  | Maxing figh turn | Stoped for Tratic | South | Esast | South | Sest |
| State Route | Snonomish A | Afinimgon | ${ }^{531}$ |  |  |  |  |  |  | 6.44 | 12／17／2022 | 2 Possbibe iniury |  | ， |  |  | Going straibt Ahead | Stopeed for Trafic | East | west | Vencice stopped | Venicle |
| State Route |  |  | 531 |  |  |  |  |  |  | 6.45 | 10033／2018 | B Posisili lijury |  |  |  |  |  |  | west | East | West |  |
| $\frac{\text { spate Route }}{\text { State }}$ | Snonomis 4 A | Afingeton | ${ }^{531}$ |  |  |  |  |  |  | ${ }_{6}^{6.45}$ | ${ }^{0} 88 / 2929219$ | No Apparenet tiury |  |  | 。 |  | Soing Straibt Ahead | Stopeed for Trafic | East | West | tase | Nest |
| Sater oute |  | Aniligeo | ${ }_{531}^{531}$ |  |  |  |  |  |  | \％ 6.46 | ${ }^{0.240772021}$ | No Apparent tupr |  | $\bigcirc$ |  |  | Stion | Goong straithtanead | Eest | west |  |  |
| State Route | Seher | Afingeton | 531 |  |  |  |  |  |  | ${ }_{6} 6.4$ | 11／06／2019 | \＃No Apparent lijury |  |  |  |  | Charging lanes | Soing Straight Ahead | Nest | East | west | ast |
| State Route | Snohomish ${ }^{\text {a }}$ | Afirigton | ${ }^{531}$ |  |  |  |  |  |  | 6.46 | 12／30／2019 | Wo Aparenet triury |  | － |  |  | Going Straight Ahead | Stoped for Trafic | West | Est | venicle stoped | Venicice stoped |
| $\frac{\text { sate Route }}{\text { Sate Poute }}$ | son | Aringoo | ${ }^{31}$ |  |  |  |  |  |  |  | ${ }^{01 / 1 / 1 / 2 / 202}$ | No norather |  |  |  |  | ang Staiaht Anead | Gorng sta |  |  |  |  |
| Sate Route | Snomomisha | Afingiton 5 | ${ }_{51}^{51}$ |  |  |  |  |  |  | 6.47 | 03／22／2021 | 1 No Apparent thiur |  |  |  |  | Changing Lanes | Going straight Ahead | West | Northeast | West | East |
| State Route |  |  | ${ }_{531}^{531}$ |  |  |  |  |  |  |  | ${ }^{03 / 082 / 2021}$ | IPosibi iniur |  | － |  |  | Goin Straigh Ahead | Stion | East | West |  |  |
| State Route | Snotomishan | Afingeton 5 |  |  |  |  |  |  |  | 6.49 | 05／08／2018 | 3 No Apparent tijury |  | 0 |  |  | Going Straight Ahead | Stopeed for Trafic | West | East | West |  |
| State Route | Snohomishat | Afington 0 | ${ }^{\text {OOSP } 1205358}$ |  |  |  |  |  |  |  | ${ }^{051 / 3 / 2022}$ | No Apparent tiviur |  |  |  |  | Charging lanes | Stating in Taffic lane | south | North | South | North |
| Stee | Snonomishal | Afinimion | ${ }^{\text {cosprp203588 }}$ |  |  |  |  |  |  | 0．60 | ${ }^{\text {a }} 12 / 1 / 55120222$ | 2 Poospabientitury |  | $\bigcirc$ |  |  | Stanting in Trafic lane | stopeed for Trafic | Venitice Sopped | North | Venicies stoped | venicie stopped |
| State foute | Snonomis 4 A | Atiringion | ${ }^{\text {Oosp } 120538}$ |  |  |  |  |  |  | 0.64 | 03／202／2022 | Possible lijur | ${ }^{1}$ | － | 2 |  | Going Straight Ahead | Slowing | south | North | th | North |
| State Route | nohom | Afrington | ${ }^{\text {005P120538 }}$ |  |  |  |  |  |  | 0.64 | 11／02／2021 | 1 No Apparent thiur |  | － |  |  | Soing straight Ahead | Slowing |  |  |  |  |
| sate Route | ， | Animston | ${ }^{\text {Losp } 120538}$ |  |  |  |  |  |  | 0.6 | 10042029 | Noapparentinur |  |  |  |  | Gonis staighthead | sowng |  | Nort |  |  |
| State Route | smonoms | Aningion | ${ }^{\text {cospr }}$ |  |  |  |  |  |  | 0．66 | ${ }^{\text {O }}$ O1／2242020 | －NoApareretivur | － | － |  |  | Soins Sraibt Anead | Stopeat orr rafic | tith | North | South | Vencies stoped |
| State foute | Snothish | AAringoton | 005P120538 |  |  |  |  |  |  | 0.68 | $07 / 19212019$ |  |  |  |  |  | 6oing straight Ahead |  | South | North | Venicice stoped | Venide stopeed |
| State Route | Snohomis 4 A | Afingeo 0 |  |  |  |  |  |  |  | 0.68 |  | 1 No Apparent tiulur |  | － |  |  | Charging lanes | Stating in Taffic lane | south | North | South | North |
| State Route | Shomis | Atingto | 005P120538 |  |  |  |  |  |  | 0.68 | 11／092021 | 1 No Apparent tijury |  |  |  |  | Going Straigh Ahead | Slowing | south | North |  |  |
| State Route |  |  |  |  |  |  |  |  |  |  | ${ }^{\text {11／2／22019 }}$（1023／2018 | Sposide in iny |  |  |  |  | Goin Staiblit head | Stoped for Trafic | South | ${ }_{\text {North }}$ | Vonicle sim | Vencice |
| State Route | Snohomis 4 A | Afingto 0 | Oospl20538 |  |  |  |  |  |  |  | 02／09／2020 | No Apparent tijury |  |  |  |  | Negotationg a aure |  | suth | Est |  |  |
| State Route | Snohomis ${ }_{\text {a }}$ | ${ }^{\text {Afiningion }}$ Alon |  |  |  |  |  |  |  | 0.70 0.70 | ${ }^{\text {O4／332022 }}$ | 2．Possibl lijury |  |  |  |  | ／Maxin E Eiph Turn | stopeed for Tratic | North | ${ }_{\text {Esast }}^{\text {East }}$ | venicle stoped | Vehicie stopeed |
| State Route | Snohomis ${ }^{\text {a }}$ | Atirigion 0 | 005P120538 |  |  |  |  |  |  | 0.71 | 08／07／2018 | B Posstio liuur |  |  |  |  | Making Rifht | Maxing Rifht tum | West | Est |  |  |
| $\frac{\text { sate Route }}{\text { Sta }}$ | Sninhomis ${ }_{\text {a }}$ |  | ${ }^{\text {lospprpes } 20538}$ |  |  |  |  |  |  |  | ${ }^{\text {06／06／2018 }}$ | 3 No Apparent tiury |  |  |  |  | Soing straigt Ahead |  | Whest | ${ }_{\text {Nerth }}^{\text {Nest }}$ | North | Venhid stoped |
| State Route | Snonomisha | Afingito 0 | 0059120660 |  |  |  |  |  |  |  | 09／2／2／2018 | 3 No Aparenent liury |  |  |  |  | Making Rifht Tum | Maxing R Ribht Tum | South | North | South | North |
| State Route | Snohomishan | Afirigto 0 | ${ }^{0059120660}$ |  |  |  |  |  |  |  | 08／28／2018 | 3 No Apparent thury |  |  |  |  | Overataing and Passing | Going Straight Ahead | south | North | south | North |
| State Route | Snohomis | Ailintion | ${ }^{00550512060}$ |  |  |  |  |  |  | ${ }^{0.05}$ | ${ }^{03 / 31 / 2022}$ | Possitil fijury |  |  |  |  | Mereing Ethering TTafic） | Ging strighthead | South | North | South | North |
| State Route |  | ${ }^{\text {Afinfingion }}$ AO | ${ }^{\text {Ooss5s205s3 }}$ |  |  |  |  |  |  | 0 | 0951／20019 |  |  |  |  |  | Chargng lanes |  | West | ${ }_{\text {South }}$ West | Vest venice stoped | South |
| State Route | Snohomis ${ }^{\text {a }}$ N | Marssille 5 | ${ }^{531}$ |  |  |  |  |  |  |  | 05／6662022 | No Aparenent tiury |  |  |  |  | Making Lett Turn | Soing Straight Ahead | South | West |  | west |
| State Route | Snohomis ${ }^{\text {a }}$ | Marssulle | ${ }^{531}$ |  |  |  |  |  |  | 5.12 | 06／10／2021 | 1 No Apparent thiury |  | 。 |  |  | Overataking and Passing | Stoped dat Sigal or 5 Stop 5 | S South | Est | venide Stoped | vehicie stopped |
| State Route | Snohomis ${ }^{\text {a }}$ | Marssille 5 | 531 |  |  |  |  |  |  | 5.12 | 08／07／2021 | 1.1 suspected Minor rijur |  | 0 |  |  | Goins Straight Ahead | Going Straight Ahead | North | south | west | ast |
| State Route | Snohomis Snomomis | Marssile | ${ }_{531}^{531}$ |  |  |  |  |  |  | 5．121 | （127／0／62020 | Possie limy |  | $\bigcirc$ |  |  |  | Making Left turn | ${ }_{\text {West }}^{\text {East }}$ | ${ }_{\text {eser }}^{\text {E．est }}$ | ${ }_{\text {E }}^{\text {East }}$ | west |
| Slate Route | Snohomis ${ }^{\text {a }}$ | Marssille 5 | ${ }^{531}$ |  |  |  |  |  |  | 5.20 | 01／21／2019 | No Apparent lijury |  |  |  |  | Soing Straight Ahead |  | Est | West |  |  |
| $\frac{\text { Slate Route }}{\text { Sile }}$ | Snohomis ${ }^{\text {N }}$ | Marssulle 5 | ${ }^{531}$ |  |  |  |  |  |  | 5.30 | 09／25／2018 | BPossibe Iniury |  | － |  |  | Going strigith thead | stopeed for raftic | West | ${ }^{\text {East }}$ | Venicie stoped | Venicies stoped |
| State Route | Snohomis Snomomis | ${ }^{\text {Marssule }}$ Marsule |  |  |  |  |  |  |  | ${ }_{5}^{5.38} 5$ | －12／772019 | No A Ppareent tijur |  |  |  |  | Makin Ripht Turn | Goin Sraight thead | ${ }^{\text {Norrh }}$ | ${ }_{\text {West }}^{\text {Werth }}$ |  | West |
| $\frac{\text { Slate Route }}{\text { State }}$ | Snahomist | Marssulle 5 | $\left.\right\|_{531} ^{511}$ |  |  |  |  |  |  | \％ 5.48 | － $11 / 25 / 2019$ | ，No Apparenetiviur |  | － |  |  | Going straigh thead | Stoped for Tratic | West | ${ }_{\text {Est }}$ | Venitie stoped | Venicle stoped |
| State Route | Snohomis ${ }^{\text {Somomis }}$ N | ${ }^{\text {Marssule }}$ Mansule |  |  |  |  |  |  |  | 5．55 | － $11 / 19272019$ | 1．No A Paperent tijury |  |  |  |  | Goin Sin Sraibt thead |  | West | Eost | Venicie stoped | Vehicic stoped |
| $\frac{\text { State }}{\text { State }}$ | Snohomis ${ }^{\text {N }}$ | Marsvile 5 | ${ }_{531}^{531}$ |  |  |  |  |  |  | 5.50 | 12／17／2020 | Possibl eliury |  | ． |  |  | Making left Tum | Going graith thead | West | Northest | West | East |
| $\frac{\text { sate Route }}{\text { State }}$ | Snohomis ${ }_{\text {chem }}$ | Marssile |  |  |  |  |  |  |  | 5.50 <br> 5.50 | －01／2572019 | P Possible Ijuy |  | $\bigcirc$ |  |  | Maxing left Turn | $\frac{\text { Soing Straibt Ahead }}{\text { Maxikg Lefturn }}$ | ${ }_{\text {enest }}^{\text {E．est }}$ | $\sum_{\text {South }}^{\text {Sast }}$ |  |  |
| $\frac{\text { Slate Route }}{\text { Sta }}$ | Snomomis ${ }^{\text {a }}$ | Marsulle 5 | ${ }_{531}^{531}$ |  |  |  |  |  |  | ${ }_{5}^{5} 54$ | 04／23／2018 | So Apparest tiur |  | 0 |  |  | Soine straibht Ahead | Stoped for Trafic－ | west | ${ }^{\text {East }}$ | Venite stoped | Venicle stoped |
| State Route | Snohomis ${ }_{\text {den }}$ | Marssule |  |  |  |  |  |  |  | 5.54 5.54 5 | － 0 O／2／7／2019 | 9 Possibe lijur |  |  |  |  | Soin straibt thead | ${ }^{\text {Stoped at S Sigal or }}$ Stop S S | Est | West |  |  |
| State Route | Snohomis | Margsule 5 | ${ }_{531}^{531}$ |  |  |  |  |  |  | 5.56 556 | ${ }^{01 / 29 / 292020}$ | Posstib liuly |  | － |  |  | Goin straib thead | stoped for Trific | East | west |  |  |
| $\frac{\text { sate Route }}{\text { State }}$ | Snohomis ${ }_{\text {S }}$ | ${ }^{\text {Marssvile }}$ Mansile |  |  |  |  |  |  |  |  |  | S Suspected Minor fium |  |  |  |  | Goin straibt Ahead | ${ }_{\text {stoped or or }}^{\text {siafic }}$ | $\frac{\text { ast }}{\text { Nest }}$ | ${ }_{\text {West }}^{\text {cest }}$ | Vehice Stopped | Vehicis stoped |
| Slate Route | Snohomis ${ }^{\text {a }}$ N | Manssille 5 | ${ }^{531}$ |  |  |  |  |  |  | 5.59 | 02／4／20018 | Possible fiury |  |  |  |  | Goine straibht Ahead | Stowing | west | ${ }_{\text {East }}$ |  | West |
| $\frac{\text { sate Roure }}{\text { State }}$ | Snohomis ${ }_{\text {den }}$ | ${ }^{\text {Marssile }}$ Mansule |  |  |  |  |  |  |  | 5.60 5.60 | －01／24／2018 | 8 No A Pparerest |  |  |  |  | Soin Straibt Ahead | stoped for Trafic | West | ${ }_{\text {East }}^{\text {East }}$ | Vehice sopped | venicis sopoped |
| State Route | Snohomis ${ }^{\text {a }}$ | Marssille 5 |  |  |  |  |  |  |  | 5.51 | 06， 1772021 | 1）No Apparent tivur |  |  |  |  | Soins straibt Ahead | sowive | Nest | East | west | ast |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | stoppeat or rific | West | Last | vencie stopped | venicics sopened |
| State Route | Snotomis | massil |  |  |  |  |  |  |  |  | 21／7／20 | Aprasert |  |  |  |  | Oin sfreigh the | Stopeed or Trafic | west | Est | Vencice stopeed | Venicie sto |



## Appendix B

Existing Traffic Count Data

Location: 1 11TH AVE NE \& 172ND ST NE PM
Date: Tuesday, February 28, 2023
Peak Hour: 05:00 PM - 06:00 PM
(303) 216-2439 www.alltrafficdata.net

## Peak Hour

Motorized Vehicles


|  | HV\% | PHF |
| :--- | :--- | :--- |
| EB | $2.3 \%$ | 0.82 |
| WB | $0.9 \%$ | 0.95 |
| NB | $0.0 \%$ | 0.85 |
| SB | $0.0 \%$ | 0.81 |
| All | $1.3 \%$ | 0.91 |

Heavy Vehicles


Pedestrians/Bicycles in Crosswalk


## Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE <br> Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | 11TH AVE NE Northbound |  |  |  | 11TH AVE NE Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 40 | 1 | 0 | 11 | 93 | 1 | 0 | 3 | 0 | 12 | 0 | 3 | 0 | 0 | 164 | 698 |
| 4:15 PM | 0 | 0 | 54 | 4 | 0 | 20 | 104 | 0 | 0 | 1 | 1 | 12 | 0 | 0 | 0 | 0 | 196 | 701 |
| 4:30 PM | 0 | 0 | 56 | 1 | 0 | 13 | 88 | 5 | 0 | 2 | 1 | 11 | 0 | 0 | 1 | 0 | 178 | 658 |
| 4:45 PM | 0 | 1 | 40 | 1 | 0 | 15 | 88 | 3 | 0 | 1 | 1 | 9 | 0 | 1 | 0 | 0 | 160 | 670 |
| 5:00 PM | 0 | 0 | 42 | 0 | 0 | 17 | 89 | 3 | 0 | 0 | 0 | 12 | 0 | 3 | 0 | 1 | 167 | 703 |
| 5:15 PM | 0 | 0 | 46 | 0 | 0 | 12 | 78 | 6 | 0 | 1 | 0 | 8 | 0 | 0 | 1 | 1 | 153 |  |
| 5:30 PM | 0 | 1 | 62 | 0 | 0 | 14 | 97 | 2 | 0 | 1 | 1 | 9 | 0 | 3 | 0 | 0 | 190 |  |
| 5:45 PM | 0 | 1 | 64 | 1 | 0 | 14 | 97 | 3 | 0 | 3 | 0 | 6 | 0 | 1 | 0 | 3 | 193 |  |
| Count Total | 0 | 3 | 404 | 8 | 0 | 116 | 734 | 23 | 0 | 12 | 4 | 79 | 0 | 11 | 2 | 5 | 1,401 |  |
| Peak Hour | 0 | 2 | 214 | 1 | 0 | 57 | 361 | 14 | 0 | 5 | 1 | 35 | 0 | 7 | 1 | 5 | 703 |  |

Traffic Counts - Heavy Vehicles and Pedestrians/Bicycles in Crosswalk

| Interval Start Time | Heavy Vehicles |  |  |  |  | Interval Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 4:00 PM | 0 | 0 | 1 | 0 | 1 | 4:00 PM |  | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM |  | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 1 | 0 | 1 | 4:30 PM |  | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 2 | 0 | 0 | 0 | 2 | 4:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 1 | 0 | 1 | 0 | 2 | 5:00 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 2 | 0 | 2 | 5:15 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 1 | 0 | 1 | 5:30 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 4 | 0 | 0 | 0 | 4 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| Count Total | 7 | 0 | 6 | 0 | 13 | Count Total |  | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 5 | 0 | 4 | 0 | 9 | Peak Hour |  | 0 | 0 | 0 | 0 | 0 |

(303) 216-2439 www.alltrafficdata.net

Location: 2 19TH DR NE \& 172ND ST NE PM
Date: Tuesday, February 28, 2023
Peak Hour: 04:00 PM - 05:00 PM

## Peak Hour

Motorized Vehicles


|  | HV\% | PHF |
| :--- | :--- | :--- |
| EB | $1.9 \%$ | 0.88 |
| WB | $1.0 \%$ | 0.87 |
| NB | $0.0 \%$ | 0.70 |
| SB | $0.0 \%$ | 0.00 |
| All | $1.2 \%$ | 0.86 |

Heavy Vehicles


Pedestrians/Bicycles in Crosswalk


## Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE <br> Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | 19TH DR NE <br> Northbound |  |  |  | 19TH DR NE <br> Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 59 | 2 | 0 | 11 | 111 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 193 | 809 |
| 4:15 PM | 0 | 0 | 74 | 1 | 0 | 9 | 136 | 0 | 0 | 2 | 0 | 12 | 0 | 0 | 0 | 0 | 234 | 794 |
| 4:30 PM | 0 | 0 | 74 | 0 | 0 | 11 | 94 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 184 | 750 |
| 4:45 PM | 0 | 0 | 52 | 1 | 0 | 11 | 124 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 198 | 782 |
| 5:00 PM | 0 | 0 | 60 | 0 | 0 | 9 | 100 | 0 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 0 | 178 | 802 |
| 5:15 PM | 0 | 0 | 57 | 1 | 0 | 9 | 106 | 0 | 0 | 1 | 0 | 16 | 0 | 0 | 0 | 0 | 190 |  |
| 5:30 PM | 0 | 0 | 76 | 1 | 0 | 12 | 117 | 0 | 0 | 1 | 0 | 9 | 0 | 0 | 0 | 0 | 216 |  |
| 5:45 PM | 0 | 0 | 80 | 0 | 0 | 15 | 117 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 218 |  |
| Count Total | 0 | 0 | 532 | 6 | 0 | 87 | 905 | 0 | 0 | 6 | 0 | 75 | 0 | 0 | 0 | 0 | 1,611 |  |
| Peak Hour | 0 | 0 | 259 | 4 | 0 | 42 | 465 | 0 | 0 | 3 | 0 | 36 | 0 | 0 | 0 | 0 | 809 |  |

Traffic Counts - Heavy Vehicles and Pedestrians/Bicycles in Crosswalk

(303) 216-2439 www.alltrafficdata.net

Location: 3 19TH AVE NE \& 172ND ST NE PM
Date: Tuesday, February 28, 2023
Peak Hour: 04:00 PM - 05:00 PM

## Peak Hour

Motorized Vehicles


|  | HV\% | PHF |
| :--- | :--- | :--- |
| EB | $2.0 \%$ | 0.84 |
| WB | $0.8 \%$ | 0.87 |
| NB | $0.0 \%$ | 0.00 |
| SB | $0.0 \%$ | 0.63 |
| All | $1.2 \%$ | 0.85 |

Heavy Vehicles


Pedestrians/Bicycles in Crosswalk


Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | 19TH AVE NE <br> Northbound |  |  |  | 19TH AVE NE <br> Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 2 | 66 | 0 | 0 | 0 | 117 | 8 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 199 | 836 |
| 4:15 PM | 0 | 7 | 82 | 0 | 0 | 0 | 138 | 7 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 10 | 247 | 817 |
| 4:30 PM | 0 | 4 | 74 | 0 | 0 | 0 | 104 | 4 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 192 | 765 |
| 4:45 PM | 0 | 0 | 63 | 0 | 0 | 0 | 123 | 4 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 7 | 198 | 805 |
| 5:00 PM | 0 | 1 | 66 | 0 | 0 | 0 | 106 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 180 | 825 |
| 5:15 PM | 0 | 5 | 69 | 0 | 0 | 0 | 109 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 195 |  |
| 5:30 PM | 0 | 12 | 74 | 0 | 0 | 0 | 128 | 9 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 4 | 232 |  |
| 5:45 PM | 0 | 5 | 82 | 0 | 0 | 0 | 118 | 4 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 6 | 218 |  |
| Count Total | 0 | 36 | 576 | 0 | 0 | 0 | 943 | 45 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 43 | 1,661 |  |
| Peak Hour | 0 | 13 | 285 | 0 | 0 | 0 | 482 | 23 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 25 | 836 |  |

Traffic Counts - Heavy Vehicles and Pedestrians/Bicycles in Crosswalk

(303) 216-2439 www.alltrafficdata.net

## Location: 1 23RD AVE NE \& 172ND ST NE PM

Date: Thursday, June 2, 2022
Peak Hour: 04:30 PM - 05:30 PM

## Peak Hour



Pedestrians/Bicycles in Crosswalk


## Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE <br> Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | 23RD AVE NE <br> Northbound |  |  |  | 23RD AVE NE Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 11 | 134 | 0 | 11 | 0 | 147 | 29 | 0 | 0 | 0 | 4 | 0 | 33 | 0 | 8 | 377 | 1,468 |
| 4:15 PM | 0 | 9 | 125 | 0 | 5 | 0 | 164 | 36 | 0 | 0 | 0 | 0 | 0 | 33 | 1 | 7 | 380 | 1,478 |
| 4:30 PM | 0 | 8 | 127 | 0 | 7 | 0 | 141 | 40 | 0 | 0 | 0 | 2 | 0 | 39 | 0 | 2 | 366 | 1,497 |
| 4:45 PM | 0 | 2 | 101 | 0 | 5 | 0 | 150 | 39 | 0 | 0 | 0 | 1 | 0 | 41 | 0 | 6 | 345 | 1,443 |
| 5:00 PM | 1 | 6 | 111 | 0 | 5 | 0 | 165 | 53 | 0 | 0 | 0 | 0 | 0 | 40 | 3 | 3 | 387 | 1,449 |
| 5:15 PM | 1 | 11 | 120 | 0 | 11 | 0 | 164 | 45 | 0 | 1 | 0 | 1 | 0 | 39 | 0 | 6 | 399 |  |
| 5:30 PM | 1 | 8 | 94 | 0 | 4 | 0 | 133 | 45 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 2 | 312 |  |
| 5:45 PM | 3 | 10 | 111 | 0 | 7 | 0 | 141 | 46 | 0 | 1 | 0 | 0 | 0 | 28 | 0 | 4 | 351 |  |
| Count Total | 6 | 65 | 923 | 0 | 55 | 0 | 1,205 | 333 | 0 | 2 | 0 | 8 | 0 | 278 | 4 | 38 | 2,917 |  |
| Peak Hour | 2 | 27 | 459 | 0 | 28 | 0 | 620 | 177 | 0 | 1 | 0 | 4 | 0 | 159 | 3 | 17 | 1,497 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles in Crosswalk

| Interval Start Time | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 4:00 PM | 3 | 3 | 2 | 0 | 8 | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM |  | 0 | 1 | 0 | 0 | 1 |
| 4:15 PM | 2 | 0 | 3 | 0 | 5 | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM |  | 0 | 0 | 0 | 1 | 1 |
| 4:30 PM | 2 | 0 | 6 | 1 | 9 | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 4:30 PM |  | 0 | 1 | 0 | 1 | 2 |
| 4:45 PM | 5 | 0 | 1 | 1 | 7 | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM |  | 0 | 1 | 2 | 5 | 8 |
| 5:00 PM | 4 | 0 | 3 | 2 | 9 | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 1 | 0 | 3 | 0 | 4 | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 5:15 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 3 | 0 | 4 | 0 | 7 | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM |  | 1 | 3 | 0 | 0 | 4 |
| 5:45 PM | 3 | 1 | 0 | 0 | 4 | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| Count Total | 23 | 4 | 22 | 4 | 53 | Count Total | 0 | 0 | 0 | 0 | 0 | Count Total |  | 1 | 6 | 2 | 7 | 16 |
| Peak Hour | 12 | 0 | 13 | 4 | 29 | Peak Hour | 0 | 0 | 0 | 0 | 0 | Peak Hour |  | 0 | 2 | 2 | 6 | 10 |

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Date: Tuesday, June 7, 2022
Peak Hour: 04:15 PM - 05:15 PM

## Peak Hour



Pedestrians/Bicycles in Crosswalk


## Traffic Counts - Motorized Vehicles

| Interval Start Time | 172ND ST NE Eastbound |  |  |  | 172ND ST NE Westbound |  |  |  | 27TH AVE NE Northbound |  |  |  | 27TH AVE NE Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 3 | 115 | 36 | 0 | 147 | 104 | 57 | 0 | 62 | 23 | 145 | 0 | 77 | 32 | 3 | 804 | 3,405 |
| 4:15 PM | 0 | 9 | 102 | 28 | 0 | 194 | 139 | 77 | 0 | 45 | 23 | 157 | 0 | 61 | 22 | 8 | 865 | 3,471 |
| 4:30 PM | 0 | 8 | 116 | 34 | 0 | 149 | 148 | 66 | 0 | 42 | 28 | 161 | 0 | 83 | 21 | 8 | 864 | 3,457 |
| 4:45 PM | 0 | 7 | 100 | 26 | 0 | 191 | 140 | 57 | 0 | 52 | 16 | 153 | 0 | 93 | 33 | 4 | 872 | 3,459 |
| 5:00 PM | 0 | 5 | 108 | 32 | 0 | 186 | 162 | 48 | 0 | 45 | 22 | 151 | 0 | 81 | 22 | 8 | 870 | 3,328 |
| 5:15 PM | 0 | 5 | 112 | 32 | 0 | 174 | 156 | 58 | 0 | 38 | 15 | 159 | 0 | 70 | 24 | 8 | 851 |  |
| 5:30 PM | 0 | 3 | 122 | 31 | 0 | 192 | 142 | 59 | 0 | 39 | 26 | 147 | 0 | 74 | 21 | 10 | 866 |  |
| 5:45 PM | 0 | 5 | 71 | 24 | 0 | 152 | 136 | 58 | 1 | 41 | 13 | 165 | 0 | 49 | 23 | 3 | 741 |  |
| Count Total | 0 | 45 | 846 | 243 | 0 | 1,385 | 1,127 | 480 | 1 | 364 | 166 | 1,238 | 0 | 588 | 198 | 52 | 6,733 |  |
| Peak Hour | 0 | 29 | 426 | 120 | 0 | 720 | 589 | 248 | 0 | 184 | 89 | 622 | 0 | 318 | 98 | 28 | 3,471 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles in Crosswalk

(303) 216-2439 www.alltrafficdata.net

## Peak Hour

Heavy Vehicles


|  | HV\% | PHF |
| :--- | :--- | :--- |
| EB | $1.2 \%$ | 0.95 |
| WB | $1.6 \%$ | 0.97 |
| NB | $0.0 \%$ | 0.00 |
| SB | $3.8 \%$ | 0.89 |
| All | $1.8 \%$ | 0.97 |

## Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | I-5 SB RAMPS <br> Northbound |  |  |  | I-5 SB RAMPS <br> Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 258 | 123 | 0 | 0 | 274 | 148 | 0 | 0 | 0 | 0 | 0 | 73 | 0 | 68 | 944 | 3,828 |
| 4:15 PM | 0 | 0 | 266 | 113 | 0 | 0 | 328 | 134 | 0 | 0 | 0 | 0 | 0 | 88 | 0 | 67 | 996 | 3,862 |
| 4:30 PM | 0 | 0 | 235 | 114 | 0 | 0 | 299 | 165 | 0 | 0 | 0 | 0 | 0 | 70 | 0 | 58 | 941 | 3,798 |
| 4:45 PM | 0 | 0 | 262 | 103 | 0 | 0 | 336 | 120 | 0 | 0 | 0 | 0 | 0 | 62 | 0 | 64 | 947 | 3,788 |
| 5:00 PM | 0 | 0 | 241 | 110 | 0 | 0 | 340 | 143 | 0 | 0 | 0 | 0 | 0 | 64 | 0 | 80 | 978 | 3,724 |
| 5:15 PM | 0 | 0 | 224 | 116 | 0 | 0 | 323 | 127 | 0 | 0 | 0 | 0 | 0 | 67 | 0 | 75 | 932 |  |
| 5:30 PM | 0 | 0 | 224 | 121 | 0 | 0 | 315 | 130 | 0 | 0 | 0 | 0 | 0 | 74 | 0 | 67 | 931 |  |
| 5:45 PM | 0 | 0 | 215 | 89 | 0 | 0 | 323 | 110 | 0 | 0 | 0 | 0 | 0 | 63 | 0 | 83 | 883 |  |
| Count Total | 0 | 0 | 1,925 | 889 | 0 | 0 | 2,538 | 1,077 | 0 | 0 | 0 | 0 | 0 | 561 | 0 | 562 | 7,552 |  |
| Peak Hour | 0 | 0 | 1,004 | 440 | 0 | 0 | 1,303 | 562 | 0 | 0 | 0 | 0 | 0 | 284 | 0 | 269 | 3,862 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles in Crosswalk

| Interval Start Time | Heavy Vehicles |  |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | NB |  | WB | SB | Total |  | EB |  | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 4:00 PM | 11 |  | 0 | 7 | 5 | 23 | 4:00 PM |  | 0 | 0 | 0 | 0 | 0 | 4:00 PM |  | 0 | 0 | 0 | 4 | 4 |
| 4:15 PM | 4 |  | 0 | 10 | 6 | 20 | 4:15 PM |  | 0 | 0 | 0 | 0 | 0 | 4:15 PM |  | 0 | 0 | 0 | 1 | 1 |
| 4:30 PM | 4 |  | 0 | 11 | 3 | 18 | 4:30 PM |  | 1 | 0 | 0 | 0 | 1 | 4:30 PM |  | 0 | 0 | 0 | 2 | 2 |
| 4:45 PM | 6 |  | 0 | 2 | 7 | 15 | 4:45 PM |  | 0 | 0 | 0 | 0 | 0 | 4:45 PM |  | 1 | 0 | 0 | 2 | 3 |
| 5:00 PM | 4 |  | 0 | 6 | 5 | 15 | 5:00 PM |  | 0 | 0 | 0 | 0 | 0 | 5:00 PM |  | 0 | 0 | 0 | 6 | 6 |
| 5:15 PM | 0 |  | 0 | 6 | 4 | 10 | 5:15 PM |  | 0 | 0 | 0 | 0 | 0 | 5:15 PM |  | 0 | 0 | 0 | 2 | 2 |
| 5:30 PM | 2 |  | 0 | 3 | 5 | 10 | 5:30 PM |  | 0 | 0 | 0 | 0 | 0 | 5:30 PM |  | 3 | 0 | 0 | 2 | 5 |
| 5:45 PM | 11 |  | 0 | 1 | 1 | 13 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| Count Total | 42 |  | 0 | 46 | 36 | 124 | Count Total |  | 1 | 0 | 0 | 0 | 1 | Count Total |  | 4 | 0 | 0 | 19 | 23 |
| Peak Hour | 18 |  | 0 | 29 | 21 | 68 | Peak Hour |  | 1 | 0 | 0 | 0 | 1 | Peak Hour |  | 1 | 0 | 0 | 11 | 12 |

Location: 5 I-5 NB RAMPS \& 172ND ST NE PM
Date: Thursday, June 2, 2022
Peak Hour: 04:15 PM - 05:15 PM
(303) 216-2439 www.alltrafficdata.net

## Peak Hour



Pedestrians/Bicycles in Crosswalk


## Traffic Counts - Motorized Vehicles

| Interval | 172ND ST NE <br> Eastbound |  |  |  | 172ND ST NE <br> Westbound |  |  |  | I-5 NB RAMPS Northbound |  |  |  | I-5 NB RAMPS Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 86 | 241 | 0 | 0 | 0 | 296 | 101 | 0 | 115 | 0 | 189 | 0 | 0 | 0 | 0 | 1,028 | 4,300 |
| 4:15 PM | 0 | 83 | 270 | 0 | 0 | 0 | 306 | 129 | 0 | 138 | 0 | 176 | 0 | 0 | 0 | 0 | 1,102 | 4,327 |
| 4:30 PM | 0 | 76 | 230 | 0 | 0 | 0 | 355 | 119 | 0 | 133 | 1 | 191 | 0 | 0 | 0 | 0 | 1,105 | 4,235 |
| 4:45 PM | 0 | 77 | 229 | 0 | 0 | 0 | 306 | 111 | 0 | 150 | 0 | 192 | 0 | 0 | 0 | 0 | 1,065 | 4,139 |
| 5:00 PM | 0 | 82 | 218 | 0 | 0 | 0 | 312 | 116 | 0 | 155 | 1 | 171 | 0 | 0 | 0 | 0 | 1,055 | 4,004 |
| 5:15 PM | 0 | 52 | 214 | 0 | 0 | 0 | 312 | 113 | 0 | 135 | 0 | 184 | 0 | 0 | 0 | 0 | 1,010 |  |
| 5:30 PM | 0 | 86 | 209 | 0 | 0 | 0 | 310 | 111 | 0 | 131 | 1 | 161 | 0 | 0 | 0 | 0 | 1,009 |  |
| 5:45 PM | 1 | 72 | 203 | 0 | 0 | 0 | 273 | 85 | 0 | 141 | 0 | 155 | 0 | 0 | 0 | 0 | 930 |  |
| Count Total | 1 | 614 | 1,814 | 0 | 0 | 0 | 2,470 | 885 | 0 | 1,098 | 3 | 1,419 | 0 | 0 | 0 | 0 | 8,304 |  |
| Peak Hour | 0 | 318 | 947 | 0 | 0 | 0 | 1,279 | 475 | 0 | 576 | 2 | 730 | 0 | 0 | 0 | 0 | 4,327 |  |

Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles in Crosswalk

| Interval Start Time | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  |  | Interval <br> Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 4:00 PM | 12 | 6 | 11 | 0 | 29 | 4:00 PM |  | 0 | 0 | 0 | 0 | 0 | 4:00 PM |  | 0 | 2 | 0 | 4 | 6 |
| 4:15 PM | 7 | 8 | 17 | 0 | 32 | 4:15 PM |  | 0 | 0 | 0 | 0 | 0 | 4:15 PM |  | 0 | 5 | 0 | 1 | 6 |
| 4:30 PM | 2 | 8 | 4 | 0 | 14 | 4:30 PM |  | 0 | 0 | 0 | 0 | 0 | 4:30 PM |  | 0 | 3 | 2 | 0 | 5 |
| 4:45 PM | 11 | 6 | 5 | 0 | 22 | 4:45 PM |  | 0 | 0 | 0 | 0 | 0 | 4:45 PM |  | 0 | 1 | 0 | 2 | 3 |
| 5:00 PM | 7 | 2 | 10 | 0 | 19 | 5:00 PM |  | 0 | 0 | 0 | 0 | 0 | 5:00 PM |  | 0 | 2 | 2 | 5 | 9 |
| 5:15 PM | 5 | 10 | 6 | 0 | 21 | 5:15 PM |  | 0 | 0 | 0 | 0 | 0 | 5:15 PM |  | 0 | 5 | 0 | 0 | 5 |
| 5:30 PM | 6 | 1 | 3 | 0 | 10 | 5:30 PM |  | 0 | 0 | 0 | 0 | 0 | 5:30 PM |  | 0 | 2 | 0 | 2 | 4 |
| 5:45 PM | 5 | 2 | 2 | 0 | 9 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 | 5:45 PM |  | 0 | 3 | 0 | 0 | 3 |
| Count Total | 55 | 43 | 58 | 0 | 156 | Count Total |  | 0 | 0 | 0 | 0 | 0 | Count Total |  | 0 | 23 | 4 | 14 | 41 |
| Peak Hour | 27 | 24 | 36 | 0 | 87 | Peak Hour |  | 0 | 0 | 0 | 0 | 0 | Peak Hour |  | 0 | 11 | 4 | 8 | 23 |

Location: 1 19TH DR NE \& 174TH ST NE PM
Date: Tuesday, March 14, 2023
Peak Hour: 04:00 PM - 05:00 PM
(303) 216-2439 www.alltrafficdata.net

## Peak Hour

Motorized Vehicles


|  | HV\% | PHF |
| :--- | :--- | :--- |
| EB | $0.0 \%$ | 0.00 |
| WB | $2.6 \%$ | 0.81 |
| NB | $0.0 \%$ | 0.85 |
| SB | $0.0 \%$ | 0.84 |
| All | $0.6 \%$ | 0.84 |

Heavy Vehicles


Pedestrians/Bicycles in Crosswalk


Traffic Counts - Motorized Vehicles

| Interval | 174TH ST NE <br> Eastbound |  |  |  | 174TH ST NE <br> Westbound |  |  |  | 19TH DR NE <br> Northbound |  |  |  | 19TH DR NE <br> Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 15 | 0 | 0 | 6 | 10 | 0 | 38 | 167 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 7 | 0 | 0 | 10 | 5 | 0 | 11 | 8 | 0 | 45 | 164 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 7 | 0 | 0 | 12 | 6 | 0 | 7 | 13 | 0 | 50 | 147 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 7 | 0 | 0 | 11 | 2 | 0 | 3 | 9 | 0 | 34 | 127 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 3 | 0 | 0 | 14 | 1 | 0 | 4 | 8 | 0 | 35 | 127 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 5 | 0 | 0 | 13 | 1 | 0 | 2 | 4 | 0 | 28 |  |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 0 | 7 | 0 | 0 | 8 | 9 | 0 | 30 |  |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 9 | 0 | 0 | 9 | 1 | 0 | 3 | 11 | 0 | 34 |  |
| Count Total | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 48 | 0 | 0 | 91 | 16 | 0 | 44 | 72 | 0 | 294 |  |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 26 | 0 | 0 | 48 | 13 | 0 | 27 | 40 | 0 | 167 |  |

Traffic Counts - Heavy Vehicles and Pedestrians/Bicycles in Crosswalk

| Interval Start Time | Heavy Vehicles |  |  |  |  | Interval Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | NB | WB | SB | Total |  | EB |  | NB | WB | SB | Total |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM |  | 0 | 0 | 1 | 0 | 1 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM |  | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 1 | 0 | 1 | 4:30 PM |  | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 1 | 0 | 0 | 1 | 5:15 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM |  | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 5:45 PM |  | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 1 | 1 | 0 | 2 | Count Total |  | 0 | 0 | 1 | 0 | 1 |
| Peak Hour | 0 | 0 | 1 | 0 | 1 | Peak Hour |  | 0 | 0 | 1 | 0 | 1 |

## Appendix C

Level of Service (LOS) Calculations

2023 Existing - Weekday PM Peak Hour

|  | $\rangle$ |  |  | $t$ | $\leftarrow$ |  |  | $\uparrow$ |  | $\downarrow$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  | \% | 1 |  |  | \$ |  |  | \$ |  |
| Traffic Volume (vph) | 2 | 214 | 1 | 57 | 361 | 14 | 5 | 1 | 35 | 7 | 1 | 5 |
| Future Volume (vph) | 2 | 214 | 1 | 57 | 361 | 14 | 5 | 1 | 35 | 7 | 1 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 5\% |  |  | -4\% |  |
| Storage Length (tt) | 0 |  | 0 | 175 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 35 |  |  | 25 |  |  | 25 |  |  | 25 |  |
| Link Distance (ft) |  | 369 |  |  | 1809 |  |  | 529 |  |  | 387 |  |
| Travel Time (s) |  | 7.2 |  |  | 49.3 |  |  | 14.4 |  |  | 10.6 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |



| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 412 | 0 | 0 | 236 | 0 | 0 | 774 | 778 | 236 | 790 | 771 | 405 |
| Stage 1 | - | - | - | - | - | - | 240 | 240 | - | 531 | 531 | - |
| Stage 2 | - | - | - | - | - | - | 534 | 538 | - | 259 | 240 | - |
| Critical Hdwy | 4.12 | - | - | 4.11 | - | - | 8.1 | 7.5 | 6.7 | 6.3 | 5.7 | 5.8 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 7.1 | 6.5 | - | 5.3 | 4.7 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 7.1 | 6.5 | - | 5.3 | 4.7 | - |
| Follow-up Hdwy | 2.218 | - | - | 2.209 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1147 | - | - | 1337 | - | - | 257 | 266 | 782 | 370 | 395 | 680 |
| Stage 1 | - | - | - | - | - | - | 718 | 665 | - | 603 | 596 | - |
| Stage 2 | - | - | - | - | - | - | 460 | 453 | - | 795 | 750 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1147 | - | - | 1337 | - | - | 245 | 253 | 782 | 337 | 376 | 680 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 245 | 253 | - | 337 | 376 | - |
| Stage 1 | - | - | - | - | - | - | 717 | 664 | - | 602 | 568 | - |
| Stage 2 | - | - | - | - | - | - | 434 | 432 | - | 753 | 749 | - |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 1 | 11.6 | 13.8 |
| HCM LOS |  | $B$ | $B$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 593 | 1147 | - | - | 1337 | - | - |
| HCM Lane V/C Ratio | 0.076 | 0.002 | - | - | 0.047 | - | - |
| HCM Control Delay (s) | 11.6 | 8.1 | 0 | - | 7.8 | - | - |
| HCM Lane LOS | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 0 | - | - | 0.1 | - | - |




|  | 4 | $\rightarrow$ | 4 |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\hat{*}$ | 个 |  | M |  |
| Traffic Volume (vph) | 13 | 285 | 482 | 23 | 8 | 25 |
| Future Volume (vph) | 13 | 285 | 482 | 23 | 8 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Link Speed (mph) |  | 25 | 25 |  | 35 |  |
| Link Distance (ft) |  | 686 | 653 |  | 670 |  |
| Travel Time (s) |  | 18.7 | 17.8 |  | 13.1 |  |
| Peak Hour Factor | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 |
| Heavy Vehicles (\%) | 2\% | 2\% | 1\% | 1\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Sign Control |  | Free | Free |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |



## LANE LEVEL OF SERVICE

## Lane Level of Service

$\square$ Site: 4 [2023 Existing - PM Peak Hour (Site Folder: 23rd Ave
NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.2.202
23rd Ave NE / 172nd St NE
Site Category: 2023 Existing - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used). Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [2023 Existing - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202
23rd Ave NE / 172nd St NE
Site Category: 2023 Existing - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|l} \hline \text { Mov } \\ \hline \text { ID } \end{array}$ |  | Mov Class |  | $\begin{aligned} & \text { rand } \\ & \text { lows } \\ & \mathrm{HV} \text { ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { rival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{array}$ | $\begin{gathered} c k \text { Of } \\ \text { ue } \\ \text { Dist ] } \\ \text { ft } \end{gathered}$ | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed <br> mph |
| South: Private Dwy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.008 | 8.6 | LOS A | 0.0 | 1.1 | 0.66 | 0.49 | 0.66 | 23.5 |
| 8 | T1 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.008 | 3.6 | LOS A | 0.0 | 1.1 | 0.66 | 0.49 | 0.66 | 23.7 |
| 18 | R2 | All MCs | 4 | 0.0 | 4 | 0.0 | 0.008 | 4.3 | LOS A | 0.0 | 1.1 | 0.66 | 0.49 | 0.66 | 23.6 |
| Appr |  |  | 6 | 0.0 | 6 | 0.0 | 0.008 | 4.9 | LOS A | 0.0 | 1.1 | 0.66 | 0.49 | 0.66 | 23.6 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 31 | 1.6 | 31 | 1.6 | 0.422 | 10.9 | LOS B | 3.2 | 82.2 | 0.18 | 0.33 | 0.18 | 31.9 |
| 1 | L2 | All MCs | 1 | 1.6 | 1 | 1.6 | 0.422 | 8.7 | LOS A | 3.2 | 82.2 | 0.18 | 0.33 | 0.18 | 31.9 |
| 6 | T1 | All MCs | 680 | 1.6 | 680 | 1.6 | 0.422 | 3.1 | LOS A | 3.2 | 82.2 | 0.18 | 0.33 | 0.18 | 32.5 |
| 16 | R2 | All MCs | 194 | 1.6 | 194 | 1.6 | 0.157 | 3.6 | LOS A | 0.9 | 21.8 | 0.16 | 0.41 | 0.16 | 32.2 |
| Appr |  |  | 905 | 1.6 | 905 | 1.6 | 0.422 | 3.5 | LOS A | 3.2 | 82.2 | 0.18 | 0.35 | 0.18 | 32.4 |
| North: 23 rd Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 174 | 2.2 | 174 | 2.2 | 0.226 | 9.2 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 0.68 | 22.7 |
| 4 | T1 | All MCs | 3 | 2.2 | 3 | 2.2 | 0.226 | 3.9 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 0.68 | 22.9 |
| 14 | R2 | All MCs | 19 | 2.2 | 19 | 2.2 | 0.226 | 5.0 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 0.68 | 22.8 |
| Appr |  |  | 197 | 2.2 | 197 | 2.2 | 0.226 | 8.7 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 0.68 | 22.7 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 2 | 2.5 | 2 | 2.5 | 0.436 | 11.9 | LOS B | 3.0 | 76.8 | 0.49 | 0.44 | 0.49 | 31.3 |
| 5 | L2 | All MCs | 30 | 2.5 | 30 | 2.5 | 0.436 | 9.7 | LOS A | 3.0 | 76.8 | 0.49 | 0.44 | 0.49 | 31.3 |
| 2 | T1 | All MCs | 503 | 2.5 | 503 | 2.5 | 0.436 | 3.7 | LOS A | 3.0 | 76.8 | 0.49 | 0.44 | 0.49 | 31.8 |
| 12 | R2 | All MCs | 1 | 2.5 | 1 | 2.5 | 0.436 | 4.0 | LOS A | 3.0 | 76.8 | 0.49 | 0.44 | 0.49 | 31.6 |
| Approach |  |  | 536 | 2.5 | 536 | 2.5 | 0.436 | 4.1 | LOS A | 3.0 | 76.8 | 0.49 | 0.44 | 0.49 | 31.8 |
| All Vehicles |  |  | 1645 | 2.0 | 1645 | 2.0 | 0.436 | 4.3 | LOS A | 3.2 | 82.2 | 0.34 | 0.42 | 0.34 | 30.6 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {¢ }}$ |  | ${ }^{7} 1$ | 中4 | 「 | \％ | 4 | 「＇ | 1 | $\uparrow$ |  |
| Traffic Volume（vph） | 30 | 439 | 124 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 101 | 29 |
| Future Volume（vph） | 30 | 439 | 124 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 101 | 29 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 250 |  | 0 | 425 |  | 200 | 125 |  | 0 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 2 |  | 1 | 1 |  | 1 | 2 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 25 |  |  | 25 |  |
| Link Distance（ft） |  | 394 |  |  | 613 |  |  | 444 |  |  | 470 |  |
| Travel Time（s） |  | 7.7 |  |  | 11.9 |  |  | 12.1 |  |  | 12.8 |  |
| Confl．Peds．（\＃／hr） | 1 |  |  |  |  | 1 | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Turn Type | Prot | NA |  | Prot | NA | Perm | Prot | NA | pt＋ov | Prot | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 81 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  | 6 |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 | 6 | 3 | 8 | 81 | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 7.0 |  | 3.0 | 7.0 | 7.0 | 3.0 | 5.0 |  | 3.0 | 5.0 |  |
| Minimum Split（s） | 9.0 | 38.0 |  | 9.0 | 38.0 | 38.0 | 9.0 | 11.0 |  | 9.0 | 46.0 |  |
| Total Split（s） | 20.0 | 40.0 |  | 40.0 | 60.0 | 60.0 | 35.0 | 15.0 |  | 35.0 | 15.0 |  |
| Total Split（\％） | 15．4\％ | 30．8\％ |  | 30．8\％ | 46．2\％ | 46．2\％ | 26．9\％ | 11．5\％ |  | 26．9\％ | 11．5\％ |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／Lag | Lead | Lead |  | Lag | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | Min |  | C－Min | C－Min | C－Min | None | None |  | Min | Min |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 75 （58\％），Referenced to phase 1：WBL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 135 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：$\quad$ 5：27th Ave NE／Spring Ln Ave \＆172nd St NE


HCM 6th Signalized Intersection Summary
5：27th Ave NE／Spring Ln Ave \＆172nd St NE

|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\dagger$ | \％ |  | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {a }}$ |  | \％ | 中4 | 7 | \％ | 4 | 「＇ | ${ }^{7} 1$ | $\dagger$ |  |
| Traffic Volume（veh／h） | 30 | 439 | 124 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 101 | 29 |
| Future Volume（veh／h） | 30 | 439 | 124 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 101 | 29 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 30 | 439 | 124 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 101 | 29 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 38 | 1084 | 304 | 797 | 2160 | 963 | 218 | 146 | 488 | 396 | 97 | 28 |
| Arrive On Green | 0.02 | 0.40 | 0.40 | 0.38 | 1.00 | 1.00 | 0.12 | 0.08 | 0.08 | 0.11 | 0.07 | 0.07 |
| Sat Flow，veh／h | 1781 | 2741 | 768 | 3483 | 3582 | 1596 | 1795 | 1885 | 1585 | 3483 | 1405 | 403 |
| Grp Volume（v），veh／h | 30 | 283 | 280 | 742 | 607 | 255 | 190 | 92 | 641 | 328 | 0 | 130 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1732 | 1742 | 1791 | 1596 | 1795 | 1885 | 1585 | 1742 | 0 | 1808 |
| Q Serve（g＿s），s | 2.2 | 14.9 | 15.1 | 26.6 | 0.0 | 0.0 | 13.5 | 6.2 | 9.2 | 12.0 | 0.0 | 9.0 |
| Cycle Q Clear（g＿c），s | 2.2 | 14.9 | 15.1 | 26.6 | 0.0 | 0.0 | 13.5 | 6.2 | 9.2 | 12.0 | 0.0 | 9.0 |
| Prop In Lane | 1.00 |  | 0.44 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.22 |
| Lane Grp Cap（c），veh／h | 38 | 703 | 685 | 797 | 2160 | 963 | 218 | 146 | 488 | 396 | 0 | 125 |
| V／C Ratio（X） | 0.79 | 0.40 | 0.41 | 0.93 | 0.28 | 0.26 | 0.87 | 0.63 | 1.31 | 0.83 | 0.00 | 1.04 |
| Avail Cap（c＿a），veh／h | 192 | 703 | 685 | 911 | 2160 | 963 | 401 | 146 | 488 | 777 | 0 | 125 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 0.78 | 0.78 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 63.3 | 28.3 | 28.3 | 39.2 | 0.0 | 0.0 | 56.1 | 58.2 | 20.7 | 56.4 | 0.0 | 60.5 |
| Incr Delay（d2），s／veh | 22.9 | 0.4 | 0.4 | 11.8 | 0.3 | 0.5 | 7.8 | 8.5 | 154.8 | 3.4 | 0.0 | 91.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.2 | 6.4 | 6.3 | 11.2 | 0.1 | 0.1 | 6.6 | 3.3 | 30.3 | 5.5 | 0.0 | 7.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 86.2 | 28.6 | 28.7 | 50.9 | 0.3 | 0.5 | 63.9 | 66.7 | 175.4 | 59.8 | 0.0 | 151.5 |
| LnGrp LOS | F | C | C | D | A | A | E | E | F | E | A | F |
| Approach Vol，veh／h |  | 593 |  |  | 1604 |  |  | 923 |  |  | 458 |  |
| Approach Delay，s／veh |  | 31.6 |  |  | 23.7 |  |  | 141.6 |  |  | 85.8 |  |
| Approach LOS |  | C |  |  | C |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 35.8 | 57.4 | 21.8 | 15.0 | 8.8 | 84.4 | 20.8 | 16.1 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 34.0 | 34.0 | 29.0 | 9.0 | 14.0 | 54.0 | 29.0 | 9.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 28.6 | 17.1 | 15.5 | 11.0 | 4.2 | 2.0 | 14.0 | 11.2 |  |  |  |  |
| Green Ext Time（p＿c），s | 1.2 | 3.1 | 0.3 | 0.0 | 0.0 | 5.6 | 0.8 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 63.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | E |  |  |  |  |  |  |  |  |  |

Notes
User approved pedestrian interval to be less than phase max green．

|  | 4 | $\rightarrow$ |  |  |  |  | 4 | 4 | \％ | $\pm$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 中4 | 「 |  |  |  | \％ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 0 | 1034 | 453 | 0 | 1342 | 579 | 0 | 0 | 0 | 293 | 0 | 277 |
| Future Volume（vph） | 0 | 1034 | 453 | 0 | 1342 | 579 | 0 | 0 | 0 | 293 | 0 | 277 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 3\％ |  |  | －3\％ |  |  | 0\％ |  |  | 3\％ |  |
| Storage Length（ft） | 0 |  | 250 | 0 |  | 0 | 0 |  | 0 | 400 |  | 400 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 0 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 613 |  |  | 915 |  |  | 299 |  |  | 608 |  |
| Travel Time（s） |  | 11.9 |  |  | 17.8 |  |  | 6.8 |  |  | 13.8 |  |
| Confl．Peds．（\＃／hr） | 11 |  |  |  |  | 11 | 1 |  |  |  |  | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 1\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ | 4\％ | 4\％ | 4\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 50\％ |  |  |
| Turn Type |  | NA | Perm |  | NA | Perm |  |  |  | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  |  |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  |  |  |  | 4 |
| Detector Phase |  | 2 | 2 |  | 6 | 6 |  |  |  | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  |  | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） |  | 24.8 | 24.8 |  | 34.1 | 34.1 |  |  |  | 33.8 | 33.8 | 33.8 |
| Total Split（s） |  | 90.0 | 90.0 |  | 40.0 | 40.0 |  |  |  | 40.0 | 40.0 | 40.0 |
| Total Split（\％） |  | 69．2\％ | 69．2\％ |  | 30．8\％ | 30．8\％ |  |  |  | 30．8\％ | 30．8\％ | 30．8\％ |
| Yellow Time（s） |  | 3.8 | 3.8 |  | 4.1 | 4.1 |  |  |  | 3.8 | 3.8 | 3.8 |
| All－Red Time（s） |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 5.8 | 5.8 |  | 6.1 | 6.1 |  |  |  | 5.8 | 5.8 | 5.8 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode |  | C－Min | C－Min |  | C－Min | C－Min |  |  |  | None | None | None |

Intersection Summary
Area Type：
Other
Cycle Length： 130
Actuated Cycle Length： 130
Offset： 0 （0\％），Referenced to phase 2：EBT and 6：WBT，Start of Red
Natural Cycle： 70
Control Type：Actuated－Coordinated
Splits and Phases：6：I－5 SB Ramp \＆172nd St NE


|  | $\rangle$ | $\rightarrow$ | $\checkmark$ | 7 |  |  |  |  | \％ |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 中4 | 「 |  | 性 | 「 |  |  |  | ${ }^{1}$ | $\uparrow$ | 7 |
| Traffic Volume（veh／h） | 0 | 1034 | 453 | 0 | 1342 | 579 | 0 | 0 | 0 | 293 | 0 | 277 |
| Future Volume（veh／h） | 0 | 1034 | 453 | 0 | 1342 | 579 | 0 | 0 | 0 | 293 | 0 | 277 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 0 | 1832 | 1832 | 0 | 1988 | 1988 |  |  |  | 1788 | 1788 | 1788 |
| Adj Flow Rate，veh／h | 0 | 1066 | 0 | 0 | 1384 | 0 |  |  |  | 302 | 0 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |  |  |  | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 1 | 1 | 0 | 2 | 2 |  |  |  | 4 | 4 | 4 |
| Cap，veh／h | 0 | 2752 |  | 0 | 2986 |  |  |  |  | 401 | 0 |  |
| Arrive On Green | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 |  |  |  | 0.12 | 0.00 | 0.00 |
| Sat Flow，veh／h | 0 | 3573 | 1553 | 0 | 3877 | 1685 |  |  |  | 3405 | 0 | 1515 |
| Grp Volume（v），veh／h | 0 | 1066 | 0 | 0 | 1384 | 0 |  |  |  | 302 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1741 | 1553 | 0 | 1889 | 1685 |  |  |  | 1703 | 0 | 1515 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 11.2 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 11.2 | 0.0 | 0.0 |
| Prop In Lane | 0.00 |  | 1.00 | 0.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 2752 |  | 0 | 2986 |  |  |  |  | 401 | 0 |  |
| V／C Ratio（X） | 0.00 | 0.39 |  | 0.00 | 0.46 |  |  |  |  | 0.75 | 0.00 |  |
| Avail Cap（c＿a），veh／h | 0 | 2752 |  | 0 | 2986 |  |  |  |  | 896 | 0 |  |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 2.00 | 2.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.56 | 0.00 | 0.00 | 0.69 | 0.00 |  |  |  | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 55.5 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 4.9 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 |  |  |  | 5.1 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 60.4 | 0.0 | 0.0 |
| LnGrp LOS | A | A |  | A | A |  |  |  |  | E | A |  |
| Approach Vol，veh／h |  | 1066 |  |  | 1384 |  |  |  |  |  | 302 |  |
| Approach Delay，s／veh |  | 0.2 |  |  | 0.4 |  |  |  |  |  | 60.4 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | E |  |
| Timer－Assigned Phs |  | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 108.9 |  | 21.1 |  | 108.9 |  |  |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s |  | ＊ 6.1 |  | ＊ 5.8 |  | 6.1 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | ＊ 84 |  | ＊ 34 |  | 33.9 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 13.2 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 15.7 |  | 1.9 |  | 17.6 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［EBR，WBR，SBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 |  |  |  |  |  | $4$ | 9 | $p$ | $\pm$ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 44 |  |  | 种4 | 「 | \％ | \＆ | 「゙ |  |  |  |
| Traffic Volume（vph） | 328 | 975 | 0 | 0 | 1317 | 489 | 593 | 2 | 752 | 0 | 0 | 0 |
| Future Volume（vph） | 328 | 975 | 0 | 0 | 1317 | 489 | 593 | 2 | 752 | 0 | 0 | 0 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 0\％ |  |  | 6\％ |  |  | 5\％ |  |  | 0\％ |  |
| Storage Length（ft） | 600 |  | 0 | 0 |  | 300 | 400 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 1 | 0 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 915 |  |  | 978 |  |  | 589 |  |  | 234 |  |
| Travel Time（s） |  | 17.8 |  |  | 19.1 |  |  | 13.4 |  |  | 5.3 |  |
| Confl．Peds．（\＃／hr） | 8 |  | 11 | 11 |  | 8 |  |  | 4 | 4 |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ |
| Shared Lane Trafic（\％） |  |  |  |  |  |  | 50\％ |  |  |  |  |  |
| Turn Type | pm＋pt | NA |  |  | NA | Perm | Split | NA | Perm |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 | 8 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  | 6 |  |  | 8 |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 | 6 | 8 | 8 | 8 |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ s ） | 5.0 | 7.0 |  |  | 7.0 | 7.0 | 5.0 | 5.0 | 5.0 |  |  |  |
| Minimum Split（s） | 10.6 | 24.1 |  |  | 23.8 | 23.8 | 40.8 | 40.8 | 40.8 |  |  |  |
| Total Split（s） | 40.0 | 89.0 |  |  | 49.0 | 49.0 | 41.0 | 41.0 | 41.0 |  |  |  |
| Total Split（\％） | 30．8\％ | 68．5\％ |  |  | 37．7\％ | 37．7\％ | 31．5\％ | 31．5\％ | 31．5\％ |  |  |  |
| Yellow Time（s） | 3.6 | 4.1 |  |  | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |  |  |
| All－Red Time（s） | 2.0 | 2.0 |  |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |  |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Total Lost Time（s） | 5.6 | 6.1 |  |  | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |  |  |  |
| Lead／Lag | Lead |  |  |  | Lag | Lag |  |  |  |  |  |  |
| Lead－Lag Optimize？ | Yes |  |  |  | Yes | Yes |  |  |  |  |  |  |
| Recall Mode | None | C－Min |  |  | C－Min | C－Min | None | None | None |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 0 （0\％），Referenced to phase 2：EBTL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：7：I－5 NB Ramps \＆172nd St NE


HCM 6th Signalized Intersection Summary
7：I－5 NB Ramps \＆172nd St NE

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 | 4 | \％ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 44 |  |  | 坐乐 | 「 | \％ | $\uparrow$ | 「 |  |  |  |
| Traffic Volume（veh／h） | 328 | 975 | 0 | 0 | 1317 | 489 | 593 | 2 | 752 | 0 | 0 | 0 |
| Future Volume（veh／h） | 328 | 975 | 0 | 0 | 1317 | 489 | 593 | 2 | 752 | 0 | 0 | 0 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 0 | 0 | 1658 | 1658 | 1723 | 1723 | 1723 |  |  |  |
| Adj Flow Rate，veh／h | 335 | 995 | 0 | 0 | 1344 | 0 | 606 | 0 | 0 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |  |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 0 | 0 | 2 | 2 | 2 | 2 | 2 |  |  |  |
| Cap，veh／h | 392 | 2450 | 0 | 0 | 2419 |  | 719 | 0 |  |  |  |  |
| Arrive On Green | 0.22 | 1.00 | 0.00 | 0.00 | 0.53 | 0.00 | 0.22 | 0.00 | 0.00 |  |  |  |
| Sat Flow，veh／h | 1781 | 3647 | 0 | 0 | 4676 | 1405 | 3282 | 0 | 1460 |  |  |  |
| Grp Volume（v），veh／h | 335 | 995 | 0 | 0 | 1344 | 0 | 606 | 0 | 0 |  |  |  |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 0 | 0 | 1509 | 1405 | 1641 | 0 | 1460 |  |  |  |
| Q Serve（g＿s），s | 11.6 | 0.0 | 0.0 | 0.0 | 25.6 | 0.0 | 23.0 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear（g＿c），s | 11.6 | 0.0 | 0.0 | 0.0 | 25.6 | 0.0 | 23.0 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 1.00 |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 392 | 2450 | 0 | 0 | 2419 |  | 719 | 0 |  |  |  |  |
| V／C Ratio（X） | 0.85 | 0.41 | 0.00 | 0.00 | 0.56 |  | 0.84 | 0.00 |  |  |  |  |
| Avail Cap（c＿a），veh／h | 664 | 2450 | 0 | 0 | 2419 |  | 889 | 0 |  |  |  |  |
| HCM Platoon Ratio | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter（I） | 0.90 | 0.90 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |  |  |
| Uniform Delay（d），s／veh | 16.4 | 0.0 | 0.0 | 0.0 | 20.0 | 0.0 | 48.6 | 0.0 | 0.0 |  |  |  |
| Incr Delay（d2），s／veh | 5.0 | 0.5 | 0.0 | 0.0 | 0.9 | 0.0 | 7.3 | 0.0 | 0.0 |  |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \％ile BackOfQ（50\％），veh／ln | 5.3 | 0.2 | 0.0 | 0.0 | 8.9 | 0.0 | 10.1 | 0.0 | 0.0 |  |  |  |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 21.4 | 0.5 | 0.0 | 0.0 | 21.0 | 0.0 | 55.9 | 0.0 | 0.0 |  |  |  |
| LnGrp LOS | C | A | A | A | C |  | E | A |  |  |  |  |
| Approach Vol，veh／h |  | 1330 |  |  | 1344 |  |  | 606 |  |  |  |  |
| Approach Delay，s／veh |  | 5.7 |  |  | 21.0 |  |  | 55.9 |  |  |  |  |
| Approach LOS |  | A |  |  | C |  |  | E |  |  |  |  |
| Timer－Assigned Phs |  | 2 |  |  | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ |  | 95.7 |  |  | 20.1 | 75.6 |  | 34.3 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s |  | 6.1 |  |  | 5.6 | ＊ 6.1 |  | 5.8 |  |  |  |  |
| Max Green Setting（Gmax），s |  | 82.9 |  |  | 34.4 | ＊ 43 |  | 35.2 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  |  | 13.6 | 27.6 |  | 25.0 |  |  |  |  |
| Green Ext Time（p＿c），s |  | 14.0 |  |  | 1.0 | 10.3 |  | 3.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 21.2 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

2026 No Action - Weekday PM Peak Hour

|  | $\Rightarrow$ |  |  | $\checkmark$ | $\leftarrow$ |  | 4 | 4 | 7 | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  | \% | $\hat{1}$ |  |  | $\uparrow$ |  |  | \& |  |
| Trafic Volume (vph) | 2 | 234 | 1 | 62 | 394 | 15 | 5 | 1 | 38 | 8 | 1 | 5 |
| Future Volume (vph) | 2 | 234 | 1 | 62 | 394 | 15 | 5 | 1 | 38 | 8 | 1 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 5\% |  |  | -4\% |  |
| Storage Length (ft) | 0 |  | 0 | 175 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 35 |  |  | 25 |  |  | 25 |  |  | 25 |  |
| Link Distance (ft) |  | 369 |  |  | 1809 |  |  | 529 |  |  | 387 |  |
| Travel Time (s) |  | 7.2 |  |  | 49.3 |  |  | 14.4 |  |  | 10.6 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other <br> Control Type: Unsignalized  | Other |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |




|  | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Approach | 1 | 12 | 14.9 |  |
| HCM Control Delay, s | 0.1 |  | B | B |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 565 | 1111 | - | - | 1313 | - | - | 380 |
| HCM Lane V/C Ratio | 0.086 | 0.002 | - | - | 0.052 | - | - | 0.04 |
| HCM Control Delay (s) | 12 | 8.2 | 0 | - | 7.9 | - | - | 14.9 |
| HCM Lane LOS | B | A | A | - | A | - | - | B |
| HCM 95th \%tile Q(veh) | 0.3 | 0 |  |  | 0.2 | - | - | 0.1 |




## LANE LEVEL OF SERVICE

Lane Level of Service
$\forall$ Site: 3 [2026 No Action - PM Peak Hour (Site Folder: 19th Ave
NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.2.202
19th Ave NE / 172nd St NE
Site Category: 2026 No Action - PM Peak Hour
Roundabout

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| LOS | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used).
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\square$ Site: 3 [2026 No Action - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202
19th Ave NE / 172nd St NE
Site Category: 2026 No Action - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{gathered} \text { land } \\ \text { lows } \\ \mathrm{HV} \text { ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { rival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service |  | ck Of e Dist ] ft | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> mph |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 1 | 0.8 | 1 | 0.8 | 0.486 | 10.1 | LOS B | 3.4 | 85.4 | 0.13 | 0.38 | 0.13 | 31.7 |
| 6 | T1 | All MCs | 620 | 0.8 | 620 | 0.8 | 0.486 | 3.7 | LOS A | 3.4 | 85.4 | 0.13 | 0.38 | 0.13 | 32.2 |
| 16 | R2 | All MCs | 29 | 0.8 | 29 | 0.8 | 0.486 | 3.7 | LOS A | 3.4 | 85.4 | 0.13 | 0.38 | 0.13 | 32.0 |
| Appr |  |  | 651 | 0.8 | 651 | 0.8 | 0.486 | 3.8 | LOS A | 3.4 | 85.4 | 0.13 | 0.38 | 0.13 | 32.2 |
| North: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 11 | 0.0 | 11 | 0.0 | 0.048 | 8.4 | LOS A | 0.2 | 5.9 | 0.57 | 0.59 | 0.57 | 23.3 |
| 14 | R2 | All MCs | 32 | 0.0 | 32 | 0.0 | 0.048 | 4.7 | LOS A | 0.2 | 5.9 | 0.57 | 0.59 | 0.57 | 23.4 |
| Approach |  |  | 42 | 0.0 | 42 | 0.0 | 0.048 | 5.6 | LOS A | 0.2 | 5.9 | 0.57 | 0.59 | 0.57 | 23.4 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | U | All MCs | 1 | 2.0 | 1 | 2.0 | 0.289 | 10.0 | LOS B | 1.8 | 44.9 | 0.09 | 0.39 | 0.09 | 31.7 |
| 5 | L2 | All MCs | 16 | 2.0 | 16 | 2.0 | 0.289 | 8.1 | LOS A | 1.8 | 44.9 | 0.09 | 0.39 | 0.09 | 31.7 |
| 2 | T1 | All MCs | 366 | 2.0 | 366 | 2.0 | 0.289 | 3.7 | LOS A | 1.8 | 44.9 | 0.09 | 0.39 | 0.09 | 32.2 |
| Approach |  |  | 384 | 2.0 | 384 | 2.0 | 0.289 | 3.9 | LOS A | 1.8 | 44.9 | 0.09 | 0.39 | 0.09 | 32.2 |
| All Vehicles |  |  | 1076 | 1.2 | 1076 |  | 0.486 | 3.9 | LOS A | 3.4 | 85.4 | 0.13 | 0.39 | 0.13 | 31.8 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

## LANE LEVEL OF SERVICE

Lane Level of Service
$\square$ Site: 4 [2026 No Action - PM Peak Hour (Site Folder: 23rd Ave
NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.2.202
23rd Ave NE / 172nd St NE
Site Category: 2026 No Action - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used).
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## - Site: 4 [2026 No Action - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.2.202
23rd Ave NE / 172nd St NE
Site Category: 2026 No Action - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{gathered} \text { land } \\ \text { lows } \\ \mathrm{HV} \text { ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { rrival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | ck Of e Dist ] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed <br> mph |
| South: Private Dwy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.009 | 9.2 | LOS A | 0.1 | 1.4 | 0.71 | 0.53 | 0.71 | 23.4 |
| 8 | T1 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.009 | 4.2 | LOS A | 0.1 | 1.4 | 0.71 | 0.53 | 0.71 | 23.6 |
| 18 | R2 | All MCs | 5 | 0.0 | 5 | 0.0 | 0.009 | 4.9 | LOS A | 0.1 | 1.4 | 0.71 | 0.53 | 0.71 | 23.5 |
| Approach |  |  | 7 | 0.0 | 7 | 0.0 | 0.009 | 5.4 | LOS A | 0.1 | 1.4 | 0.71 | 0.53 | 0.71 | 23.5 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1u | U | All MCs | 34 | 1.6 | 34 | 1.6 | 0.462 | 11.0 | LOS B | 3.8 | 96.6 | 0.20 | 0.34 | 0.20 | 31.9 |
| 1 | L2 | All MCs | 1 | 1.6 | 1 | 1.6 | 0.462 | 8.7 | LOS A | 3.8 | 96.6 | 0.20 | 0.34 | 0.20 | 31.9 |
| 6 | T1 | All MCs | 743 | 1.6 | 743 | 1.6 | 0.462 | 3.2 | LOS A | 3.8 | 96.6 | 0.20 | 0.34 | 0.20 | 32.4 |
| 16 | R2 | All MCs | 212 | 1.6 | 212 | 1.6 | 0.172 | 3.6 | LOS A | 1.0 | 24.5 | 0.17 | 0.41 | 0.17 | 32.2 |
| Approach |  |  | 989 | 1.6 | 989 | 1.6 | 0.462 | 3.5 | LOS A | 3.8 | 96.6 | 0.20 | 0.35 | 0.20 | 32.3 |
| North: 23rd Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 190 | 2.2 | 190 | 2.2 | 0.261 | 9.9 | LOS A | 1.6 | 40.4 | 0.73 | 0.70 | 0.73 | 22.6 |
| 4 | T1 | All MCs | 3 | 2.2 | 3 | 2.2 | 0.261 | 4.6 | LOS A | 1.6 | 40.4 | 0.73 | 0.70 | 0.73 | 22.7 |
| 14 | R2 | All MCs | 20 | 2.2 | 20 | 2.2 | 0.261 | 5.7 | LOS A | 1.6 | 40.4 | 0.73 | 0.70 | 0.73 | 22.7 |
| Approach |  |  | 214 | 2.2 | 214 | 2.2 | 0.261 | 9.4 | LOS A | 1.6 | 40.4 | 0.73 | 0.70 | 0.73 | 22.6 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 2 | 2.5 | 2 | 2.5 | 0.484 | 12.1 | LOS B | 3.5 | 90.2 | 0.54 | 0.45 | 0.54 | 31.1 |
| 5 | L2 | All MCs | 32 | 2.5 | 32 | 2.5 | 0.484 | 9.9 | LOS A | 3.5 | 90.2 | 0.54 | 0.45 | 0.54 | 31.1 |
| 2 | T1 | All MCs | 550 | 2.5 | 550 | 2.5 | 0.484 | 3.9 | LOS A | 3.5 | 90.2 | 0.54 | 0.45 | 0.54 | 31.7 |
| 12 | R2 | All MCs | 1 | 2.5 | 1 | 2.5 | 0.484 | 4.2 | LOS A | 3.5 | 90.2 | 0.54 | 0.45 | 0.54 | 31.5 |
| Approach |  |  | 585 | 2.5 | 585 | 2.5 | 0.484 | 4.3 | LOS A | 3.5 | 90.2 | 0.54 | 0.45 | 0.54 | 31.7 |
| All Vehicles |  |  | 1796 | 2.0 | 1796 | 2.0 | 0.484 | 4.5 | LOS A | 3.8 | 96.6 | 0.38 | 0.43 | 0.38 | 30.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {¢ }}$ |  | 4 | 中4 | 「 | \％ | 4 | 「＇ | \％ | $\uparrow$ |  |
| Traffic Volume（vph） | 33 | 479 | 135 | 810 | 663 | 279 | 207 | 100 | 700 | 358 | 110 | 32 |
| Future Volume（vph） | 33 | 479 | 135 | 810 | 663 | 279 | 207 | 100 | 700 | 358 | 110 | 32 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 250 |  | 0 | 425 |  | 200 | 125 |  | 0 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 2 |  | 1 | 1 |  | 1 | 2 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 25 |  |  | 25 |  |
| Link Distance（ft） |  | 394 |  |  | 613 |  |  | 444 |  |  | 470 |  |
| Travel Time（s） |  | 7.7 |  |  | 11.9 |  |  | 12.1 |  |  | 12.8 |  |
| Confl．Peds．（\＃／hr） | 1 |  |  |  |  | 1 | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Turn Type | Prot | NA |  | Prot | NA | Perm | Prot | NA | pt＋ov | Prot | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 81 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  | 6 |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 | 6 | 3 | 8 | 81 | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 7.0 |  | 3.0 | 7.0 | 7.0 | 3.0 | 5.0 |  | 3.0 | 5.0 |  |
| Minimum Split（s） | 9.0 | 38.0 |  | 9.0 | 38.0 | 38.0 | 9.0 | 11.0 |  | 9.0 | 46.0 |  |
| Total Split（s） | 20.0 | 40.0 |  | 40.0 | 60.0 | 60.0 | 35.0 | 15.0 |  | 35.0 | 15.0 |  |
| Total Split（\％） | 15．4\％ | 30．8\％ |  | 30．8\％ | 46．2\％ | 46．2\％ | 26．9\％ | 11．5\％ |  | 26．9\％ | 11．5\％ |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／Lag | Lead | Lead |  | Lag | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | Min |  | C－Min | C－Min | C－Min | None | None |  | Min | Min |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 75 （58\％），Referenced to phase 1：WBL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 145 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：$\quad$ 5：27th Ave NE／Spring Ln Ave \＆172nd St NE


HCM 6th Signalized Intersection Summary
5: 27th Ave NE/Spring Ln Ave \& 172nd St NE

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Notes
User approved pedestrian interval to be less than phase max green.

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | \％ | （ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 44 | 「 |  |  |  | ${ }^{*}$ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 0 | 1130 | 495 | 0 | 1467 | 633 | 0 | 0 | 0 | 320 | 0 | 303 |
| Future Volume（vph） | 0 | 1130 | 495 | 0 | 1467 | 633 | 0 | 0 | 0 | 320 | 0 | 303 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 3\％ |  |  | －3\％ |  |  | 0\％ |  |  | 3\％ |  |
| Storage Length（ft） | 0 |  | 250 | 0 |  | 0 | 0 |  | 0 | 400 |  | 400 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 0 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 613 |  |  | 915 |  |  | 299 |  |  | 608 |  |
| Travel Time（s） |  | 11.9 |  |  | 17.8 |  |  | 6.8 |  |  | 13.8 |  |
| Confl．Peds．（\＃／hr） | 11 |  |  |  |  | 11 | 1 |  |  |  |  | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 1\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ | 4\％ | 4\％ | 4\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 50\％ |  |  |
| Turn Type |  | NA | Perm |  | NA | Perm |  |  |  | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  |  |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  |  |  |  | 4 |
| Detector Phase |  | 2 | 2 |  | 6 | 6 |  |  |  | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  |  | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） |  | 24.8 | 24.8 |  | 34.1 | 34.1 |  |  |  | 33.8 | 33.8 | 33.8 |
| Total Split（s） |  | 90.0 | 90.0 |  | 40.0 | 40.0 |  |  |  | 40.0 | 40.0 | 40.0 |
| Total Split（\％） |  | 69．2\％ | 69．2\％ |  | 30．8\％ | 30．8\％ |  |  |  | 30．8\％ | 30．8\％ | 30．8\％ |
| Yellow Time（s） |  | 3.8 | 3.8 |  | 4.1 | 4.1 |  |  |  | 3.8 | 3.8 | 3.8 |
| All－Red Time（s） |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 5.8 | 5.8 |  | 6.1 | 6.1 |  |  |  | 5.8 | 5.8 | 5.8 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode |  | C－Min | C－Min |  | C－Min | C－Min |  |  |  | None | None | None |

## Intersection Summary

## Area Type：

Cycle Length： 130
Actuated Cycle Length： 130
Offset： 0 （0\％），Referenced to phase 2：EBT and 6：WBT，Start of Red
Natural Cycle： 75
Control Type：Actuated－Coordinated
Splits and Phases：6：I－5 SB Ramp \＆172nd St NE


|  | $\rangle$ | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 |  | \％ |  | $\frac{1}{*}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 性 | 「 |  |  |  | ＊ | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 0 | 1130 | 495 | 0 | 1467 | 633 | 0 | 0 | 0 | 320 | 0 | 303 |
| Future Volume（veh／h） | 0 | 1130 | 495 | 0 | 1467 | 633 | 0 | 0 | 0 | 320 | 0 | 303 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 0 | 1832 | 1832 | 0 | 1988 | 1988 |  |  |  | 1788 | 1788 | 1788 |
| Adj Flow Rate，veh／h | 0 | 1165 | 0 | 0 | 1512 | 0 |  |  |  | 330 | 0 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |  |  |  | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 1 | 1 | 0 | 2 | 2 |  |  |  | 4 | 4 | 4 |
| Cap，veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 432 | 0 |  |
| Arrive On Green | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 |  |  |  | 0.13 | 0.00 | 0.00 |
| Sat Flow，veh／h | 0 | 3573 | 1553 | 0 | 3877 | 1685 |  |  |  | 3405 | 0 | 1515 |
| Grp Volume（v），veh／h | 0 | 1165 | 0 | 0 | 1512 | 0 |  |  |  | 330 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1741 | 1553 | 0 | 1889 | 1685 |  |  |  | 1703 | 0 | 1515 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 12.2 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 12.2 | 0.0 | 0.0 |
| Prop In Lane | 0.00 |  | 1.00 | 0.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 432 | 0 |  |
| V／C Ratio（X） | 0.00 | 0.43 |  | 0.00 | 0.51 |  |  |  |  | 0.76 | 0.00 |  |
| Avail Cap（c＿a），veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 896 | 0 |  |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 2.00 | 2.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.47 | 0.00 | 0.00 | 0.58 | 0.00 |  |  |  | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 54.9 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 4.8 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 |  |  |  | 5.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 59.7 | 0.0 | 0.0 |
| LnGrp LOS | A | A |  | A | A |  |  |  |  | E | A |  |
| Approach Vol，veh／h |  | 1165 |  |  | 1512 |  |  |  |  |  | 330 |  |
| Approach Delay，s／veh |  | 0.2 |  |  | 0.4 |  |  |  |  |  | 59.7 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | E |  |
| Timer－Assigned Phs |  | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 107.7 |  | 22.3 |  | 107.7 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），s |  | ＊ 6.1 |  | ＊ 5.8 |  | 6.1 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | ＊ 84 |  | ＊ 34 |  | 33.9 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 14.2 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 18.4 |  | 2.1 |  | 19.6 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［EBR，WBR，SBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 44 |  |  | 來4 | F' | \% | $\uparrow$ | 「 |  |  |  |
| Traffic Volume (vph) | 358 | 1066 | 0 | 0 | 1440 | 535 | 648 | 2 | 822 | 0 | 0 | 0 |
| Future Volume (vph) | 358 | 1066 | 0 | 0 | 1440 | 535 | 648 | 2 | 822 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 6\% |  |  | 5\% |  |  | 0\% |  |
| Storage Length (ft) | 600 |  | 0 | 0 |  | 300 | 400 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 915 |  |  | 978 |  |  | 589 |  |  | 234 |  |
| Travel Time (s) |  | 17.8 |  |  | 19.1 |  |  | 13.4 |  |  | 5.3 |  |
| Confl. Peds. (\#/hr) | 8 |  | 11 | 11 |  | 8 |  |  | 4 | 4 |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  | 50\% |  |  |  |  |  |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Split | NA | Perm |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 | 8 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  | 6 |  |  | 8 |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 | 6 | 8 | 8 | 8 |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  |  | 7.0 | 7.0 | 5.0 | 5.0 | 5.0 |  |  |  |
| Minimum Split (s) | 10.6 | 24.1 |  |  | 23.8 | 23.8 | 40.8 | 40.8 | 40.8 |  |  |  |
| Total Split (s) | 40.0 | 89.0 |  |  | 49.0 | 49.0 | 41.0 | 41.0 | 41.0 |  |  |  |
| Total Split (\%) | 30.8\% | 68.5\% |  |  | 37.7\% | 37.7\% | 31.5\% | 31.5\% | 31.5\% |  |  |  |
| Yellow Time (s) | 3.6 | 4.1 |  |  | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |  |  |
| All-Red Time (s) | 2.0 | 2.0 |  |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Total Lost Time (s) | 5.6 | 6.1 |  |  | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |  |  |  |
| Lead/Lag | Lead |  |  |  | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  |  | Yes | Yes |  |  |  |  |  |  |
| Recall Mode | None | C-Min |  |  | C-Min | C-Min | None | None | None |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL and 6:WBT, Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 7: I-5 NB Ramps \& 172nd St NE


HCM 6th Signalized Intersection Summary
7：I－5 NB Ramps \＆172nd St NE

|  | 4 | $\rightarrow$ | 7 | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 44 |  |  | 种4 | 「 | ${ }^{1}$ | $\uparrow$ | 「 |  |  |  |
| Trafic Volume（veh／h） | 358 | 1066 | 0 | 0 | 1440 | 535 | 648 | 2 | 822 | 0 | 0 | 0 |
| Future Volume（veh／h） | 358 | 1066 | 0 | 0 | 1440 | 535 | 648 | 2 | 822 | 0 | 0 | 0 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 0 | 0 | 1658 | 1658 | 1723 | 1723 | 1723 |  |  |  |
| Adj Flow Rate，veh／h | 365 | 1088 | 0 | 0 | 1469 | 0 | 662 | 0 | 0 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |  |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 0 | 0 | 2 | 2 | 2 | 2 | 2 |  |  |  |
| Cap，veh／h | 389 | 2399 | 0 | 0 | 2244 |  | 766 | 0 |  |  |  |  |
| Arrive On Green | 0.27 | 1.00 | 0.00 | 0.00 | 0.50 | 0.00 | 0.23 | 0.00 | 0.00 |  |  |  |
| Sat Flow，veh／h | 1781 | 3647 | 0 | 0 | 4676 | 1405 | 3282 | 0 | 1460 |  |  |  |
| Grp Volume（v），veh／h | 365 | 1088 | 0 | 0 | 1469 | 0 | 662 | 0 | 0 |  |  |  |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 0 | 0 | 1509 | 1405 | 1641 | 0 | 1460 |  |  |  |
| Q Serve（g＿s），s | 14.7 | 0.0 | 0.0 | 0.0 | 31.5 | 0.0 | 25.2 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear（g＿c），s | 14.7 | 0.0 | 0.0 | 0.0 | 31.5 | 0.0 | 25.2 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 1.00 |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 389 | 2399 | 0 | 0 | 2244 |  | 766 | 0 |  |  |  |  |
| V／C Ratio（X） | 0.94 | 0.45 | 0.00 | 0.00 | 0.65 |  | 0.86 | 0.00 |  |  |  |  |
| Avail Cap（c＿a），veh／h | 618 | 2399 | 0 | 0 | 2244 |  | 889 | 0 |  |  |  |  |
| HCM Platoon Ratio | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter（l） | 0.87 | 0.87 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |  |  |
| Uniform Delay（d），s／veh | 20.7 | 0.0 | 0.0 | 0.0 | 24.5 | 0.0 | 47.8 | 0.0 | 0.0 |  |  |  |
| Incr Delay（d2），s／veh | 14.3 | 0.5 | 0.0 | 0.0 | 1.5 | 0.0 | 8.9 | 0.0 | 0.0 |  |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \％ile BackOfQ（50\％），veh／ln | 6.3 | 0.2 | 0.0 | 0.0 | 11.3 | 0.0 | 11.2 | 0.0 | 0.0 |  |  |  |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 35.0 | 0.5 | 0.0 | 0.0 | 26.0 | 0.0 | 56.7 | 0.0 | 0.0 |  |  |  |
| LnGrp LOS | C | A | A | A | C |  | E | A |  |  |  |  |
| Approach Vol，veh／h |  | 1453 |  |  | 1469 |  |  | 662 |  |  |  |  |
| Approach Delay，s／veh |  | 9.2 |  |  | 26.0 |  |  | 56.7 |  |  |  |  |
| Approach LOS |  | A |  |  | C |  |  | E |  |  |  |  |
| Timer－Assigned Phs |  | 2 |  |  | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ |  | 93.9 |  |  | 23.3 | 70.5 |  | 36.1 |  |  |  |  |
| Change Period（Y＋Rc），s |  | 6.1 |  |  | 5.6 | ＊ 6.1 |  | 5.8 |  |  |  |  |
| Max Green Setting（Gmax），s |  | 82.9 |  |  | 34.4 | ＊ 43 |  | 35.2 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  |  | 16.7 | 33.5 |  | 27.2 |  |  |  |  |
| Green Ext Time（p＿c），s |  | 16.3 |  |  | 1.0 | 7.5 |  | 2.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 24.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

|  | $\Rightarrow$ |  |  | $\checkmark$ | $\leftarrow$ |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  | \% | $\hat{1}$ |  |  | * |  |  | \& |  |
| Trafic Volume (vph) | 2 | 244 | 1 | 63 | 401 | 15 | 5 | 1 | 40 | 8 | 1 | 5 |
| Future Volume (vph) | 2 | 244 | 1 | 63 | 401 | 15 | 5 | 1 | 40 | 8 | 1 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 5\% |  |  | -4\% |  |
| Storage Length (tt) | 0 |  | 0 | 175 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 35 |  |  | 25 |  |  | 25 |  |  | 25 |  |
| Link Distance (ft) |  | 369 |  |  | 1809 |  |  | 529 |  |  | 387 |  |
| Travel Time (s) |  | 7.2 |  |  | 49.3 |  |  | 14.4 |  |  | 10.6 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |







## LANE LEVEL OF SERVICE

## Lane Level of Service

$\forall$ Site: 3 [2026 With Project - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2026 With Project - PM Peak Hour
Roundabout

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| LOS | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used).
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\nabla$ Site: 3 [2026 With Project - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2026 With Project - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{aligned} & \text { land } \\ & \text { lows } \\ & \mathrm{HV} \text { ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { rrival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{array}$ | ck Of ue Dist ] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 1 | 0.8 | 1 | 0.8 | 0.542 | 10.3 | LOS B | 4.3 | 108.5 | 0.23 | 0.39 | 0.23 | 31.5 |
| 6 | T1 | All MCs | 620 | 0.8 | 620 | 0.8 | 0.542 | 3.9 | LOS A | 4.3 | 108.5 | 0.23 | 0.39 | 0.23 | 32.0 |
| 16 | R2 | All MCs | 92 | 0.8 | 92 | 0.8 | 0.542 | 3.9 | LOS A | 4.3 | 108.5 | 0.23 | 0.39 | 0.23 | 31.8 |
| Appr |  |  | 713 | 0.8 | 713 | 0.8 | 0.542 | 4.0 | LOS A | 4.3 | 108.5 | 0.23 | 0.39 | 0.23 | 32.0 |
| North: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 54 | 0.0 | 54 | 0.0 | 0.115 | 8.6 | LOS A | 0.6 | 15.1 | 0.60 | 0.64 | 0.60 | 23.0 |
| 14 | R2 | All MCs | 46 | 0.0 | 46 | 0.0 | 0.115 | 4.9 | LOS A | 0.6 | 15.1 | 0.60 | 0.64 | 0.60 | 23.1 |
| Approach |  |  | 100 | 0.0 | 100 | 0.0 | 0.115 | 6.9 | LOS A | 0.6 | 15.1 | 0.60 | 0.64 | 0.60 | 23.0 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 1 | 2.0 | 1 | 2.0 | 0.317 | 10.3 | LOS B | 2.0 | 50.9 | 0.23 | 0.42 | 0.23 | 31.3 |
| 5 | L2 | All MCs | 36 | 2.0 | 36 | 2.0 | 0.317 | 8.4 | LOS A | 2.0 | 50.9 | 0.23 | 0.42 | 0.23 | 31.3 |
| 2 | T1 | All MCs | 366 | 2.0 | 366 | 2.0 | 0.317 | 4.0 | LOS A | 2.0 | 50.9 | 0.23 | 0.42 | 0.23 | 31.8 |
| Approach |  |  | 404 | 2.0 | 404 | 2.0 | 0.317 | 4.4 | LOS A | 2.0 | 50.9 | 0.23 | 0.42 | 0.23 | 31.8 |
| All Vehicles |  |  | 1216 | 1.1 | 1216 | 1.1 | 0.542 | 4.3 | LOS A | 4.3 | 108.5 | 0.26 | 0.42 | 0.26 | 30.9 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2022 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: TENW | Licence: PLUS / 1PC | Processed: Friday, July 7, 2023 10:47:21 AM
Project: T:\Active Projects\English Crossing (Marysville) - 2023-012\Planning\LOS\English Crossing.sip9

## LANE LEVEL OF SERVICE

## Lane Level of Service

$\forall$ Site: 4 [2026 With Project - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2026 With Project - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | B | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used). Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\checkmark$ Site: 4 [2026 With Project - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2026 With Project - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{aligned} & \text { land } \\ & \text { lows } \\ & \mathrm{HV} \text { ] } \\ & \% \end{aligned}$ |  | rival ows HV ] \% | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | ck Of ue Dist $]$ ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed <br> mph |
| South: Private Dwy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.010 | 9.5 | LOS A | 0.1 | 1.5 | 0.74 | 0.54 | 0.74 | 23.3 |
| 8 | T1 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.010 | 4.5 | LOS A | 0.1 | 1.5 | 0.74 | 0.54 | 0.74 | 23.5 |
| 18 | R2 | All MCs | 5 | 0.0 | 5 | 0.0 | 0.010 | 5.3 | LOS A | 0.1 | 1.5 | 0.74 | 0.54 | 0.74 | 23.4 |
| Approach |  |  | 7 | 0.0 | 7 | 0.0 | 0.010 | 5.8 | LOS A | 0.1 | 1.5 | 0.74 | 0.54 | 0.74 | 23.4 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 34 | 1.6 | 34 | 1.6 | 0.495 | 11.0 | LOS B | 4.3 | 109.7 | 0.22 | 0.33 | 0.22 | 31.8 |
| 1 | L2 | All MCs | 1 | 1.6 | 1 | 1.6 | 0.495 | 8.8 | LOS A | 4.3 | 109.7 | 0.22 | 0.33 | 0.22 | 31.8 |
| 6 | T1 | All MCs | 799 | 1.6 | 799 | 1.6 | 0.495 | 3.2 | LOS A | 4.3 | 109.7 | 0.22 | 0.33 | 0.22 | 32.4 |
| 16 | R2 | All MCs | 212 | 1.6 | 212 | 1.6 | 0.175 | 3.6 | LOS A | 1.0 | 25.1 | 0.17 | 0.41 | 0.17 | 32.2 |
| Approach |  |  | 1046 | 1.6 | 1046 | 1.6 | 0.495 | 3.5 | LOS A | 4.3 | 109.7 | 0.21 | 0.35 | 0.21 | 32.3 |
| North: 23rd Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 190 | 2.2 | 190 | 2.2 | 0.276 | 10.5 | LOS B | 1.7 | 43.9 | 0.77 | 0.72 | 0.77 | 22.4 |
| 4 | T1 | All MCs | 3 | 2.2 | 3 | 2.2 | 0.276 | 5.2 | LOS A | 1.7 | 43.9 | 0.77 | 0.72 | 0.77 | 22.6 |
| 14 | R2 | All MCs | 20 | 2.2 | 20 | 2.2 | 0.276 | 6.3 | LOS A | 1.7 | 43.9 | 0.77 | 0.72 | 0.77 | 22.5 |
| Approach |  |  | 214 | 2.2 | 214 | 2.2 | 0.276 | 10.1 | LOS B | 1.7 | 43.9 | 0.77 | 0.72 | 0.77 | 22.4 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 2 | 2.5 | 2 | 2.5 | 0.518 | 12.2 | LOS B | 4.0 | 101.0 | 0.57 | 0.46 | 0.57 | 31.1 |
| 5 | L2 | All MCs | 32 | 2.5 | 32 | 2.5 | 0.518 | 10.0 | LOS A | 4.0 | 101.0 | 0.57 | 0.46 | 0.57 | 31.1 |
| 2 | T1 | All MCs | 589 | 2.5 | 589 | 2.5 | 0.518 | 4.0 | LOS A | 4.0 | 101.0 | 0.57 | 0.46 | 0.57 | 31.7 |
| 12 | R2 | All MCs | 1 | 2.5 | 1 | 2.5 | 0.518 | 4.3 | LOS A | 4.0 | 101.0 | 0.57 | 0.46 | 0.57 | 31.4 |
| Approach |  |  | 624 | 2.5 | 624 | 2.5 | 0.518 | 4.3 | LOS A | 4.0 | 101.0 | 0.57 | 0.46 | 0.57 | 31.6 |
| All Vehicles |  |  | 1891 | 2.0 | 1891 | 2.0 | 0.518 | 4.5 | LOS A | 4.3 | 109.7 | 0.39 | 0.43 | 0.39 | 30.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {¢ }}$ |  | 4 | 44 | 「 | \％ | 4 | 「＇ | \％ | $\uparrow$ |  |
| Traffic Volume（vph） | 33 | 513 | 138 | 810 | 712 | 279 | 211 | 100 | 700 | 358 | 110 | 32 |
| Future Volume（vph） | 33 | 513 | 138 | 810 | 712 | 279 | 211 | 100 | 700 | 358 | 110 | 32 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 250 |  | 0 | 425 |  | 200 | 125 |  | 0 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 2 |  | 1 | 1 |  | 1 | 2 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 25 |  |  | 25 |  |
| Link Distance（ft） |  | 394 |  |  | 613 |  |  | 444 |  |  | 470 |  |
| Travel Time（s） |  | 7.7 |  |  | 11.9 |  |  | 12.1 |  |  | 12.8 |  |
| Confl．Peds．（\＃／hr） | 1 |  |  |  |  | 1 | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Turn Type | Prot | NA |  | Prot | NA | Perm | Prot | NA | pt＋ov | Prot | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 81 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  | 6 |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 | 6 | 3 | 8 | 81 | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 7.0 |  | 3.0 | 7.0 | 7.0 | 3.0 | 5.0 |  | 3.0 | 5.0 |  |
| Minimum Split（s） | 9.0 | 38.0 |  | 9.0 | 38.0 | 38.0 | 9.0 | 11.0 |  | 9.0 | 46.0 |  |
| Total Split（s） | 20.0 | 40.0 |  | 40.0 | 60.0 | 60.0 | 35.0 | 15.0 |  | 35.0 | 15.0 |  |
| Total Split（\％） | 15．4\％ | 30．8\％ |  | 30．8\％ | 46．2\％ | 46．2\％ | 26．9\％ | 11．5\％ |  | 26．9\％ | 11．5\％ |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／Lag | Lead | Lead |  | Lag | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | Min |  | C－Min | C－Min | C－Min | None | None |  | Min | Min |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 75 （58\％），Referenced to phase 1：WBL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 145 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：$\quad$ 5：27th Ave NE／Spring Ln Ave \＆172nd St NE


HCM 6th Signalized Intersection Summary
5: 27th Ave NE/Spring Ln Ave \& 172nd St NE

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Notes
User approved pedestrian interval to be less than phase max green.

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | \％ | （ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 44 | 「 |  |  |  | ${ }^{*}$ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 0 | 1149 | 510 | 0 | 1506 | 633 | 0 | 0 | 0 | 320 | 0 | 313 |
| Future Volume（vph） | 0 | 1149 | 510 | 0 | 1506 | 633 | 0 | 0 | 0 | 320 | 0 | 313 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 3\％ |  |  | －3\％ |  |  | 0\％ |  |  | 3\％ |  |
| Storage Length（ft） | 0 |  | 250 | 0 |  | 0 | 0 |  | 0 | 400 |  | 400 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 0 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 613 |  |  | 915 |  |  | 299 |  |  | 608 |  |
| Travel Time（s） |  | 11.9 |  |  | 17.8 |  |  | 6.8 |  |  | 13.8 |  |
| Confl．Peds．（\＃／hr） | 11 |  |  |  |  | 11 | 1 |  |  |  |  | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 1\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ | 4\％ | 4\％ | 4\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 50\％ |  |  |
| Turn Type |  | NA | Perm |  | NA | Perm |  |  |  | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  |  |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  |  |  |  | 4 |
| Detector Phase |  | 2 | 2 |  | 6 | 6 |  |  |  | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  |  | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） |  | 24.8 | 24.8 |  | 34.1 | 34.1 |  |  |  | 33.8 | 33.8 | 33.8 |
| Total Split（s） |  | 90.0 | 90.0 |  | 40.0 | 40.0 |  |  |  | 40.0 | 40.0 | 40.0 |
| Total Split（\％） |  | 69．2\％ | 69．2\％ |  | 30．8\％ | 30．8\％ |  |  |  | 30．8\％ | 30．8\％ | 30．8\％ |
| Yellow Time（s） |  | 3.8 | 3.8 |  | 4.1 | 4.1 |  |  |  | 3.8 | 3.8 | 3.8 |
| All－Red Time（s） |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 5.8 | 5.8 |  | 6.1 | 6.1 |  |  |  | 5.8 | 5.8 | 5.8 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode |  | C－Min | C－Min |  | C－Min | C－Min |  |  |  | None | None | None |

## Intersection Summary

## Area Type：

Other
Cycle Length： 130
Actuated Cycle Length： 130
Offset： 0 （0\％），Referenced to phase 2：EBT and 6：WBT，Start of Red
Natural Cycle： 75
Control Type：Actuated－Coordinated
Splits and Phases：6：I－5 SB Ramp \＆172nd St NE


|  | 4 | $\rightarrow$ |  | 7 |  |  |  |  |  |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 中4 | 「 |  | 44 | 「 |  |  |  | ${ }^{*}$ | 4 | 「 |
| Traffic Volume（veh／h） | 0 | 1149 | 510 | 0 | 1506 | 633 | 0 | 0 | 0 | 320 | 0 | 313 |
| Future Volume（veh／h） | 0 | 1149 | 510 | 0 | 1506 | 633 | 0 | 0 | 0 | 320 | 0 | 313 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 0 | 1832 | 1832 | 0 | 1988 | 1988 |  |  |  | 1788 | 1788 | 1788 |
| Adj Flow Rate，veh／h | 0 | 1185 | 0 | 0 | 1553 | 0 |  |  |  | 330 | 0 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |  |  |  | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 1 | 1 | 0 | 2 | 2 |  |  |  | 4 | 4 | 4 |
| Cap，veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 432 | 0 |  |
| Arrive On Green | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 |  |  |  | 0.13 | 0.00 | 0.00 |
| Sat Flow，veh／h | 0 | 3573 | 1553 | 0 | 3877 | 1685 |  |  |  | 3405 | 0 | 1515 |
| Grp Volume（v），veh／h | 0 | 1185 | 0 | 0 | 1553 | 0 |  |  |  | 330 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1741 | 1553 | 0 | 1889 | 1685 |  |  |  | 1703 | 0 | 1515 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 12.2 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 12.2 | 0.0 | 0.0 |
| Prop In Lane | 0.00 |  | 1.00 | 0.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 432 | 0 |  |
| V／C Ratio（X） | 0.00 | 0.44 |  | 0.00 | 0.53 |  |  |  |  | 0.76 | 0.00 |  |
| Avail Cap（c＿a），veh／h | 0 | 2721 |  | 0 | 2952 |  |  |  |  | 896 | 0 |  |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 2.00 | 2.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.45 | 0.00 | 0.00 | 0.55 | 0.00 |  |  |  | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 54.9 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 4.8 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 |  |  |  | 5.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 |  |  |  | 59.7 | 0.0 | 0.0 |
| LnGrp LOS | A | A |  | A | A |  |  |  |  | E | A |  |
| Approach Vol，veh／h |  | 1185 |  |  | 1553 |  |  |  |  |  | 330 |  |
| Approach Delay，s／veh |  | 0.2 |  |  | 0.4 |  |  |  |  |  | 59.7 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | E |  |
| Timer－Assigned Phs |  | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ |  | 107.7 |  | 22.3 |  | 107.7 |  |  |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s |  | ＊ 6.1 |  | ＊ 5.8 |  | 6.1 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | ＊ 84 |  | ＊ 34 |  | 33.9 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c +11 ），s |  | 2.0 |  | 14.2 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 19.0 |  | 2.1 |  | 20.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.7 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［EBR，WBR，SBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 44 |  |  | 來4 | F' | \% | $\uparrow$ | 「 |  |  |  |
| Traffic Volume (vph) | 365 | 1078 | 0 | 0 | 1457 | 535 | 670 | 2 | 822 | 0 | 0 | 0 |
| Future Volume (vph) | 365 | 1078 | 0 | 0 | 1457 | 535 | 670 | 2 | 822 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 6\% |  |  | 5\% |  |  | 0\% |  |
| Storage Length (ft) | 600 |  | 0 | 0 |  | 300 | 400 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 915 |  |  | 978 |  |  | 589 |  |  | 234 |  |
| Travel Time (s) |  | 17.8 |  |  | 19.1 |  |  | 13.4 |  |  | 5.3 |  |
| Confl. Peds. (\#/hr) | 8 |  | 11 | 11 |  | 8 |  |  | 4 | 4 |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  | 50\% |  |  |  |  |  |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Split | NA | Perm |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 | 8 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  | 6 |  |  | 8 |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 | 6 | 8 | 8 | 8 |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  |  | 7.0 | 7.0 | 5.0 | 5.0 | 5.0 |  |  |  |
| Minimum Split (s) | 10.6 | 24.1 |  |  | 23.8 | 23.8 | 40.8 | 40.8 | 40.8 |  |  |  |
| Total Split (s) | 40.0 | 89.0 |  |  | 49.0 | 49.0 | 41.0 | 41.0 | 41.0 |  |  |  |
| Total Split (\%) | 30.8\% | 68.5\% |  |  | 37.7\% | 37.7\% | 31.5\% | 31.5\% | 31.5\% |  |  |  |
| Yellow Time (s) | 3.6 | 4.1 |  |  | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |  |  |
| All-Red Time (s) | 2.0 | 2.0 |  |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Total Lost Time (s) | 5.6 | 6.1 |  |  | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |  |  |  |
| Lead/Lag | Lead |  |  |  | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  |  | Yes | Yes |  |  |  |  |  |  |
| Recall Mode | None | C-Min |  |  | C-Min | C-Min | None | None | None |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL and 6:WBT, Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 7: I-5 NB Ramps \& 172nd St NE


|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | \％ |  | 1 | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 44 |  |  | 坐乐 | 「 | ＊ | $\uparrow$ | 「 |  |  |  |
| Traffic Volume（veh／h） | 365 | 1078 | 0 | 0 | 1457 | 535 | 670 | 2 | 822 | 0 | 0 | 0 |
| Future Volume（veh／h） | 365 | 1078 | 0 | 0 | 1457 | 535 | 670 | 2 | 822 | 0 | 0 | 0 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 0 | 0 | 1658 | 1658 | 1723 | 1723 | 1723 |  |  |  |
| Adj Flow Rate，veh／h | 372 | 1100 | 0 | 0 | 1487 | 0 | 685 | 0 | 0 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |  |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 0 | 0 | 2 | 2 | 2 | 2 | 2 |  |  |  |
| Cap，veh／h | 396 | 2379 | 0 | 0 | 2173 |  | 784 | 0 |  |  |  |  |
| Arrive On Green | 0.29 | 1.00 | 0.00 | 0.00 | 0.48 | 0.00 | 0.24 | 0.00 | 0.00 |  |  |  |
| Sat Flow，veh／h | 1781 | 3647 | 0 | 0 | 4676 | 1405 | 3282 | 0 | 1460 |  |  |  |
| Grp Volume（v），veh／h | 372 | 1100 | 0 | 0 | 1487 | 0 | 685 | 0 | 0 |  |  |  |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 0 | 0 | 1509 | 1405 | 1641 | 0 | 1460 |  |  |  |
| Q Serve（g＿s），s | 16.0 | 0.0 | 0.0 | 0.0 | 33.1 | 0.0 | 26.1 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear（g＿c），s | 16.0 | 0.0 | 0.0 | 0.0 | 33.1 | 0.0 | 26.1 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 1.00 |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 396 | 2379 | 0 | 0 | 2173 |  | 784 | 0 |  |  |  |  |
| V／C Ratio（X） | 0.94 | 0.46 | 0.00 | 0.00 | 0.68 |  | 0.87 | 0.00 |  |  |  |  |
| Avail Cap（c＿a），veh／h | 607 | 2379 | 0 | 0 | 2173 |  | 889 | 0 |  |  |  |  |
| HCM Platoon Ratio | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter（l） | 0.87 | 0.87 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |  |  |
| Uniform Delay（d），s／veh | 21.9 | 0.0 | 0.0 | 0.0 | 26.2 | 0.0 | 47.6 | 0.0 | 0.0 |  |  |  |
| Incr Delay（d2），s／veh | 15.4 | 0.6 | 0.0 | 0.0 | 1.8 | 0.0 | 9.6 | 0.0 | 0.0 |  |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \％ile BackOfQ（50\％），veh／ln | 6.2 | 0.2 | 0.0 | 0.0 | 11.9 | 0.0 | 11.7 | 0.0 | 0.0 |  |  |  |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 37.3 | 0.6 | 0.0 | 0.0 | 27.9 | 0.0 | 57.2 | 0.0 | 0.0 |  |  |  |
| LnGrp LOS | D | A | A | A | C |  | E | A |  |  |  |  |
| Approach Vol，veh／h |  | 1472 |  |  | 1487 |  |  | 685 |  |  |  |  |
| Approach Delay，s／veh |  | 9.8 |  |  | 27.9 |  |  | 57.2 |  |  |  |  |
| Approach LOS |  | A |  |  | C |  |  | E |  |  |  |  |
| Timer－Assigned Phs |  | 2 |  |  | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 93.1 |  |  | 24.6 | 68.5 |  | 36.9 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 6.1 |  |  | 5.6 | ＊ 6.1 |  | 5.8 |  |  |  |  |
| Max Green Setting（Gmax），s |  | 82.9 |  |  | 34.4 | ＊ 43 |  | 35.2 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  |  | 18.0 | 35.1 |  | 28.1 |  |  |  |  |
| Green Ext Time（p＿c），s |  | 16.6 |  |  | 1.0 | 6.4 |  | 2.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 26.1 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 | 4 | 4 | 4 | $\dagger$ | \% | ( | $\frac{1}{1}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | * |  | ${ }^{7}$ | F |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 9 | 2 | 49 | 14 | 4 | 28 | 70 | 52 | 14 | 30 | 44 | 12 |
| Future Volume (vph) | 9 | 2 | 49 | 14 | 4 | 28 | 70 | 52 | 14 | 30 | 44 | 12 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 50 |  | 0 | 50 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 25 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 94 |  |  | 694 |  |  | 670 |  |  | 298 |  |
| Travel Time (s) |  | 2.6 |  |  | 18.9 |  |  | 13.1 |  |  | 5.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  | 1 | 1 |  |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Heavy Vehicles (\%) | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 0\% | 0\% | 0\% | 0\% | 3\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |



2032 No Action - Weekday PM Peak Hour

|  | $\Rightarrow$ |  |  | $\checkmark$ | $\leftarrow$ |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  | \% | ¢ |  |  | * |  |  | \& |  |
| Trafic Volume (vph) | 3 | 279 | 1 | 74 | 471 | 18 | 7 | 1 | 46 | 9 | 1 | 7 |
| Future Volume (vph) | 3 | 279 | 1 | 74 | 471 | 18 | 7 | 1 | 46 | 9 | 1 | 7 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 5\% |  |  | -4\% |  |
| Storage Length (tt) | 0 |  | 0 | 175 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 35 |  |  | 25 |  |  | 25 |  |  | 25 |  |
| Link Distance (ft) |  | 369 |  |  | 1809 |  |  | 529 |  |  | 387 |  |
| Travel Time (s) |  | 7.2 |  |  | 49.3 |  |  | 14.4 |  |  | 10.6 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other <br> Control Type: Unsignalized  | Other |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |



| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficicting Flow All | 538 | 0 | 0 | 308 | 0 | 0 | 1009 | 1014 | 308 | 1030 | 1004 | 528 |  |
| Stage 1 | - | - | . | - | . | . | 314 | 314 | . | 690 | 690 | - |  |
| Stage 2 | - | - | - | - | - | - | 695 | 700 | - | 340 | 314 | - |  |
| Critical Hdwy | 4.12 | - | - | 4.11 | - | - | 8.1 | 7.5 | 6.7 | 6.3 | 5.7 | 5.8 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 7.1 | 6.5 | - | 5.3 | 4.7 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 7.1 | 6.5 |  | 5.3 | 4.7 | - |  |
| Follow-up Hdwy | 2.218 | - | - | 2.209 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |  |
| Pot Cap-1 Maneuver | 1030 | - | - | 1258 | - | - | 167 | 181 | 706 | 268 | 305 | 588 |  |
| Stage 1 | - | - | - | - | - | - | 643 | 605 | - | 511 | 523 | - |  |
| Stage 2 | - | - | - | - | - | - | 359 | 366 | - | 732 | 708 | - |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1030 | - | - | 1258 | - | - | 156 | 169 | 706 | 235 | 284 | 588 |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 156 | 169 | - | 235 | 284 | - |  |
| Stage 1 | - | - | - | - | - | - | 640 | 603 | - | 509 | 490 | - |  |
| Stage 2 | - | - | - | - | - | - | 331 | 343 | - | 676 | 705 | - |  |


| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 1.1 | 13.8 | 17.1 |
| HCM LOS |  | B | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh//) | 466 | 1030 | - | - | 1258 | - | -316 |
| HCM Lane V/C Ratio | 0.127 | 0.003 | - | - | 0.065 | - | -0.059 |
| HCM Control Delay (s) | 13.8 | 8.5 | 0 | - | 8.1 | - | -17.1 |
| HCM Lane LOS | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.4 | 0 | - | - | 0.2 | - | - |
| C |  | 0.2 |  |  |  |  |  |




## LANE LEVEL OF SERVICE

## Lane Level of Service

$\theta$ Site: 3 [2032 No Action - PM Peak Hour (Site Folder: 19th Ave
NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2032 No Action - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used).
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## - Site: 3 [2032 No Action - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2032 No Action - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | and <br> ows <br> HV ] <br> \% |  | $\begin{aligned} & \text { rival } \\ & \text { ows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | $\begin{gathered} \mathrm{ck} \text { Of } \\ \mathrm{ue} \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.018 | 12.0 | LOS B | 0.1 | 2.3 | 0.53 | 0.58 | 0.53 | 33.5 |
| 8 | T1 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.018 | 6.3 | LOS A | 0.1 | 2.3 | 0.53 | 0.58 | 0.53 | 34.2 |
| 18 | R2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.018 | 6.1 | LOS A | 0.1 | 2.3 | 0.53 | 0.58 | 0.53 | 33.9 |
| Appro |  |  | 18 | 3.0 | 18 | 3.0 | 0.018 | 8.1 | LOS A | 0.1 | 2.3 | 0.53 | 0.58 | 0.53 | 33.8 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1u | U | All MCs | 1 | 3.0 | 1 | 3.0 | 0.447 | 11.0 | LOS B | 3.2 | 82.6 | 0.17 | 0.32 | 0.17 | 32.0 |
| 1 | L2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.447 | 10.0 | LOS A | 3.2 | 82.6 | 0.17 | 0.32 | 0.17 | 33.6 |
| 6 | T1 | All MCs | 740 | 3.0 | 740 | 3.0 | 0.447 | 3.2 | LOS A | 3.2 | 82.6 | 0.17 | 0.32 | 0.17 | 32.6 |
| 16 | R2 | All MCs | 35 | 3.0 | 35 | 3.0 | 0.029 | 3.6 | LOS A | 0.1 | 3.4 | 0.13 | 0.41 | 0.13 | 32.3 |
| Appr |  |  | 782 | 3.0 | 782 | 3.0 | 0.447 | 3.2 | LOS A | 3.2 | 82.6 | 0.17 | 0.32 | 0.17 | 32.6 |
| North: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 12 | 3.0 | 12 | 3.0 | 0.068 | 9.2 | LOS A | 0.4 | 9.5 | 0.66 | 0.61 | 0.66 | 23.7 |
| 4 | T1 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.068 | 7.5 | LOS A | 0.4 | 9.5 | 0.66 | 0.61 | 0.66 | 28.5 |
| 14 | R2 | All MCs | 39 | 3.0 | 39 | 3.0 | 0.068 | 5.0 | LOS A | 0.4 | 9.5 | 0.66 | 0.61 | 0.66 | 23.8 |
| Approach |  |  | 56 | 3.0 | 56 | 3.0 | 0.068 | 6.1 | LOS A | 0.4 | 9.5 | 0.66 | 0.61 | 0.66 | 24.2 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 1 | 3.0 | 1 | 3.0 | 0.327 | 10.9 | LOS B | 2.1 | 53.1 | 0.14 | 0.30 | 0.14 | 32.3 |
| 5 | L2 | All MCs | 20 | 3.0 | 20 | 3.0 | 0.327 | 8.7 | LOS A | 2.1 | 53.1 | 0.14 | 0.30 | 0.14 | 32.3 |
| 2 | T1 | All MCs | 438 | 3.0 | 438 | 3.0 | 0.327 | 2.6 | LOS A | 2.1 | 53.1 | 0.14 | 0.30 | 0.14 | 32.9 |
| 12 | R2 | All MCs | 6 | 3.0 | 6 |  | 0.327 | 3.9 | LOS A | 2.1 | 53.1 | 0.14 | 0.30 | 0.14 | 34.3 |
| Appr |  |  | 465 | 3.0 | 465 | 3.0 | 0.327 | 2.9 | LOS A | 2.1 | 53.1 | 0.14 | 0.30 | 0.14 | 32.9 |
| All Ve | icles |  | 1321 | 3.0 | 1321 | 3.0 | 0.447 | 3.3 | LOS A | 3.2 | 82.6 | 0.19 | 0.33 | 0.19 | 32.2 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

## LANE LEVEL OF SERVICE

Lane Level of Service
$\square$ Site: 4 [2032 No Action - PM Peak Hour (Site Folder: 23rd Ave
NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2032 No Action - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | B | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used). Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\square$ Site: 4 [2032 No Action - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2032 No Action - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class |  | $\begin{aligned} & \text { land } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { rival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service |  | $\begin{gathered} \mathrm{ck} \text { Of } \\ \text { de } \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South: Private Dwy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.011 | 10.9 | LOS B | 0.1 | 1.7 | 0.77 | 0.57 | 0.77 | 23.0 |
| 8 | T1 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.011 | 5.8 | LOS A | 0.1 | 1.7 | 0.77 | 0.57 | 0.77 | 23.2 |
| 18 | R2 | All MCs | 5 | 0.0 | 5 | 0.0 | 0.011 | 6.6 | LOS A | 0.1 | 1.7 | 0.77 | 0.57 | 0.77 | 23.1 |
| Approach |  |  | 7 | 0.0 | 7 | 0.0 | 0.011 | 7.1 | LOS A | 0.1 | 1.7 | 0.77 | 0.57 | 0.77 | 23.1 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 40 | 1.6 | 40 | 1.6 | 0.373 | 11.1 | LOS B | 2.7 | 67.4 | 0.22 | 0.35 | 0.22 | 31.8 |
| 1 | L2 | All MCs | 1 | 1.6 | 1 | 1.6 | 0.373 | 8.8 | LOS A | 2.7 | 67.4 | 0.22 | 0.35 | 0.22 | 31.8 |
| 6 | T1 | All MCs | 886 | 1.6 | 886 | 1.6 | 0.373 | 3.1 | LOS A | 2.7 | 68.7 | 0.21 | 0.34 | 0.21 | 32.5 |
| 16 | R2 | All MCs | 253 | 1.6 | 253 | 1.6 | 0.373 | 3.4 | LOS A | 2.7 | 68.7 | 0.20 | 0.34 | 0.20 | 32.3 |
| Approach |  |  | 1181 | 1.6 | 1181 | 1.6 | 0.373 | 3.4 | LOS A | 2.7 | 68.7 | 0.21 | 0.34 | 0.21 | 32.4 |
| North: 23 rd Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 228 | 2.2 | 228 | 2.2 | 0.352 | 12.0 | LOS B | 2.3 | 58.8 | 0.82 | 0.75 | 0.82 | 22.1 |
| 4 | T1 | All MCs | 4 | 2.2 | 4 | 2.2 | 0.352 | 6.9 | LOS A | 2.3 | 58.8 | 0.82 | 0.75 | 0.82 | 22.2 |
| 14 | R2 | All MCs | 24 | 2.2 | 24 | 2.2 | 0.352 | 7.8 | LOS A | 2.3 | 58.8 | 0.82 | 0.75 | 0.82 | 22.2 |
| Approach |  |  | 256 | 2.2 | 256 | 2.2 | 0.352 | 11.6 | LOS B | 2.3 | 58.8 | 0.82 | 0.75 | 0.82 | 22.1 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5u | U | All MCs | 3 | 2.5 | 3 | 2.5 | 0.269 | 12.2 | LOS B | 1.7 | 43.5 | 0.51 | 0.48 | 0.51 | 31.0 |
| 5 | L2 | All MCs | 38 | 2.5 | 38 | 2.5 | 0.269 | 9.9 | LOS A | 1.7 | 43.5 | 0.51 | 0.48 | 0.51 | 31.0 |
| 2 | T1 | All MCs | 656 | 2.5 | 656 | 2.5 | 0.269 | 4.0 | LOS A | 1.8 | 46.3 | 0.50 | 0.44 | 0.50 | 31.7 |
| 12 | R2 | All MCs | 1 | 2.5 | 1 | 2.5 | 0.269 | 4.2 | LOS A | 1.8 | 46.3 | 0.49 | 0.41 | 0.49 | 31.5 |
| Approach |  |  | 699 | 2.5 | 699 | 2.5 | 0.269 | 4.3 | LOS A | 1.8 | 46.3 | 0.50 | 0.44 | 0.50 | 31.6 |
| All Vehicles |  |  | 2144 | 2.0 | 2144 | 2.0 | 0.373 | 4.7 | LOS A | 2.7 | 68.7 | 0.38 | 0.43 | 0.38 | 30.4 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {¢ }}$ |  | 4 | 44 | 「 | \％ | 4 | 「 | \％ | $\uparrow$ |  |
| Traffic Volume（vph） | 39 | 573 | 161 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 132 | 38 |
| Future Volume（vph） | 39 | 573 | 161 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 132 | 38 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 250 |  | 0 | 425 |  | 200 | 125 |  | 0 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 2 |  | 1 | 1 |  | 1 | 2 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 25 |  |  | 25 |  |
| Link Distance（ft） |  | 394 |  |  | 613 |  |  | 444 |  |  | 470 |  |
| Travel Time（s） |  | 7.7 |  |  | 11.9 |  |  | 12.1 |  |  | 12.8 |  |
| Confl．Peds．（\＃／hr） | 1 |  |  |  |  | 1 | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Turn Type | Prot | NA |  | Prot | NA | Perm | Prot | NA | pt＋ov | Prot | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 81 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  | 6 |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 | 6 | 3 | 8 | 81 | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 7.0 |  | 3.0 | 7.0 | 7.0 | 3.0 | 5.0 |  | 3.0 | 5.0 |  |
| Minimum Split（s） | 9.0 | 38.0 |  | 9.0 | 38.0 | 38.0 | 9.0 | 11.0 |  | 9.0 | 46.0 |  |
| Total Split（s） | 20.0 | 40.0 |  | 40.0 | 60.0 | 60.0 | 35.0 | 15.0 |  | 35.0 | 15.0 |  |
| Total Split（\％） | 15．4\％ | 30．8\％ |  | 30．8\％ | 46．2\％ | 46．2\％ | 26．9\％ | 11．5\％ |  | 26．9\％ | 11．5\％ |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／Lag | Lead | Lead |  | Lag | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | Min |  | C－Min | C－Min | C－Min | None | None |  | Min | Min |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 75 （58\％），Referenced to phase 1：WBL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 145 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：$\quad$ 5：27th Ave NE／Spring Ln Ave \＆172nd St NE


HCM 6th Signalized Intersection Summary
5：27th Ave NE／Spring Ln Ave \＆172nd St NE

|  | 4 | $\rightarrow$ | \％ | 7 |  | 4 | 4 | 4 | \％ | （ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {a }}$ |  | 7\％ | 中4 | 「 | \％ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume（veh／h） | 39 | 573 | 161 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 132 | 38 |
| Future Volume（veh／h） | 39 | 573 | 161 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 132 | 38 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 39 | 573 | 161 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 132 | 38 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 50 | 908 | 254 | 911 | 2023 | 901 | 275 | 151 | 545 | 497 | 97 | 28 |
| Arrive On Green | 0.03 | 0.33 | 0.33 | 0.44 | 0.94 | 0.94 | 0.15 | 0.08 | 0.08 | 0.14 | 0.07 | 0.07 |
| Sat Flow，veh／h | 1781 | 2740 | 768 | 3483 | 3582 | 1596 | 1795 | 1885 | 1586 | 3483 | 1404 | 404 |
| Grp Volume（v），veh／h | 39 | 371 | 363 | 968 | 792 | 333 | 247 | 120 | 836 | 427 | 0 | 170 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1731 | 1742 | 1791 | 1596 | 1795 | 1885 | 1586 | 1742 | 0 | 1808 |
| Q Serve（g＿s），s | 2.8 | 22.9 | 23.1 | 34.0 | 2.6 | 2.4 | 17.6 | 8.1 | 10.4 | 15.6 | 0.0 | 9.0 |
| Cycle Q Clear（g＿c），s | 2.8 | 22.9 | 23.1 | 34.0 | 2.6 | 2.4 | 17.6 | 8.1 | 10.4 | 15.6 | 0.0 | 9.0 |
| Prop In Lane | 1.00 |  | 0.44 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.22 |
| Lane Grp Cap（c），veh／h | 50 | 589 | 574 | 911 | 2023 | 901 | 275 | 151 | 545 | 497 | 0 | 125 |
| V／C Ratio（X） | 0.78 | 0.63 | 0.63 | 1.06 | 0.39 | 0.37 | 0.90 | 0.80 | 1.54 | 0.86 | 0.00 | 1.36 |
| Avail Cap（c＿a），veh／h | 192 | 589 | 574 | 911 | 2023 | 901 | 401 | 151 | 545 | 777 | 0 | 125 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.51 | 0.51 | 0.51 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 62.8 | 36.7 | 36.8 | 36.6 | 1.7 | 1.7 | 54.0 | 58.8 | 20.3 | 54.5 | 0.0 | 60.5 |
| Incr Delay（d2），s／veh | 17.1 | 2.2 | 2.3 | 40.2 | 0.3 | 0.6 | 15.3 | 25.0 | 250.0 | 5.0 | 0.0 | 204.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.5 | 10.2 | 10.0 | 17.3 | 0.8 | 0.7 | 9.2 | 5.0 | 47.9 | 7.2 | 0.0 | 11.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 79.8 | 38.9 | 39.0 | 76.8 | 2.0 | 2.3 | 69.3 | 83.8 | 270.2 | 59.5 | 0.0 | 264.6 |
| LnGrp LOS | E | D | D | F | A | A | E | F | F | E | A | F |
| Approach Vol，veh／h |  | 773 |  |  | 2093 |  |  | 1203 |  |  | 597 |  |
| Approach Delay，s／veh |  | 41.0 |  |  | 36.6 |  |  | 210.4 |  |  | 117.9 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ）， s | 40.0 | 49.1 | 25.9 | 15.0 | 9.7 | 79.4 | 24.5 | 16.4 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 34.0 | 34.0 | 29.0 | 9.0 | 14.0 | 54.0 | 29.0 | 9.0 |  |  |  |  |
| Max Q Clear Time（g＿c +1 ），s | 36.0 | 25.1 | 19.6 | 11.0 | 4.8 | 4.6 | 17.6 | 12.4 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 3.0 | 0.4 | 0.0 | 0.0 | 8.1 | 1.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 92.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | F |  |  |  |  |  |  |  |  |  |

User approved pedestrian interval to be less than phase max green．

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | \％ | （ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 44 | 「 |  |  |  | ＊ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 0 | 1349 | 591 | 0 | 1751 | 755 | 0 | 0 | 0 | 382 | 0 | 362 |
| Future Volume（vph） | 0 | 1349 | 591 | 0 | 1751 | 755 | 0 | 0 | 0 | 382 | 0 | 362 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 3\％ |  |  | －3\％ |  |  | 0\％ |  |  | 3\％ |  |
| Storage Length（ft） | 0 |  | 250 | 0 |  | 0 | 0 |  | 0 | 400 |  | 400 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 0 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 613 |  |  | 915 |  |  | 299 |  |  | 608 |  |
| Travel Time（s） |  | 11.9 |  |  | 17.8 |  |  | 6.8 |  |  | 13.8 |  |
| Confl．Peds．（\＃／hr） | 11 |  |  |  |  | 11 | 1 |  |  |  |  | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 1\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ | 4\％ | 4\％ | 4\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 50\％ |  |  |
| Turn Type |  | NA | Perm |  | NA | Perm |  |  |  | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  |  |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  |  |  |  | 4 |
| Detector Phase |  | 2 | 2 |  | 6 | 6 |  |  |  | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  |  | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） |  | 24.8 | 24.8 |  | 34.1 | 34.1 |  |  |  | 33.8 | 33.8 | 33.8 |
| Total Split（s） |  | 90.0 | 90.0 |  | 40.0 | 40.0 |  |  |  | 40.0 | 40.0 | 40.0 |
| Total Split（\％） |  | 69．2\％ | 69．2\％ |  | 30．8\％ | 30．8\％ |  |  |  | 30．8\％ | 30．8\％ | 30．8\％ |
| Yellow Time（s） |  | 3.8 | 3.8 |  | 4.1 | 4.1 |  |  |  | 3.8 | 3.8 | 3.8 |
| All－Red Time（s） |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 5.8 | 5.8 |  | 6.1 | 6.1 |  |  |  | 5.8 | 5.8 | 5.8 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode |  | C－Min | C－Min |  | C－Min | C－Min |  |  |  | None | None | None |

## Intersection Summary

## Area Type：

Cycle Length： 130
Actuated Cycle Length： 130
Offset： 0 （ $0 \%$ ），Referenced to phase 2：EBT and 6：WBT，Start of Red
Natural Cycle： 90
Control Type：Actuated－Coordinated
Splits and Phases：6：I－5 SB Ramp \＆172nd St NE


|  | $\rangle$ | $\rightarrow$ | $\checkmark$ | 7 |  |  | ， |  | \％ |  | $\frac{1}{*}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 中4 | 「 |  | 44 | 「 |  |  |  | ${ }^{1}$ | $\uparrow$ | 7 |
| Traffic Volume（veh／h） | 0 | 1349 | 591 | 0 | 1751 | 755 | 0 | 0 | 0 | 382 | 0 | 362 |
| Future Volume（veh／h） | 0 | 1349 | 591 | 0 | 1751 | 755 | 0 | 0 | 0 | 382 | 0 | 362 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 0 | 1832 | 1832 | 0 | 1988 | 1988 |  |  |  | 1788 | 1788 | 1788 |
| Adj Flow Rate，veh／h | 0 | 1391 | 0 | 0 | 1805 | 0 |  |  |  | 394 | 0 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |  |  |  | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 1 | 1 | 0 | 2 | 2 |  |  |  | 4 | 4 | 4 |
| Cap，veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 501 | 0 |  |
| Arrive On Green | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 |  |  |  | 0.15 | 0.00 | 0.00 |
| Sat Flow，veh／h | 0 | 3573 | 1553 | 0 | 3877 | 1685 |  |  |  | 3405 | 0 | 1515 |
| Grp Volume（v），veh／h | 0 | 1391 | 0 | 0 | 1805 | 0 |  |  |  | 394 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1741 | 1553 | 0 | 1889 | 1685 |  |  |  | 1703 | 0 | 1515 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 14.5 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 14.5 | 0.0 | 0.0 |
| Prop In Lane | 0.00 |  | 1.00 | 0.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 501 | 0 |  |
| V／C Ratio（X） | 0.00 | 0.52 |  | 0.00 | 0.63 |  |  |  |  | 0.79 | 0.00 |  |
| Avail Cap（c＿a），veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 896 | 0 |  |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 2.00 | 2.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.19 | 0.00 | 0.00 | 0.17 | 0.00 |  |  |  | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 53.5 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 |  |  |  | 4.7 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 |  |  |  | 6.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 |  |  |  | 58.2 | 0.0 | 0.0 |
| LnGrp LOS | A | A |  | A | A |  |  |  |  | E | A |  |
| Approach Vol，veh／h |  | 1391 |  |  | 1805 |  |  |  |  |  | 394 |  |
| Approach Delay，s／veh |  | 0.1 |  |  | 0.2 |  |  |  |  |  | 58.2 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | E |  |
| Timer－Assigned Phs |  | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+\mathrm{Rc}$ ），s |  | 105.1 |  | 24.9 |  | 105.1 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），s |  | ＊ 6.1 |  | ＊ 5.8 |  | 6.1 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | ＊ 84 |  | ＊ 34 |  | 33.9 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 16.5 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 25.7 |  | 2.4 |  | 23.7 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［EBR，WBR，SBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 44 |  |  | 坐4 | F' | \% | $\uparrow$ | 「' |  |  |  |
| Traffic Volume (vph) | 427 | 1273 | 0 | 0 | 1719 | 638 | 774 | 3 | 981 | 0 | 0 | 0 |
| Future Volume (vph) | 427 | 1273 | 0 | 0 | 1719 | 638 | 774 | 3 | 981 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 6\% |  |  | 5\% |  |  | 0\% |  |
| Storage Length (ft) | 600 |  | 0 | 0 |  | 300 | 400 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 915 |  |  | 978 |  |  | 589 |  |  | 234 |  |
| Travel Time (s) |  | 17.8 |  |  | 19.1 |  |  | 13.4 |  |  | 5.3 |  |
| Confl. Peds. (\#/hr) | 8 |  | 11 | 11 |  | 8 |  |  | 4 | 4 |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  | 50\% |  |  |  |  |  |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Split | NA | Perm |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 | 8 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  | 6 |  |  | 8 |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 | 6 | 8 | 8 | 8 |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  |  | 7.0 | 7.0 | 5.0 | 5.0 | 5.0 |  |  |  |
| Minimum Split (s) | 10.6 | 24.1 |  |  | 23.8 | 23.8 | 40.8 | 40.8 | 40.8 |  |  |  |
| Total Split (s) | 40.0 | 89.0 |  |  | 49.0 | 49.0 | 41.0 | 41.0 | 41.0 |  |  |  |
| Total Split (\%) | 30.8\% | 68.5\% |  |  | 37.7\% | 37.7\% | 31.5\% | 31.5\% | 31.5\% |  |  |  |
| Yellow Time (s) | 3.6 | 4.1 |  |  | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |  |  |
| All-Red Time (s) | 2.0 | 2.0 |  |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Total Lost Time (s) | 5.6 | 6.1 |  |  | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |  |  |  |
| Lead/Lag | Lead |  |  |  | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  |  | Yes | Yes |  |  |  |  |  |  |
| Recall Mode | None | C-Min |  |  | C-Min | C-Min | None | None | None |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL and 6:WBT, Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: $\quad$ : I-5 NB Ramps \& 172nd St NE


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

## Notes

User approved volume balancing among the lanes for turning movement.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Unsignalized Delay for [NBR, WBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\Rightarrow$ |  |  | $\checkmark$ | $\leftarrow$ |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  | \% | ¢ |  |  | * |  |  | \& |  |
| Trafic Volume (vph) | 3 | 289 | 1 | 75 | 478 | 18 | 7 | 1 | 48 | 9 | 1 | 7 |
| Future Volume (vph) | 3 | 289 | 1 | 75 | 478 | 18 | 7 | 1 | 48 | 9 | 1 | 7 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 5\% |  |  | -4\% |  |
| Storage Length (tt) | 0 |  | 0 | 175 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 35 |  |  | 25 |  |  | 25 |  |  | 25 |  |
| Link Distance (ft) |  | 369 |  |  | 1809 |  |  | 529 |  |  | 387 |  |
| Travel Time (s) |  | 7.2 |  |  | 49.3 |  |  | 14.4 |  |  | 10.6 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |




|  | EB | WB | NB | SB |
| :--- | :--- | :---: | :---: | ---: |
| Approach | 1.1 | 14 | 17.4 |  |
| HCM Control Delay, s | 0.1 |  | B | C |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 460 | 1024 | - | - | 1247 | - | - |
| HCM Lane V/C Ratio | 0.134 | 0.003 | - | - | 0.066 | - | -0.061 |
| HCM Control Delay (s) | 14 | 8.5 | 0 | - | 8.1 | - | - |
| HCM Lane LOS | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0.2 | - | - |




## LANE LEVEL OF SERVICE

## Lane Level of Service

$\square$ Site: 3 [2032 With Project - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2032 With Project - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | A | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used).
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\checkmark$ Site: 3 [2032 With Project - PM Peak Hour (Site Folder: 19th Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
19th Ave NE / 172nd St NE
Site Category: 2032 With Project - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{aligned} & \text { land } \\ & \text { lows } \\ & \mathrm{HV} \text { ] } \\ & \% \end{aligned}$ |  | rival ows HV ] \% | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service |  | ck Of le Dist ] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed <br> mph |
| South: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.019 | 12.4 | LOS B | 0.1 | 2.6 | 0.58 | 0.60 | 0.58 | 33.3 |
| 8 | T1 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.019 | 6.7 | LOS A | 0.1 | 2.6 | 0.58 | 0.60 | 0.58 | 34.0 |
| 18 | R2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.019 | 6.5 | LOS A | 0.1 | 2.6 | 0.58 | 0.60 | 0.58 | 33.7 |
| Approach |  |  | 18 | 3.0 | 18 | 3.0 | 0.019 | 8.5 | LOS A | 0.1 | 2.6 | 0.58 | 0.60 | 0.58 | 33.7 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 1 | 3.0 | 1 | 3.0 | 0.454 | 11.1 | LOS B | 3.3 | 84.4 | 0.23 | 0.33 | 0.23 | 31.9 |
| 1 | L2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.454 | 10.1 | LOS B | 3.3 | 84.4 | 0.23 | 0.33 | 0.23 | 33.4 |
| 6 | T1 | All MCs | 740 | 3.0 | 740 | 3.0 | 0.454 | 3.3 | LOS A | 3.3 | 84.4 | 0.23 | 0.33 | 0.23 | 32.4 |
| 16 | R2 | All MCs | 98 | 3.0 | 98 | 3.0 | 0.083 | 3.7 | LOS A | 0.4 | 10.0 | 0.18 | 0.42 | 0.18 | 32.2 |
| Approach |  |  | 845 | 3.0 | 845 | 3.0 | 0.454 | 3.4 | LOS A | 3.3 | 84.4 | 0.22 | 0.34 | 0.22 | 32.4 |
| North: 19th Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 55 | 3.0 | 55 | 3.0 | 0.140 | 9.4 | LOS A | 0.8 | 20.5 | 0.69 | 0.65 | 0.69 | 23.2 |
| 4 | T1 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.140 | 7.7 | LOS A | 0.8 | 20.5 | 0.69 | 0.65 | 0.69 | 27.7 |
| 14 | R2 | All MCs | 53 | 3.0 | 53 |  | 0.140 | 5.2 | LOS A | 0.8 | 20.5 | 0.69 | 0.65 | 0.69 | 23.3 |
| Approach |  |  | 114 | 3.0 | 114 | 3.0 | 0.140 | 7.4 | LOS A | 0.8 | 20.5 | 0.69 | 0.65 | 0.69 | 23.4 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $5 u$ | U | All MCs | 1 | 3.0 | 1 | 3.0 | 0.355 | 11.1 | LOS B | 2.4 | 60.9 | 0.27 | 0.35 | 0.27 | 31.8 |
| 5 | L2 | All MCs | 40 | 3.0 | 40 | 3.0 | 0.355 | 8.9 | LOS A | 2.4 | 60.9 | 0.27 | 0.35 | 0.27 | 31.8 |
| 2 | T1 | All MCs | 438 | 3.0 | 438 | 3.0 | 0.355 | 2.9 | LOS A | 2.4 | 60.9 | 0.27 | 0.35 | 0.27 | 32.5 |
| 12 | R2 | All MCs | 6 | 3.0 | 6 | 3.0 | 0.355 | 4.1 | LOS A | 2.4 | 60.9 | 0.27 | 0.35 | 0.27 | 33.8 |
| Approach |  |  | 485 | 3.0 | 485 | 3.0 | 0.355 | 3.4 | LOS A | 2.4 | 60.9 | 0.27 | 0.35 | 0.27 | 32.4 |
| All Vehicles |  |  | 1461 | 3.0 | 1461 | 3.0 | 0.454 | 3.8 | LOS A | 3.3 | 84.4 | 0.28 | 0.37 | 0.28 | 31.5 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

## LANE LEVEL OF SERVICE

## Lane Level of Service

$\forall$ Site: 4 [2032 With Project - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]
Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2032 With Project - PM Peak Hour
Roundabout

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | A | A | B | A | A |



Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used). Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

## MOVEMENT SUMMARY

## $\square$ Site: 4 [2032 With Project - PM Peak Hour (Site Folder: 23rd Ave NE / 172nd St NE)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200
23rd Ave NE / 172nd St NE
Site Category: 2032 With Project - PM Peak Hour
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Mov Class |  | $\begin{aligned} & \text { land } \\ & \text { lows } \\ & \mathrm{HV} \text { ] } \\ & \% \end{aligned}$ |  | rival ows HV ] \% | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service |  | $\begin{aligned} & c k \text { Of } \\ & \text { e } \\ & \text { Dist ] } \\ & \mathrm{ft} \end{aligned}$ | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed <br> mph |
| South: Private Dwy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.011 | 11.4 | LOS B | 0.1 | 1.8 | 0.80 | 0.59 | 0.80 | 22.9 |
| 8 | T1 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.011 | 6.3 | LOS A | 0.1 | 1.8 | 0.80 | 0.59 | 0.80 | 23.0 |
| 18 | R2 | All MCs | 5 | 0.0 | 5 | 0.0 | 0.011 | 7.2 | LOS A | 0.1 | 1.8 | 0.80 | 0.59 | 0.80 | 23.0 |
| Approach |  |  | 7 | 0.0 | 7 | 0.0 | 0.011 | 7.7 | LOS A | 0.1 | 1.8 | 0.80 | 0.59 | 0.80 | 23.0 |
| East: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 u | U | All MCs | 40 | 1.6 | 40 | 1.6 | 0.391 | 11.1 | LOS B | 2.9 | 72.5 | 0.22 | 0.35 | 0.22 | 31.8 |
| 1 | L2 | All MCs | 1 | 1.6 | 1 | 1.6 | 0.391 | 8.8 | LOS A | 2.9 | 72.5 | 0.22 | 0.35 | 0.22 | 31.8 |
| 6 | T1 | All MCs | 943 | 1.6 | 943 | 1.6 | 0.391 | 3.1 | LOS A | 2.9 | 73.8 | 0.21 | 0.34 | 0.21 | 32.4 |
| 16 | R2 | All MCs | 253 | 1.6 | 253 | 1.6 | 0.391 | 3.4 | LOS A | 2.9 | 73.8 | 0.20 | 0.34 | 0.20 | 32.3 |
| Approach |  |  | 1237 | 1.6 | 1237 | 1.6 | 0.391 | 3.4 | LOS A | 2.9 | 73.8 | 0.21 | 0.34 | 0.21 | 32.4 |
| North: 23rd Ave NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 228 | 2.2 | 228 | 2.2 | 0.373 | 13.1 | LOS B | 2.5 | 64.6 | 0.86 | 0.77 | 0.87 | 21.9 |
| 4 | T1 | All MCs | 4 | 2.2 | 4 | 2.2 | 0.373 | 7.9 | LOS A | 2.5 | 64.6 | 0.86 | 0.77 | 0.87 | 22.0 |
| 14 | R2 | All MCs | 24 | 2.2 | 24 |  | 0.373 | 8.8 | LOS A | 2.5 | 64.6 | 0.86 | 0.77 | 0.87 | 22.0 |
| Approach |  |  | 256 | 2.2 | 256 | 2.2 | 0.373 | 12.6 | LOS B | 2.5 | 64.6 | 0.86 | 0.77 | 0.87 | 21.9 |
| West: 172nd St NE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 u | U | All MCs | 3 | 2.5 | 3 | 2.5 | 0.285 | 12.2 | LOS B | 1.8 | 46.9 | 0.52 | 0.48 | 0.52 | 30.9 |
| 5 | L2 | All MCs | 38 | 2.5 | 38 | 2.5 | 0.285 | 9.9 | LOS A | 1.8 | 46.9 | 0.52 | 0.48 | 0.52 | 31.0 |
| 2 | T1 | All MCs | 696 | 2.5 | 696 | 2.5 | 0.285 | 4.0 | LOS A | 2.0 | 50.0 | 0.51 | 0.44 | 0.51 | 31.6 |
| 12 | R2 | All MCs | 1 | 2.5 | 1 | 2.5 | 0.285 | 4.3 | LOS A | 2.0 | 50.0 | 0.50 | 0.41 | 0.50 | 31.5 |
| Approach |  |  | 738 | 2.5 | 738 | 2.5 | 0.285 | 4.3 | LOS A | 2.0 | 50.0 | 0.51 | 0.44 | 0.51 | 31.6 |
| All Vehicles |  |  | 2239 | 2.0 | 2239 | 2.0 | 0.391 | 4.8 | LOS A | 2.9 | 73.8 | 0.39 | 0.43 | 0.39 | 30.4 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: SIDRA HCM.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {a }}$ |  | 4 | 中4 | 「 | \％ | 4 | 「 | \％ | $\uparrow$ |  |
| Traffic Volume（vph） | 39 | 607 | 164 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 132 | 38 |
| Future Volume（vph） | 39 | 607 | 164 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 132 | 38 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 250 |  | 0 | 425 |  | 200 | 125 |  | 0 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 2 |  | 1 | 1 |  | 1 | 2 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 25 |  |  | 25 |  |
| Link Distance（ft） |  | 394 |  |  | 613 |  |  | 444 |  |  | 470 |  |
| Travel Time（s） |  | 7.7 |  |  | 11.9 |  |  | 12.1 |  |  | 12.8 |  |
| Confl．Peds．（\＃／hr） | 1 |  |  |  |  | 1 | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Turn Type | Prot | NA |  | Prot | NA | Perm | Prot | NA | pt＋ov | Prot | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 81 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  | 6 |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 | 6 | 3 | 8 | 81 | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 7.0 |  | 3.0 | 7.0 | 7.0 | 3.0 | 5.0 |  | 3.0 | 5.0 |  |
| Minimum Split（s） | 9.0 | 38.0 |  | 9.0 | 38.0 | 38.0 | 9.0 | 11.0 |  | 9.0 | 46.0 |  |
| Total Split（s） | 20.0 | 40.0 |  | 40.0 | 60.0 | 60.0 | 35.0 | 15.0 |  | 35.0 | 15.0 |  |
| Total Split（\％） | 15．4\％ | 30．8\％ |  | 30．8\％ | 46．2\％ | 46．2\％ | 26．9\％ | 11．5\％ |  | 26．9\％ | 11．5\％ |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／Lag | Lead | Lead |  | Lag | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | Min |  | C－Min | C－Min | C－Min | None | None |  | Min | Min |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type：Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 75 （58\％），Referenced to phase 1：WBL and 6：WBT，Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 145 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：$\quad$ 5：27th Ave NE／Spring Ln Ave \＆172nd St NE


HCM 6th Signalized Intersection Summary
5：27th Ave NE／Spring Ln Ave \＆172nd St NE

|  | 4 | $\rightarrow$ | \％ | 7 |  | 4 | 4 | 4 | \％ | （ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {a }}$ |  | 7\％ | 中4 | 「 | \％ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume（veh／h） | 39 | 607 | 164 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 132 | 38 |
| Future Volume（veh／h） | 39 | 607 | 164 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 132 | 38 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 39 | 607 | 164 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 132 | 38 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 50 | 910 | 245 | 911 | 2015 | 898 | 279 | 155 | 548 | 497 | 97 | 28 |
| Arrive On Green | 0.03 | 0.33 | 0.33 | 0.44 | 0.94 | 0.94 | 0.16 | 0.08 | 0.08 | 0.14 | 0.07 | 0.07 |
| Sat Flow，veh／h | 1781 | 2766 | 746 | 3483 | 3582 | 1596 | 1795 | 1885 | 1586 | 3483 | 1404 | 404 |
| Grp Volume（v），veh／h | 39 | 389 | 382 | 968 | 841 | 333 | 251 | 120 | 836 | 427 | 0 | 170 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1735 | 1742 | 1791 | 1596 | 1795 | 1885 | 1586 | 1742 | 0 | 1808 |
| Q Serve（g＿s），s | 2.8 | 24.5 | 24.6 | 34.0 | 3.0 | 2.5 | 17.8 | 8.1 | 10.7 | 15.6 | 0.0 | 9.0 |
| Cycle Q Clear（g＿c），s | 2.8 | 24.5 | 24.6 | 34.0 | 3.0 | 2.5 | 17.8 | 8.1 | 10.7 | 15.6 | 0.0 | 9.0 |
| Prop In Lane | 1.00 |  | 0.43 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.22 |
| Lane Grp Cap（c），veh／h | 50 | 585 | 571 | 911 | 2015 | 898 | 279 | 155 | 548 | 497 | 0 | 125 |
| V／C Ratio（X） | 0.78 | 0.67 | 0.67 | 1.06 | 0.42 | 0.37 | 0.90 | 0.78 | 1.53 | 0.86 | 0.00 | 1.36 |
| Avail Cap（c＿a），veh／h | 192 | 585 | 571 | 911 | 2015 | 898 | 401 | 155 | 548 | 777 | 0 | 125 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.47 | 0.47 | 0.47 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 62.8 | 37.5 | 37.5 | 36.6 | 1.8 | 1.8 | 53.9 | 58.5 | 19.9 | 54.5 | 0.0 | 60.5 |
| Incr Delay（d2），s／veh | 17.1 | 2.9 | 3.0 | 39.4 | 0.3 | 0.6 | 15.9 | 21.4 | 245.6 | 5.0 | 0.0 | 204.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.5 | 11.0 | 10.8 | 17.2 | 0.8 | 0.8 | 9.3 | 4.8 | 47.5 | 7.2 | 0.0 | 11.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 79.8 | 40.3 | 40.5 | 76.0 | 2.1 | 2.4 | 69.8 | 79.9 | 265.5 | 59.5 | 0.0 | 264.6 |
| LnGrp LOS | E | D | D | F | A | A | E | E | F | E | A | F |
| Approach Vol，veh／h |  | 810 |  |  | 2142 |  |  | 1207 |  |  | 597 |  |
| Approach Delay，s／veh |  | 42.3 |  |  | 35.6 |  |  | 206.4 |  |  | 117.9 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ）， s | 40.0 | 48.8 | 26.2 | 15.0 | 9.7 | 79.1 | 24.5 | 16.7 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 34.0 | 34.0 | 29.0 | 9.0 | 14.0 | 54.0 | 29.0 | 9.0 |  |  |  |  |
| Max Q Clear Time（g＿c +1 ），s | 36.0 | 26.6 | 19.8 | 11.0 | 4.8 | 5.0 | 17.6 | 12.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 2.8 | 0.4 | 0.0 | 0.0 | 8.6 | 1.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 90.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | F |  |  |  |  |  |  |  |  |  |

User approved pedestrian interval to be less than phase max green．

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | \％ | （ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 44 | 「 |  |  |  | ＊ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 0 | 1368 | 606 | 0 | 1790 | 755 | 0 | 0 | 0 | 382 | 0 | 372 |
| Future Volume（vph） | 0 | 1368 | 606 | 0 | 1790 | 755 | 0 | 0 | 0 | 382 | 0 | 372 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade（\％） |  | 3\％ |  |  | －3\％ |  |  | 0\％ |  |  | 3\％ |  |
| Storage Length（ft） | 0 |  | 250 | 0 |  | 0 | 0 |  | 0 | 400 |  | 400 |
| Storage Lanes | 0 |  | 1 | 0 |  | 1 | 0 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 613 |  |  | 915 |  |  | 299 |  |  | 608 |  |
| Travel Time（s） |  | 11.9 |  |  | 17.8 |  |  | 6.8 |  |  | 13.8 |  |
| Confl．Peds．（\＃／hr） | 11 |  |  |  |  | 11 | 1 |  |  |  |  | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 1\％ | 2\％ | 2\％ | 2\％ | 0\％ | 0\％ | 0\％ | 4\％ | 4\％ | 4\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 50\％ |  |  |
| Turn Type |  | NA | Perm |  | NA | Perm |  |  |  | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  |  |  | 4 | 4 |  |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  |  |  |  | 4 |
| Detector Phase |  | 2 | 2 |  | 6 | 6 |  |  |  | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  |  | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） |  | 24.8 | 24.8 |  | 34.1 | 34.1 |  |  |  | 33.8 | 33.8 | 33.8 |
| Total Split（s） |  | 90.0 | 90.0 |  | 40.0 | 40.0 |  |  |  | 40.0 | 40.0 | 40.0 |
| Total Split（\％） |  | 69．2\％ | 69．2\％ |  | 30．8\％ | 30．8\％ |  |  |  | 30．8\％ | 30．8\％ | 30．8\％ |
| Yellow Time（s） |  | 3.8 | 3.8 |  | 4.1 | 4.1 |  |  |  | 3.8 | 3.8 | 3.8 |
| All－Red Time（s） |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 5.8 | 5.8 |  | 6.1 | 6.1 |  |  |  | 5.8 | 5.8 | 5.8 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode |  | C－Min | C－Min |  | C－Min | C－Min |  |  |  | None | None | None |

## Intersection Summary

## Area Type：

Other
Cycle Length： 130
Actuated Cycle Length： 130
Offset： 0 （0\％），Referenced to phase 2：EBT and 6：WBT，Start of Red
Natural Cycle： 90
Control Type：Actuated－Coordinated
Splits and Phases：6：I－5 SB Ramp \＆172nd St NE


|  | $\rangle$ | $\rightarrow$ | \％ | 7 |  |  | ， |  | \％ |  | $\frac{1}{*}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 中4 | 「 |  | 性 | 「 |  |  |  | ${ }^{1}$ | $\uparrow$ | 7 |
| Traffic Volume（veh／h） | 0 | 1368 | 606 | 0 | 1790 | 755 | 0 | 0 | 0 | 382 | 0 | 372 |
| Future Volume（veh／h） | 0 | 1368 | 606 | 0 | 1790 | 755 | 0 | 0 | 0 | 382 | 0 | 372 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 0 | 1832 | 1832 | 0 | 1988 | 1988 |  |  |  | 1788 | 1788 | 1788 |
| Adj Flow Rate，veh／h | 0 | 1410 | 0 | 0 | 1845 | 0 |  |  |  | 394 | 0 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |  |  |  | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 1 | 1 | 0 | 2 | 2 |  |  |  | 4 | 4 | 4 |
| Cap，veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 501 | 0 |  |
| Arrive On Green | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 |  |  |  | 0.15 | 0.00 | 0.00 |
| Sat Flow，veh／h | 0 | 3573 | 1553 | 0 | 3877 | 1685 |  |  |  | 3405 | 0 | 1515 |
| Grp Volume（v），veh／h | 0 | 1410 | 0 | 0 | 1845 | 0 |  |  |  | 394 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1741 | 1553 | 0 | 1889 | 1685 |  |  |  | 1703 | 0 | 1515 |
| Q Serve（g＿s），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 14.5 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 14.5 | 0.0 | 0.0 |
| Prop In Lane | 0.00 |  | 1.00 | 0.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 501 | 0 |  |
| V／C Ratio（X） | 0.00 | 0.53 |  | 0.00 | 0.64 |  |  |  |  | 0.79 | 0.00 |  |
| Avail Cap（c＿a），veh／h | 0 | 2651 |  | 0 | 2876 |  |  |  |  | 896 | 0 |  |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 2.00 | 2.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.16 | 0.00 | 0.00 | 0.13 | 0.00 |  |  |  | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 53.5 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 |  |  |  | 4.7 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 |  |  |  | 6.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 |  |  |  | 58.2 | 0.0 | 0.0 |
| LnGrp LOS | A | A |  | A | A |  |  |  |  | E | A |  |
| Approach Vol，veh／h |  | 1410 |  |  | 1845 |  |  |  |  |  | 394 |  |
| Approach Delay，s／veh |  | 0.1 |  |  | 0.1 |  |  |  |  |  | 58.2 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | E |  |
| Timer－Assigned Phs |  | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 105.1 |  | 24.9 |  | 105.1 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），s |  | ＊ 6.1 |  | ＊ 5.8 |  | 6.1 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | ＊ 84 |  | ＊ 34 |  | 33.9 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c +1 ），s |  | 2.0 |  | 16.5 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 26.4 |  | 2.4 |  | 24.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［EBR，WBR，SBR］is excluded from calculations of the approach delay and intersection delay．

|  | * |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 44 |  |  | 坐4 | F' | \% | $\uparrow$ | 「' |  |  |  |
| Traffic Volume (vph) | 434 | 1285 | 0 | 0 | 1736 | 638 | 796 | 3 | 981 | 0 | 0 | 0 |
| Future Volume (vph) | 434 | 1285 | 0 | 0 | 1736 | 638 | 796 | 3 | 981 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 0\% |  |  | 6\% |  |  | 5\% |  |  | 0\% |  |
| Storage Length (ft) | 600 |  | 0 | 0 |  | 300 | 400 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 35 |  |  | 35 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 915 |  |  | 978 |  |  | 589 |  |  | 234 |  |
| Travel Time (s) |  | 17.8 |  |  | 19.1 |  |  | 13.4 |  |  | 5.3 |  |
| Confl. Peds. (\#/hr) | 8 |  | 11 | 11 |  | 8 |  |  | 4 | 4 |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  | 50\% |  |  |  |  |  |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Split | NA | Perm |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 | 8 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  | 6 |  |  | 8 |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 | 6 | 8 | 8 | 8 |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  |  | 7.0 | 7.0 | 5.0 | 5.0 | 5.0 |  |  |  |
| Minimum Split (s) | 10.6 | 24.1 |  |  | 23.8 | 23.8 | 40.8 | 40.8 | 40.8 |  |  |  |
| Total Split (s) | 40.0 | 89.0 |  |  | 49.0 | 49.0 | 41.0 | 41.0 | 41.0 |  |  |  |
| Total Split (\%) | 30.8\% | 68.5\% |  |  | 37.7\% | 37.7\% | 31.5\% | 31.5\% | 31.5\% |  |  |  |
| Yellow Time (s) | 3.6 | 4.1 |  |  | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |  |  |
| All-Red Time (s) | 2.0 | 2.0 |  |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Total Lost Time (s) | 5.6 | 6.1 |  |  | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |  |  |  |
| Lead/Lag | Lead |  |  |  | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  |  | Yes | Yes |  |  |  |  |  |  |
| Recall Mode | None | C-Min |  |  | C-Min | C-Min | None | None | None |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL and 6:WBT, Start of Red |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 7: I-5 NB Ramps \& 172nd St NE


|  | 4 |  |  | $\%$ |  |  | 4 | 9 | \％ |  | 1 | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 44 |  |  | 坐乐 | 「 | \％ | $\uparrow$ | 「 |  |  |  |
| Traffic Volume（veh／h） | 434 | 1285 | 0 | 0 | 1736 | 638 | 796 | 3 | 981 | 0 | 0 | 0 |
| Future Volume（veh／h） | 434 | 1285 | 0 | 0 | 1736 | 638 | 796 | 3 | 981 | 0 | 0 | 0 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 0 | 0 | 1658 | 1658 | 1723 | 1723 | 1723 |  |  |  |
| Adj Flow Rate，veh／h | 443 | 1311 | 0 | 0 | 1771 | 0 | 814 | 0 | 0 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |  |  |  |
| Percent Heavy Veh，\％ | 2 | 2 | 0 | 0 | 2 | 2 | 2 | 2 | 2 |  |  |  |
| Cap，veh／h | 462 | 2286 | 0 | 0 | 1684 |  | 870 | 0 |  |  |  |  |
| Arrive On Green | 0.46 | 1.00 | 0.00 | 0.00 | 0.37 | 0.00 | 0.27 | 0.00 | 0.00 |  |  |  |
| Sat Flow，veh／h | 1781 | 3647 | 0 | 0 | 4676 | 1405 | 3282 | 0 | 1460 |  |  |  |
| Grp Volume（v），veh／h | 443 | 1311 | 0 | 0 | 1771 | 0 | 814 | 0 | 0 |  |  |  |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 0 | 0 | 1509 | 1405 | 1641 | 0 | 1460 |  |  |  |
| Q Serve（g＿s），s | 26.9 | 0.0 | 0.0 | 0.0 | 48.4 | 0.0 | 31.5 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear（g＿c），s | 26.9 | 0.0 | 0.0 | 0.0 | 48.4 | 0.0 | 31.5 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 1.00 |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Lane Grp Cap（c），veh／h | 462 | 2286 | 0 | 0 | 1684 |  | 870 | 0 |  |  |  |  |
| V／C Ratio（X） | 0.96 | 0.57 | 0.00 | 0.00 | 1.05 |  | 0.94 | 0.00 |  |  |  |  |
| Avail Cap（c＿a），veh／h | 527 | 2286 | 0 | 0 | 1684 |  | 889 | 0 |  |  |  |  |
| HCM Platoon Ratio | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter（I） | 0.77 | 0.77 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |  |  |
| Uniform Delay（d），s／veh | 26.7 | 0.0 | 0.0 | 0.0 | 40.8 | 0.0 | 46.7 | 0.0 | 0.0 |  |  |  |
| Incr Delay（d2），s／veh | 23.3 | 0.8 | 0.0 | 0.0 | 36.9 | 0.0 | 16.9 | 0.0 | 0.0 |  |  |  |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \％ile BackOfQ（50\％），veh／ln | 12.8 | 0.3 | 0.0 | 0.0 | 23.3 | 0.0 | 14.8 | 0.0 | 0.0 |  |  |  |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 50.0 | 0.8 | 0.0 | 0.0 | 77.7 | 0.0 | 63.6 | 0.0 | 0.0 |  |  |  |
| LnGrp LOS | D | A | A | A | F |  | E | A |  |  |  |  |
| Approach Vol，veh／h |  | 1754 |  |  | 1771 |  |  | 814 |  |  |  |  |
| Approach Delay，s／veh |  | 13.2 |  |  | 77.7 |  |  | 63.6 |  |  |  |  |
| Approach LOS |  | B |  |  | E |  |  | E |  |  |  |  |
| Timer－Assigned Phs |  | 2 |  |  | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ |  | 89.7 |  |  | 35.3 | 54.5 |  | 40.3 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s |  | 6.1 |  |  | 5.6 | ＊ 6.1 |  | 5.8 |  |  |  |  |
| Max Green Setting（Gmax），s |  | 82.9 |  |  | 34.4 | ＊ 43 |  | 35.2 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  |  | 28.9 | 50.4 |  | 33.5 |  |  |  |  |
| Green Ext Time（p＿c），s |  | 22.9 |  |  | 0.7 | 0.0 |  | 0.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 49.0 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  | 4 | 4 | $\dagger$ | $p$ | - | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \& |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 9 | 2 | 49 | 17 | 4 | 34 | 70 | 63 | 17 | 35 | 52 | 12 |
| Future Volume (vph) | 9 | 2 | 49 | 17 | 4 | 34 | 70 | 63 | 17 | 35 | 52 | 12 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 50 |  | 0 | 50 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Link Speed (mph) |  | 25 |  |  | 25 |  |  | 35 |  |  | 35 |  |
| Link Distance (ft) |  | 94 |  |  | 694 |  |  | 670 |  |  | 298 |  |
| Travel Time (s) |  | 2.6 |  |  | 18.9 |  |  | 13.1 |  |  | 5.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  | 1 | 1 |  |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Heavy Vehicles (\%) | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 0\% | 0\% | 0\% | 0\% | 3\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |



## Appendix D

Trip Generation Calculations

## English Crossing (Marysville)

Weekday Trip Generation Summary

| Land Use | Units ${ }^{1}$ | $\begin{gathered} \text { ITE } \\ \text { LUC }^{2} \end{gathered}$ | Trip Rate or Equation ${ }^{2}$ | Directional Distribution | Trips Generated |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In Out | In | Out | Total |
| DAILY |  |  |  |  |  |  |  |
| Proposed Use: |  |  |  |  |  |  |  |
| Single-Family Attached Housing | 250 DU | 215 | $\mathrm{T}=7.62(\mathrm{X})-50.48$ | $50 \%$ 50\% | 927 | 928 | 1,855 |
|  |  |  |  | New Daily Trips = | 927 | 928 | 1,855 |
| AM PEAK HOUR |  |  |  |  |  |  |  |
| Proposed Use: |  |  |  |  |  |  |  |
| Single-Family Attached Housing | 250 DU | 215 | $T=0.52(X)-5.70$ | 25\% $75 \%$ | 31 | 93 | 124 |
|  |  |  |  | New AM Peak Hour Trips = | 31 | 93 | 124 |
| PM PEAK HOUR |  |  |  |  |  |  |  |
| Proposed Use: |  |  |  |  |  |  |  |
| Single-Family Attached Housing | 250 DU | 215 | $T=0.60(X)-3.93$ | $59 \%$ 41\% | 86 | 60 | 146 |
|  |  |  |  | New PM Peak Hour Trips = | 86 | 60 | 146 |
| Notes: |  |  |  |  |  |  |  |
| ${ }^{2}$ Based on Institute of Transportation Eng | (ITE) Trip G | ation Ma | 1 th Edition, 2021. |  |  |  |  |

## Appendix E

City of Marysville Model Distribution

LAKEWOOD N/O 172ND ST NE - EXISTING
(20\%


Existing Distribution
Marysvillet Marysville


THE CITY OF MARYSVILLE DISCLAIMS ANY WARRANTY OF MERCHANTABILITY OR WARRANTY OF FITNESS OF THIS
DATA FOR ANY PARTICULAR PURPOSE, EITHER EXPRESSE OR IMPLIED. NO REPRESENTATION OR WARRANTY IS MADE CONCERNING THE ACCURACY, CURRENCY, COMPLETENESS OR QUALITY OF DATA DEPICTED. ANY USER OF THIS DATA ASSUMES ALL RESPONSIBILITY FOR USE THEREOF, AND FURTHER AGREES TO HOLD THE CITY OF MARYSVILLE LABUITY ARISING FROM ANY USE OF THIS DATA.

Tulalip
Indian
Indian
Reservation


## Appendix F

Snohomish County Key Intersection Impacts

Table F1
AM Peak Hour Trip Assignment at Key Intersections

| Key <br> Intersection ID\# | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 476 | 0 | 4 | 0 | 5 | 13 | 0 | 0 | 0 | 2 | 0 | 0 | 0 |
| 50 | 0 | 3 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 1 | 0 | 0 |
| 70 | 0 | 0 | 0 | 3 | 0 | 6 | 0 | 0 | 1 | 2 | 0 | 0 |
| 68 | 0 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 85 | 3 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 475 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 5 | 0 |
| 71 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 3 |
| 72 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |

Table F2
PM Peak Hour Trip Assignment at Key Intersections

| Key Intersection ID\# | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 476 | 0 | 21 | 0 | 6 | 15 | 0 | 0 | 0 | 9 | 0 | 0 | 0 |
| 50 | 0 | 13 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 5 | 0 | 0 |
| 70 | 0 | 0 | 0 | 3 | 0 | 6 | 0 | 0 | 4 | 9 | 0 | 0 |
| 68 | 0 | 4 | 0 | 3 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 0 |
| 85 | 4 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 475 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 6 | 0 |
| 71 | 6 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 4 |
| 72 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |



Attachment F1: Weekday AM Peak Hour Project Trip Distribution \& Assignment


Attachment F2: Weekday PM Peak Hour Project Trip Distribution \& Assignment


Figure F3: Weekday AM Peak Hour Project Trip Assignment at Key Intersections


Figure F4: Weekday PM Peak Hour Project Trip Assignment at Key Intersections

## Appendix G

Snohomish County Mitigation Offer Form

## Traffic Mitigation Offer to Snohomish County

The applicant completes part one and submits it to the City with a completed county traffic worksheet. The City completes part two and sends it to the County. The County completes part three and sends it back to the City.
Part One to be completed by Applicant

| Basic Development Information |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Name of City in which development is located Marysville |  |  |  |  |
| Name of Proposed Development English Crossing |  |  |  |  |
| City Project File Number (if known) PA23012 |  |  |  |  |
| Name of Applicant Huseby Homes |  |  |  |  |
| Address of Applicant 13110 NE 177th Place \#228 Woodinvile, WA 98072 |  |  |  |  |
| Proportionate Share Calculation: Choose Option A or B |  |  |  |  |
| $\square$ Option A: Based on a percentage of the County's adopted impact fee (attach traffic worksheet.) |  |  |  |  |
| 1. The applicable percentage of the County's fee: 20 \% |  |  |  |  |
| 2. Net New Average Daily Traffic: 1,855 ADT |  |  |  |  |
| 3. The adopted County impact fee for this development: 185 \$/ADT |  |  |  |  |
| 4. Total Proportionate Share Amount: \$ 68,635 |  |  |  |  |
| Option B: Based on a comprehensive traffic study (attach traffic worksheet and traffic study)$\qquad$ No road improvements are impacted. Hence, proportionate share amount is zero (\$0).$\qquad$ The following road improvements are impacted. The calculation of proportionate shares is summarized below. |  |  |  |  |
| List by Names/Description the Impacted County Projects (attach other pages if necessary) | County Project ID\# | PHTs Impacting Project | Capacity Cost per PHT | Proportionate Share Obligation per Impacted Project |
| 1. |  |  |  |  |
| 2. |  |  |  |  |
| 3. |  |  |  |  |
| 4. Total Proportionate Share Amount (sum of obligations for each impacted project) \$ |  |  |  |  |

## Trip Distribution and Assignment if required

If required, attach AM and PM peak-hour trip distribution and assignment. Attach traffic worksheet showing whether or not it is required and traffic study.

Mitigation of other impacts if required for developments generating more than 50 Peak-Hour Trips Mitigation of Impacts on Level of Service

- No impact or not applicable $\qquad$ Mitigation as described in attached traffic study.

Mitigation of Impacts on Inadequate Road ConditionsNo impact or not applicable $\qquad$ Mitigation as described in attached traffic study.

Mitigation for Impacts on Access or CirculationNo impact or not applicable $\qquad$ Mitigation as described in attached traffic study.

## $\square$ Written Offer

The Applicant hereby voluntarily agrees to pay the total proportionate share amount shown above for impacts of the proposed development on the capacity of Snohomish County roads and provide mitigation of all other impacts as indicated above and described in attached documents.

BY: $\qquad$ Date: $\qquad$
Signature by Authorized Official of Applicant or Authorized Representative

Print Name and Title
Instructions to Applicant. Submit this Offer, a completed county traffic worksheet, and any other attachments to the City with your initial application or send directly to Contact.pwCMS@snoco.org.

Part Two: To be completed by the City

| Receipt of Written Offer and attachments by City and routing to County |
| :--- |
| Name of Proposed Development |
| City Project File Number |
| Date Received |
| City Staffer Assigned to Project |
| Address |
| Phone |
| Instructions to City. Send this offer and all attachments to Contact.pwCMS@snoco.org <br> Received by: <br> $\frac{\text { Date: }}{\text { Initialed by City Staffer Name and Title }}$ |

Part Three: To be completed by Snohomish County



Attachment F1: Weekday AM Peak Hour Project Trip Distribution \& Assignment


Attachment F2: Weekday PM Peak Hour Project Trip Distribution \& Assignment

## Snohomish County Traffic Worksheet and Traffic Study Requirements for Developments in the City of Marysville

Snohomish County government, through an interlocal agreement (ILA) with the City of Marysville, may request traffic mitigation measures from any new development in the city that impacts roads in the unincorporated county. The City will impose the requested mitigation to the extent that the City determines that the mitigation is reasonably related to the impacts of the development. To determine the impacts, and to determine reasonable mitigation measures, the City of Marysville requires a traffic study from any development in the city that may have impacts on county roads. This 'traffic study' may be as simple as completing sections one and two of the county traffic worksheet below, or having a professional traffic engineer conduct a formal traffic study consistent with the requirements in section three below.

- If a development generates less than ten peak-hour trips and the applicant chooses Option A for mitigation payment (standard payment by percent of county impact fee), then the applicant will generally only have to fill out the first two sections of this traffic worksheet and complete a mitigation offer (see section four).
- However, if a development generates more than ten peak-hour trips, or if the applicant chooses Option $B$ for mitigation payment (comprehensive impact analysis), then the applicant will have to fill out the first section of this worksheet, complete a separate traffic study consistent with the requirements in section three, and complete a mitigation offer (see Section Four).
- Applicants should submit all documents to the City as part of their initial submittal.
- Traffic study requirements for impacts on county roads are based on the County's traffic mitigation ordinance (Chapter 30.66B) and the city/county ILA. At the end of this document find references to the county contacts and county web site (sources for may of the documents related to traffic mitigation).
- Following review of the documents submitted, the County may request supplemental information and analysis as necessary to determine the impacts of the development in accordance with the city/county ILA. The City will require the proposed development to submit the supplemental information and analysis to the extent that the City determines that it is necessary to determine the impacts of the development.


## Section One (1) Worksheet General Information

1. Name of Proposed Development __ English Crossing

City Development File Number (if known) PA23012
2. Name, Address and Phone Number of Applicant $\qquad$
Huseby Homes, 13110 NE 177th Place \#228 Woodinville, WA 98072
Phone \#: 425-286-9757
3. Development Site Address_17406 19th Ave NE, Marysville, WA
4. Is it a residential or commercial development? Yes
5. Description of Development (size and specific type)

The proposed project will include up to 250 Single-Family Attached townhome units on a site that is currently vacant.
6. How many new vehicle trips are expected to be generated by the proposed development? (For many common types of developments this information can be provided by the city or the county. For more complex developments trip generation may have to be determined under section three below)
124 AM Peak Hour_146_PM Peak Hour__1,855 Average Daily Trips (ADT)
7. Proportionate Share Impact Mitigation: All applicants have two options in determining the amount of their traffic mitigation payment:

X For determining the amount based on a percentage of the county fee go to section two.
___ For determining the amount based on a comprehensive traffic study go to section three.

1. Standard default estimated
percentage of trips impacting the or
City streets based on subareas
(See below) $\qquad$ 20 \%
2. Other Percentage: (Note: See author’s qualifications in section three below.) Estimated percentage of trips impacting county roads from attached trip distribution: $\qquad$ \%

| Residential <br> Developments <br> $20 \%$ | Commercial <br> Developments |
| :---: | :---: |
| $20 \%$ | $20 \%$ |
| $25 \%$ | $20 \%$ |
|  | $25 \%$ |
| $30 \%$ | $30 \%$ |
|  |  |
| $15 \%$ | $10 \%$ |

Sub-Area ID \#

## * City Subarea Description

| CI-MA-1 | North of 136th ST SE. <br> CI-MA-2 <br>  <br> North of 100th ST NE and South <br> of 136th ST SE. |
| :--- | :--- |
| CI-MA-3 | North of 76th ST NE, South of <br>  <br>  <br> 100th ST SE, and West of 51st |
| AV NE. |  |
| CI-MA-4 | North of 76th ST NE, South of <br>  <br> 100th ST SE, and East of 51st <br> AV NE. |
| CI-MA-5 | South of 76th ST NE. |

hes or imaginary extensions of * Note: Boundaries are either street centerlines or imaginary ex
street centerlines in places where the actual streets do not exist.

3. Development New Average Daily Trip Generation (ADT) 1,855
4. Type of Development (Residential or Commercial)_Residential
5. County Commercial Fee Rate $\$$ $\qquad$ 6. County Residential Fee Rate \$ 185
(Note: Consistent with county code and the ILA, developments pay the rate in effect at the time of their submittal. As of 07/13/11 the rates were $\$ 39$ for commercial developments and $\$ 46$ for residential developments. Through ordinance, the County Council can change these rates at any time, so consult with the County or look at Snohomish County Code 30.66B. 330 to find the latest fee rates.)
7. Calculation of Proportionate Share Impact Mitigation

$\frac{20 \%}{$| $\# 1 \text { or } \# 2 \text { above: }$ |
| :---: |
| $\% \text { of trips }$ |}$\times \frac{1,855}{\# 3 \text { above: }} \times \frac{185}{$|  ADT  |
| :---: |}$=$| \#5 or \#6 above: |
| :---: |
| Fee Rate |$>\frac{68,635}{$|  proportionate share  |
| :---: |
|  mitigating payment  |}

## 2(b) Determining whether or not an additional traffic study is necessary

Will the development generate more than 10 peak-hour trips or are there other impacts that need to be addressed (e.g., level of service, safety, or access and circulation)
$\qquad$ No. Skip section three and go to section four.
Yes. Read the introduction to section three and skip to section 3(b).

## Section Three (3) Traffic Study Requirements

Introduction: This section outlines requirements for traffic studies for impacts on County roads. If an applicant chooses (or is required) to complete a traffic study, then it should be submitted along with this worksheet and a mitigation offer. (Note on Author's Qualifications: A traffic study under this section must be conducted by an engineer licensed to practice in the state of Washington with special training and experience in traffic engineering and, preferably, membership in the institute of transportation engineers. For individuals/firms not on the City's approved list, the developer will provide, with the traffic study, the credentials of the individual or firm performing the traffic study certifying compliance with these qualifications.)

3(a) Proportionate share impact mitigation based on comprehensive traffic study

1. Development's Trip Generation and Distribution. Determine the PM peak-hour trip generation and distribution for the development consistent with Section 3(b) below.
2. Impacted Improvements. Determine which of the road sections with planned improvements in the county's impact fee cost basis (Transportation Needs Report Appendix D) are impacted by three or more development-generated directional PM peak hour trips (PM PHT).
3. Current Counts. For each impacted improvement, provide current traffic counts to determine the PM PHT.
4. Reserve Capacity. Determine "reserve capacity" for each impacted improvement by subtracting the current PM PHT from the maximum service volume (MSV) for the existing facility. Reserve capacity is set to zero if current PM PHT exceeds the MSV. For MSVs see County DPW Rule 4224.
5. New Capacity. New capacity is the incremental increase in PHT that could be accommodated with the planned improvement. Determine the new capacity of each impacted improvement by subtracting the current MSV from the future MSV after the improvement.
6. Chargeable Capacity. For each impacted improvement, add the reserve capacity to the new capacity.
7. Final Adjusted Cost. Find the cost of each impacted improvement and make any adjustments used by the County for tax credits (see Transportation Needs Report Appendix D).
8. Capacity Cost per Peak-Hour Trip. For each impacted improvement, determine the capacity cost per PM PHT by dividing the final adjusted improvement cost by the chargeable capacity.
9. Traffic Impacts. From step one above, take the total number of PM PHT (in both directions) impacting each planned improvement.
10. Proportionate Share. For each impacted improvement, determine the proportionate share impact mitigation by multiplying the capacity cost per peak-hour trip by the number of PM PHT impacting the improvement.

## 3(b) Trip Generation and AM and PM Peak Hour Trip Distribution and Assignment

Calculate AM, PM and Daily trip generation consistent with the ITE Trip Generation Handbook and Snohomish County Public Works Rule 4220. Determine the trip distribution and assignments consistent with the County's document titled "Format for Trip Distributions"(available at County web site, see below).

- Within the developments transportation service area (TSA) the distributions will be carried out to each key intersection at which the approach or departure volumes on any leg have three (3) or more peak hour trips. Get the most current list of key intersections on the web site described below. Trips should be distributed onto the road system as it is expected to be in six years.
- The distribution should be a schematic map showing the broad distributions of trips in terms of percentages on different roads. Show all City boundaries.
- The assignment should be a schematic map with the impacted key intersections identified by ID\# and turning movements for each shown in separate diagrams on the same page or on different pages. The assignment should also be presented in tabular form listing each intersection by intersection ID\#, and the number of trips at each movement.


## 3(c) Additional Analysis for Developments Generating More Than Fifty (50) Peak Hour Trips

For large developments (i.e., those generating more than 50 peak-hour trips), the County may request mitigation for impacts on the level of service of County roads, documented safety locations (the County calls such locations "inadequate road conditions" or "IRCs"), and access or circulation. The traffic study requirements below are intended to disclose impacts. Based on this information the County may request through the City that the applicant provide additional information showing possible mitigation measures. If any off-site improvements were needed for mitigation the County would work with the applicant to determine requirements for right-ofway, construction plans, right-of-way use permits, construction/maintenance bonds, and other issues.

## Impacts on Level of Service (LOS) of County Arterials

Contact Snohomish County Public Works for the most current list of arterial units in arrears and critical arterial units. Identify any arterial units in arrears or critical arterial units impacted by three or more directional peak-hour trips.

## Impacts on Inadequate Road Conditions

Contact Snohomish County Public Works for a list of the current IRCs. Identify any IRCs impacted by three or more peak-hour trips. Note: Unlike LOS impacts in which at least three or more peak hour trips have to be added in one direction to require disclosure (e.g., 3 westbound), for IRCs, any three peak hour trips added to IRC locations are considered an impact for which disclosure is necessary (e.g., 2 westbound plus 1 eastbound).

## Impacts on Access or Circulation

The County may request improvements to existing roads to provide safe and efficient access and/or circulation. In some instances, the County may request provisions for future County roads identified in the Comprehensive Plan or in Small Area Transportation Studies. If so, the County will request specific additional information through the City.

## Section Four (4) Traffic Mitigation Offer to Snohomish County

The applicant should complete a traffic mitigation offer to Snohomish County that summarizes the mitigation identified in the county traffic worksheet and any additional traffic study. This will facilitate timely review of the development and processing of the application. The form to use for the mitigation offer is titled "Traffic Mitigation Offer to Snohomish County." This form is typically provided to all applicants along with this traffic study checklist. In addition, copies are available from the county contacts or the Snohomish County web site shown below.

## Additional Information

County Web Site
Snohomish County Public Works has a web site with many documents related to traffic studies and mitigation requirements for developers. From the Snohomish County Home Page go to:

Departments/Public Works/Divisions/TES/ProgramPlanning/3066B

## County Contacts

- Elbert Esparza, Snohomish County DPW Traffic, 3000 Rockefeller M/S 607, Everett WA 98201, (425) 388-3184, elbert.esparza@snoco.org


[^0]:    Source: WSDOT Collision Records.

